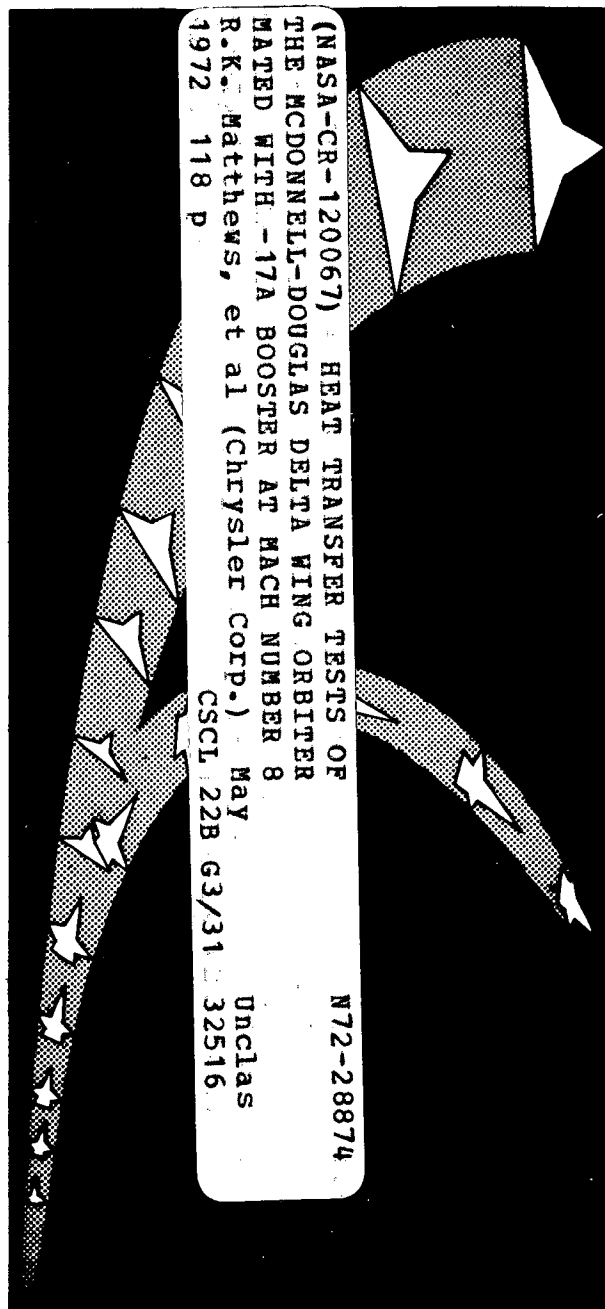


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DMS-DR-1262
CR-120,067
VOLUME I
MAY 1972



—SPACE SHUTTLE—

HEAT TRANSFER TESTS OF THE MCDONNELL-DOUGLAS DELTA WING ORBITER MATED WITH -17A BOOSTER AT MACH NUMBER 8

by

R. K. Matthews, ARO, Inc
W. R. Martindale, ARO, Inc
J. D. Warmbrod, MSFC

VKF 50 INCH
HYPERSONIC
JUL 1972
RECEIVED
TUDOR CITY
INPUT ORANGE
Arnold Engineering
Development Center

SADSAC SPACE SHUTTLE
AEROTHERMODYNAMIC
DATA MANAGEMENT SYSTEM

CONTRACT NAS8-4016
MARSHALL SPACE FLIGHT CENTER

SPACE DIVISION  CHRYSLER
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DMS-DR-1262
CR-120,067
Volume I
May, 1972

SADSAC/SPACE SHUTTLE

WIND TUNNEL TEST DATA REPORT

CONFIGURATION: McDonnell-Douglas Delta Wing Orbiter Mated With
the - 17A Booster

TEST PURPOSE: To Determine Interference Heating at Mach Number of 8

TEST FACILITY: AEDC VKF 50-Inch Hypersonic Tunnel B

TESTING AGENCY: AEDC - MSFC

TEST NO. & DATE: VT 1162-9; June, 1971

FACILITY COORDINATOR: L. L. Trimmer, ARO, Inc.

PROJECT ENGINEER(S): R. K. Matthews, W. R. Martindale, ARO, Inc.
J. D. Warmbrod, MSFC

Details of illustrations in
this document may be better
studied on microfiche

DATA MANAGEMENT SERVICES

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RELEASE APPROVAL: J. M. D. Kemp, Supervisor
Aero Thermo Data Group

CONTRACT NAS 8-4016

AMENDMENT 158

DRL 297 - 84a

This report has been prepared by Chrysler Corporation Space Division under a Data Management Contract to the NASA. Chrysler assumes no responsibility for the data presented herein other than its display characteristics.

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FOREWORD

The work reported herein was sponsored by the Marshall Space Flight Center (MSFC), NASA. The results of tests presented were obtained by ARO, Inc. (a subsidiary of Sverdrup and Parcel & Associates, Inc.), contract operator of the Arnold Engineering Development Center (AEDC), AFSC, Arnold Air Force Station, Tennessee. Ascent and reentry conditions were simulated on shuttle models designed by McDonnell Douglas (MDAC), North American Rockwell (NAR) and General Dynamics Convair (GDC). In addition a limited amount of data were obtained on two research models provided by the Langley Research Center (LRC). Because of the broad scope of these tests the data will be presented in a series of SADSAC reports. This report presents the results of the phase-change paint test conducted at Mach 8 in Tunnel B on the McDonnell Douglas Delta Wing Orbiter mated with the -17A Booster. This volume (Volume I) contains the mated data and Volume II contains the interference-free data for the orbiter and booster alone.

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NOMENCLATURE

ALPHA-MODEL (α)	Model angle of attack, deg
ALPHA-PREBEND	Sting prebend angle, deg
ALPHA-SECTOR	Tunnel sector pitch angle, deg
H(TO) or H	Heat-transfer coefficient based on $T_{aw} = T_0$, BTU/ft ² - sec - °R, and

$$H(TO) = \frac{\beta \sqrt{\rho c k}}{\sqrt{\Delta t}}$$

where β is obtained from

$$\frac{T_{pc} - T_i}{T_{aw} - T_i} = 1 - e^{\beta^2} \operatorname{erfc} \beta$$

and $\Delta t \sim$ del time

$T_{pc} \sim$ phase-change paint temperature, °R

$T_i \sim$ initial model temperature, °R

$T_{aw} \sim$ adiabatic wall temperature, °R

$\sqrt{\rho c k} \sim$ model material properties = 0.11-0.008 $\sqrt{(\Delta t)}$
BTU/ft²-sec^{1/2} - °R

H(.9T0) Heat transfer coefficient based on $T_{aw} = 0.9T_0$

H(.85T0) Heat transfer coefficient based on $T_{aw} = .85T_0$

HREF Reference heat transfer coefficient based on Fay-Riddell theory, BTU/ft²-sec °R

$$HREF = \left[\frac{8.139(P01)^{0.5} (MU-0)^{0.4} (1-P-INF/P01)^{0.25}}{(RN)^{0.5} (T0)^{0.15}} \right] \times [0.2235 + 0.0000135 (T_0 + 760)]$$

where P01 \sim stagnation pressure downstream of a normal shock, psia

MU-0 \sim air viscosity based on T_0 , lb_f sec/ft²

RN \sim reference nose radius, (0.011 ft)

MU-INF	Free-stream viscosity, lb-sec/ft ²
P-INF	Free-stream static pressure, psia
P0	Tunnel stilling chamber pressure, psia
Q-INF	Free-stream dynamic pressure, psia
RE/FT	Free-stream unit Reynolds number, ft ⁻¹
ROLL-MODEL	Model roll angle, deg
ST(T0)	Stanton number based on T ₀ , $ST(T0) = \frac{H(T0)}{\rho_{\infty} V_{\infty} [0.2235 + 0.0000135 (T_0 + T_{pc})] \times (32.17)}$
STREF	Reference Stanton number $STREF = \frac{HREF}{\rho_{\infty} V_{\infty} [0.2235 + 0.0000135 (T_0 + T_{pc})] \times (32.17)}$
T-INF	Free-stream static temperature, °R
T0	Tunnel stilling chamber temperature, °R
TW	Model wall temperature, °R
TIME	Time from start of model injection, sec
DEL TIME (Δt)	Time model exposed to airstream, sec
V-INF (V _∞)	Free-stream velocity, ft/sec
YAW	Model yaw angle, deg
X	Axial distance from booster nose to orbiter nose (1.86 in., see Fig. 3)

SECTION 1
INTRODUCTION

This report presents the results of a wind tunnel test program to determine aerodynamic heat transfer distributions on the McDonnell Douglas configurations. The tests were conducted at the Arnold Engineering Development Center (AEDC) in Tunnel B of the von Karman Gas Dynamics Facility (VKF). The test period was in June 1971.

Heat-transfer rates were determined by the phase-change paint technique on 0.011-scale Stycast[®] models using Tempilaq[®] as the surface temperature indicator. The nominal test conditions were; Mach 8, free-stream unit Reynolds numbers of 0.8×10^6 , 2.5×10^6 , and 3.7×10^6 , and angles of attack of -5, 0, +5 deg. Model details, test conditions, phase-change paint photographs and reduced heat-transfer coefficients are presented in this report.

SECTION 2

MODELS AND APPARATUS

2.1 MODEL DESCRIPTION

Model drawings were provided ARO, Inc. by the McDonnell Douglas Corporation and fabrication of the Stycast models was subcontracted to the Grumman Aircraft Corporation. Sketches showing the overall model dimensions of the orbiter and booster are presented in Figs. 1 and 2, respectively, and a photograph of the mated configuration is shown in Fig. 3. Table 1 provides additional configuration description details but it should be pointed out that the models were cast as one smooth surface without moveable control surfaces. Presented in Table 2 are model coordinate measurements referenced to the axis system illustrated in Figs. 1 and 2.

Six-in.-diam hemispheres were cast from the same batch of Stycast used to cast the models so that the Stycast thermal properties could be determined from calibration runs on the hemispheres. Also Chromel-Alumel thermocouples were cast into the models approximately 1/8-in. from the surface to measure the initial model temperature.

2.2 FACILITY DESCRIPTION

Tunnel B is a continuous, closed-circuit, variable density wind tunnel with an axisymmetric contoured nozzle and a 50-in.-diam test section. The tunnel can be operated at a nominal Mach number of 6 or 8 at stagnation pressures from 20 to 300 and 50 to 900 psia, respectively, at stagnation temperatures up to 1350°R. The model may be injected into the tunnel for a test run and then retracted for model cooling or model changes without interrupting the tunnel flow.

SECTION 3

PROCEDURES

3.1 TEST TECHNIQUE

Prior to each run the models were cleaned and cooled with alcohol and then spray painted with Tempilaq. In some cases the local interference region between the models was sprayed with a higher temperature paint since the surface temperatures were generally higher in this region (see group 206 for example). The models were installed on the model injection mechanism at the desired test attitude and the initial temperature of each model was measured with a thermocouple probe or with the model-embedded thermocouples. During the course of the test many of the embedded thermocouples became inoperative and the probe temperature was generally used to determine the initial temperatures of the models. The models were then injected into the airstream for approximately 20 seconds and during this time the model surface temperature rise produced isotherm melt lines. The progression of the melt lines was photographed with 70-mm sequenced cameras operating at 2 frames per second.

3.2 TEST CONDITIONS

Nominal test conditions are presented in the data summary sheets (Table 2). As mentioned in the foreword this test was part of a comprehensive Space Shuttle investigation and as a result the run numbers are not consecutive. The specific test conditions for each run (or group) are provided on the data tabulation sheets preceding each set of melt line photographs.

During each run the tunnel conditions and time of each picture were recorded on magnetic tape. The heat transfer coefficient for each picture was calculated from the semi-infinite slab transient heat conduction equation.

$$\frac{T_{pc} - T_i}{T_{aw} - T_i} = 1 - e\beta^2 \operatorname{erfc} \beta$$

where $\beta = \frac{h\sqrt{\Delta t}}{\sqrt{\rho ck}}$ and $\sqrt{\rho ck} = 0.11 - 0.008 \sqrt{\Delta t}$.

The equation for the thermal properties ($\sqrt{\rho ck}$) of Stycast was obtained by evaluation of a considerable amount of hemisphere calibration data and supplemented by VKF laboratory measurements.

Heat-transfer coefficients were calculated for assumed adiabatic wall temperatures of T_0 , $0.9T_0$, and $0.85T_0$ (see tabulated data sheets). The use of three values of T_{aw} provides an indication of the sensitivity of the heat-transfer coefficient (h) to the values of T_{aw} assumed. For the sake of consistency all heat-transfer coefficients shown on the photographs are based on $T_{aw} = T_0$.

All heat-transfer coefficients were non-dimensionalized by dividing by the stagnation point heat-transfer coefficient (Ref. 1) on a 0.011-ft radius sphere (a 1-ft radius sphere scaled down by the model scale).

SECTION 4

DATA PRESENTATION

The test results are presented as a series of four photographs obtained during each run and a post-test photograph of the interference

region when two paints were used. The photographs are grouped as follows:

<u>Model Surface</u>	<u>Re/ft</u>	<u>α</u>
Side view of mated configuration*	0.8×10^6	-5, 0, +5
	2.5×10^6	"
	3.7×10^6	0

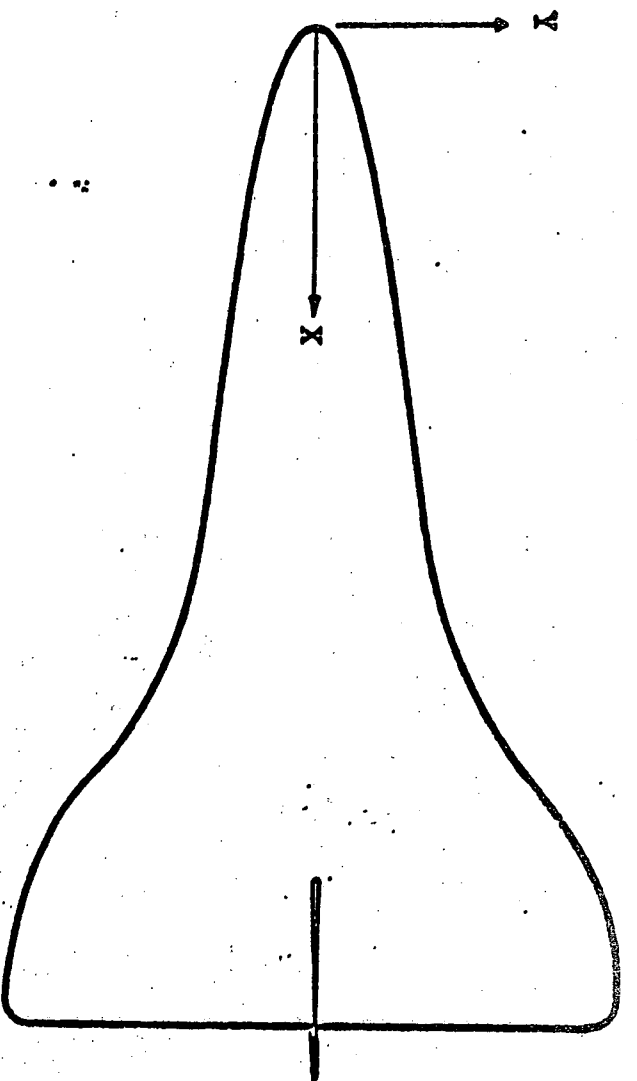
*The corresponding data for the orbiter and booster alone (non-interference) are presented in Volume II.

Preceding each set of photographs is a tabulated data sheet which lists the specific test conditions and the time of each picture with the corresponding heat-transfer parameters. Of course, the heat-transfer parameters apply only to the melt lines of the corresponding picture. Body coordinates of the melt lines may be obtained by use of the grid overlay provided with this report.

The post-test photographs give an indication of the severe heating which can occur between mated configurations if some type of wind shield or seal is not provided along the mating line. The heat-transfer ratios associated with the melt lines in these photographs are approximate because of the uncertainties in time and flow conditions which occur when the model is retracted from the airstream. Table 4, Page 38, presents a Summary Index for these data.

REFERENCES

1. Fay, J. A. and Riddell, F. R. "Theory of Stagnation Point Heat Transfer in Dissociated Air." Journal of the Aeronautical Sciences, Vol. 25, 1958, pp. 73-85.



Pressure Orifice	X/L
1	0.1
2	0.2
3	0.3
4	0.4
5	0.5
6	0.6
7	0.7
8	0.8
9	0.916
10	0.970

All Dimensions in Inches

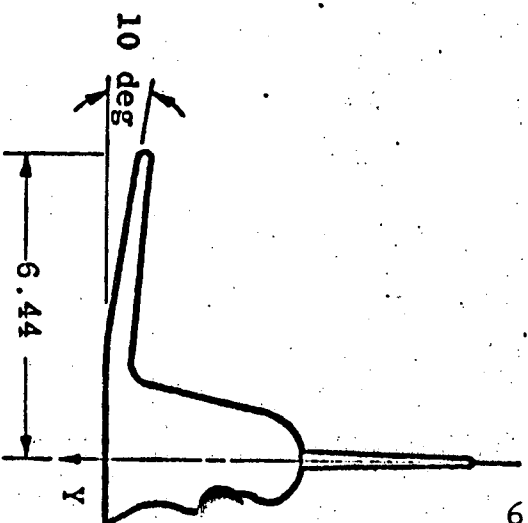
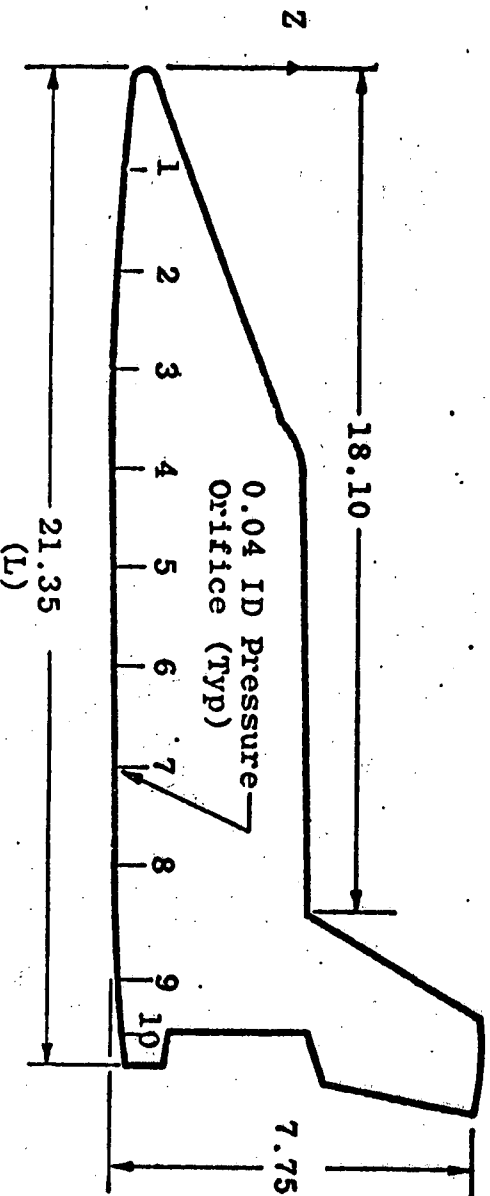


Fig. 1 McDonnell Douglas Delta Wing Orbiter Model Sketch (0.011 Scale)

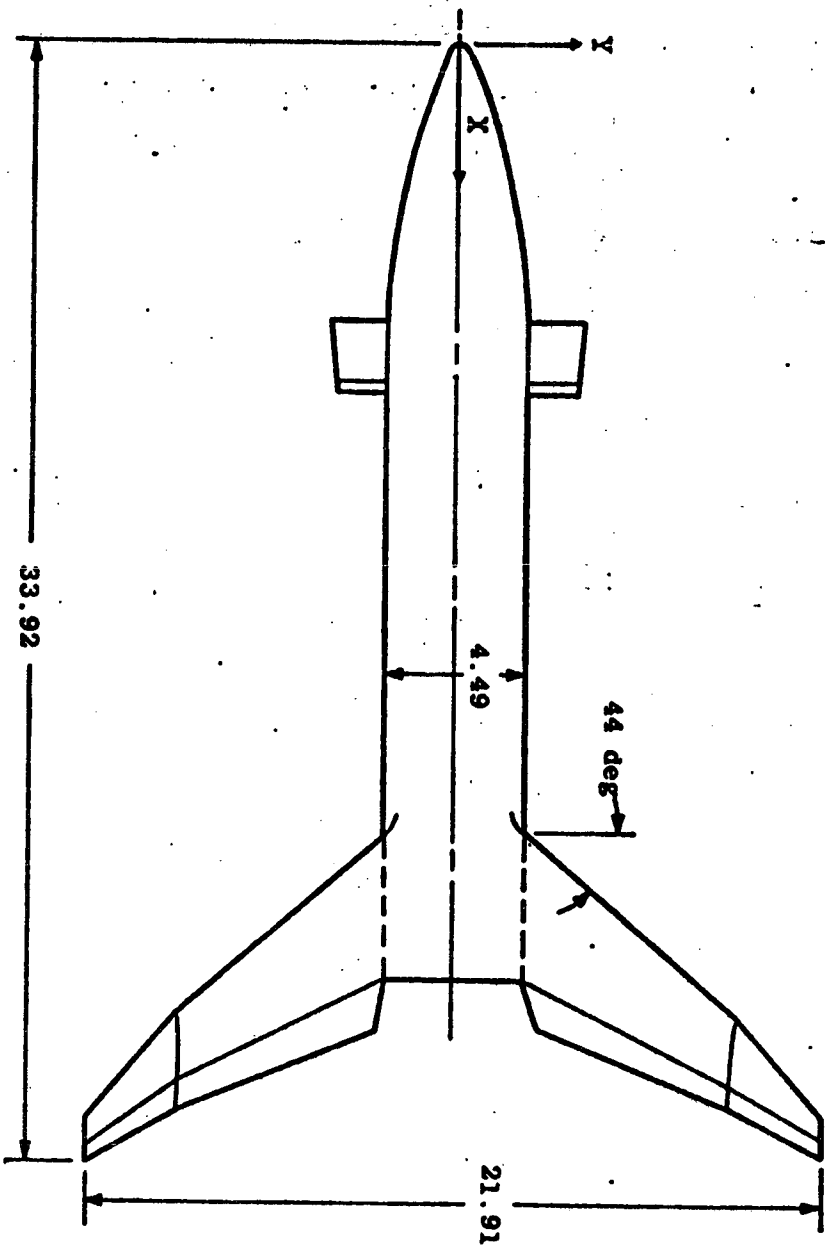
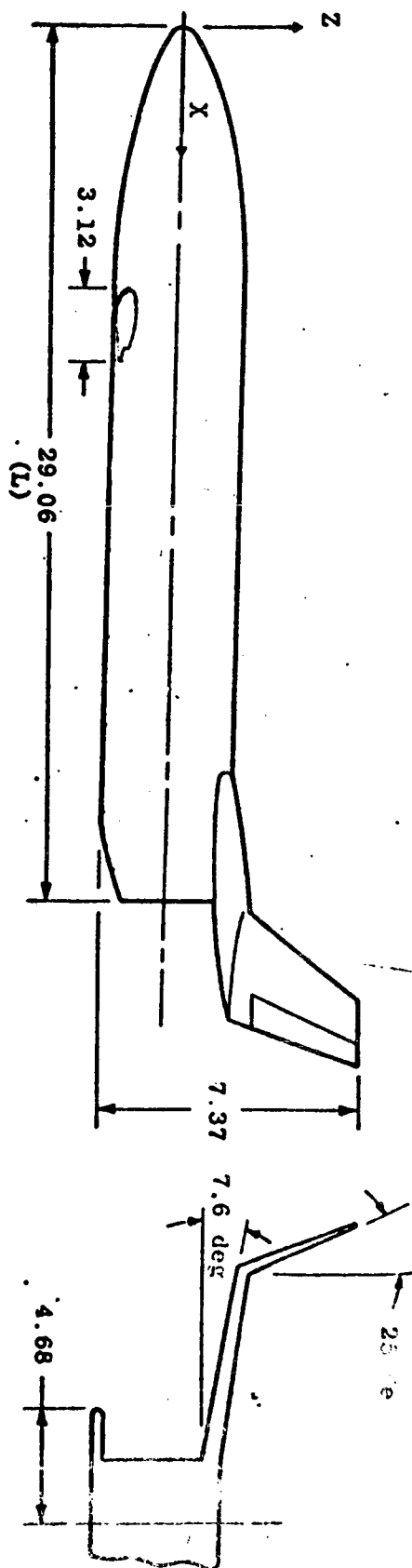


Fig. 2 McDonnell-Douglas Booster (MDAC-B)

All Dimensions in Inches
Model Scale 0.011

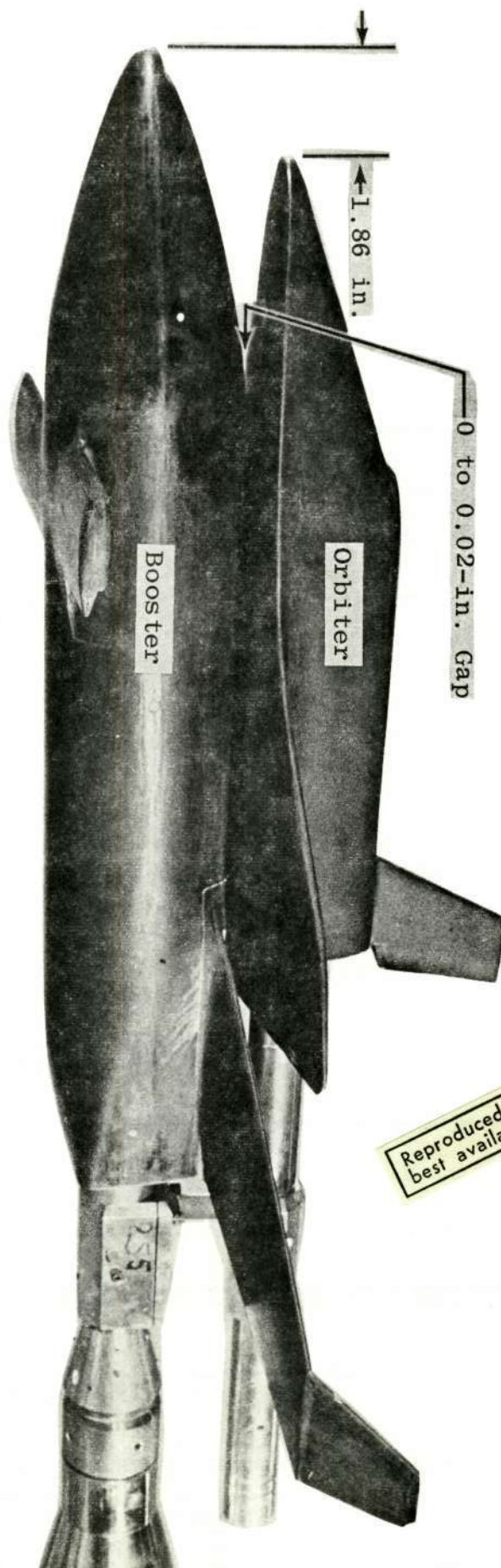


Fig. 3 Photograph of Mated Configurations

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Table 1

Configuration Description Details

MODEL COMPONENT: BODY - MDAC BoosterGENERAL DESCRIPTION: Configuration 256-17A booster; model scale 0.011DRAWING NUMBER: 256-17-0001, Rev. ADIMENSIONS:FULL-SCALEMODEL SCALE

Length (ft)

220.172.42

Max. Width (ft)

34.00.374

Max. Depth (ft)

34.00.374

Fineness Ratio

Area

Max. Cross-Sectional

Planform

Wetted

Base

MODEL COMPONENT: Wing - MDAC Booster

GENERAL DESCRIPTION: Configuration 17A Wing

Model Scale 0.011

DRAWING NUMBER: _____

DIMENSIONS:

FULL-SCALE

MODEL SCALE

TOTAL DATA

Area, ft ²		
Planform	6020.0	.729
Wetted		
Span (equivalent), ft.	146.0	1.606
Aspect Ratio	3.54	3.54
Rate of Taper		
Taper Ratio	.435	.435
Diehedral Angle, degrees	7.67	7.67
Incidence Angle, degrees	3.0	3.0
Aerodynamic Twist, degrees	0	0
Toe-In Angle		
Cant Angle		
Sweep Back Angles, degrees		
Leading Edge	44.0	44.0
Trailing Edge		
0.25 Element Line		
Chords:		
Root (Wing Sta. 0.0), inches	690.0	7.59
Tip, (equivalent)	300.0	3.30
MAC, inches	520.0	5.72
Fus. Sta. of .25 MAC		
W.P. of .25 MAC		
Airfoil Section		
Root	0010-64	0010-64
Tip	0010-64	0010-64

EXPOSED DATA

Area, ft ²	4190.0	.506
Span, (equivalent)		
Aspect Ratio		
Taper Ratio		
Chords		
Root, inches	594.0	6.54
Tip, inches	300.0	3.30
MAC		
Fus. Sta. of .25 MAC		
W.P. of .25 MAC		

MODEL COMPONENT: Elevon - MDAC Booster

GENERAL DESCRIPTION: Configuration 17A Elevons

Model Scale 0.011

DRAWING NUMBER: 256-17-0001, Rev. A

DIMENSIONS:

	<u>FULL-SCALE</u>	<u>MODEL SCALE</u>
Area	<u>617 ft²</u>	<u>.0745 ft²</u>
Span (equivalent)	<u>650 in.</u>	<u>7.15 in.</u>
Inb'd equivalent chord	<u>180 in.</u>	<u>1.98 in.</u>
Outb'd equivalent chord	<u>93 in.</u>	<u>1.02 in.</u>
Ratio Elevator chord/horizontal tail chord		
At Inb'd equiv. chord	<u>.3</u>	<u>.3</u>
At Outb'd equiv. chord	<u>.3</u>	<u>.3</u>
Sweep Back Angles, degrees		
Leading Edge	<u>33</u>	<u>33</u>
Tailing Edge	<u>27</u>	<u>27</u>
Hingeline	<u>33</u>	<u>33</u>
Area Moment (Normal to hinge line), ft ³	<u>2998</u>	<u></u>

MODEL COMPONENT: Vertical Tails - MDAC Booster

GENERAL DESCRIPTION: Configuration 17 Vertical Tails

Model Scale 0.011

DRAWING NUMBER: 256-17-0001, Rev. A

DIMENSIONS:

TOTAL DATA (Values for one)

Area
Planform (True)
(Side Projection)

Span (equivalent), inches

Aspect Ratio

Rate of Taper

Taper Ratio

Dihedral Angle, degrees

Incidence Angle, degrees

Aerodynamic Twist, degrees

Toe-In Angle

Cant Angle

Sweep Back Angles, degrees

Leading Edge

Trailing Edge

0.25 Element Line

Chords:

Root (Wing Sta. 0.0)

Tip, (equivalent), inches

MAC, inches

Fus. Sta. of .25 MAC

W.P. of .25 MAC

Airfoil Section

Root

Tip

FULL-SCALE

MODEL SCALE

438

397

276

1.21

.520

0

25

40

300

156

236

NACA

NACA

64A-009

64A-009

NACA

NACA

64A-009

64A-009

.0523

.0478

3.03

1.21

.520

0

25

40

3.30

1.71

2.59

EXPOSED DATA

Area

Span, (equivalent)

Aspect Ratio

Taper Ratio

Chords

Root

Tip

MAC

Fus. Sta. of .25 MAC

W.P. of .25 MAC

MODEL COMPONENT: Canard - MDAC Booster

GENERAL DESCRIPTION: Configuration 17A Canard

Model Scale 0.011

DRAWING NUMBER: 256-17-001, Rev. A

DIMENSIONS:

	<u>FULL-SCALE</u>	<u>MODEL SCALE</u>
Theo. Area, ft ²	<u>1660</u>	<u>.200</u>
Exp Area, ft ²	<u>1215</u>	<u>.146</u>
Aspect Ratio	<u>3.0</u>	<u>3.0</u>
Chord (Incl. Flap), ft	<u>23.625</u>	<u>.260</u>
Airfoil (360 In. Theo Chord)	NACA <u>63-018</u>	NACA <u>63-018</u>

Table 1

Configuration Description Details

MODEL COMPONENT: BODY - MDAC OrbiterGENERAL DESCRIPTION: Basic fuselage contours including canopy.

Model scale: 0.011

DRAWING NUMBER: 255 BJ 00050, Rev. B

<u>DIMENSIONS:</u>	<u>FULL-SCALE</u>	<u>MODEL SCALE</u>
Length (ft.)	<u>156.4</u>	<u>1.720</u>
Max. Width	<u>27.1</u>	<u>.298</u>
Max. Depth	<u>30.3</u>	<u>.333</u>
Finess Ratio	<u> </u>	<u> </u>
Area (ft. ²)	<u> </u>	<u> </u>
Max. Cross-Sectional	<u>627.4</u>	<u>.0759</u>
Planform	<u>3790.0</u>	<u>.459</u>
Wetted	<u>12520.0</u>	<u>1.515</u>
Base	<u>447.0</u>	<u>.0541</u>

Note: All units are ft. or sq. ft.
 These data include both sides of the vehicle.

MODEL COMPONENT: Elevon - MDAC OrbiterGENERAL DESCRIPTION: Model Scale: 0.011DRAWING NUMBER: 255 BJ 00050, Rev. BDIMENSIONS:

	<u>FULL-SCALE</u>	<u>MODEL SCALE</u>
Area, ft ²	<u>963.</u>	<u>.117</u>
Span (equivalent), ft.	<u>73.7</u>	<u>.811</u>
Inb'd equivalent chord, ft.	<u>12.8</u>	<u>.141</u>
Outb'd equivalent chord, ft.	<u>12.8</u>	<u>.141</u>
Ratio Elevator chord/horizontal tail chord		
At Inb'd equiv. chord		
At Outb'd equiv. chord		
Sweep Back Angles, degrees		
Leading Edge	<u>0.0</u>	<u>0.0</u>
Tailing Edge	<u>0.0</u>	<u>0.0</u>
Hingeline	<u>0.0</u>	<u>0.0</u>
Area Moment (Normal to hinge line)		

Note: All units are ft., sq. ft., or degrees.
These data include both sides of vehicle.

Table 1 - continued

MODEL COMPONENT: Body Flap - MDAC Orbiter

GENERAL DESCRIPTION: Model Scale: 0.011

DRAWING NUMBER: 255 BJ 00050, Rev. B

DIMENSIONS:

	<u>FULL-SCALE</u>	<u>MODEL SCALE</u>
Area, ft ²	<u>140.88</u>	<u>.0170</u>
Span (equivalent), ft.	<u>23.81</u>	<u>.262</u>
Inb'd equivalent chord, ft.	<u>5.333</u>	<u>.0587</u>
Outb'd equivalent chord, ft.	<u>12.80</u>	<u>.141</u>
Ratio Elevator chord/horizontal tail chord		
At Inb'd equiv. chord		
At Outb'd equiv. chord		
Sweep Back Angles, degrees		
Leading Edge	<u>0.0</u>	<u>0.0</u>
Tailing Edge	<u>0.0</u>	<u>0.0</u>
Hingeline	<u>0.0</u>	<u>0.0</u>
Area Moment (Normal to hinge line)		

Note: All dimensions in ft., sq. ft., or degrees.
These data include both sides of vehicle.

MODEL COMPONENT: Wing - MDAC Orbiter

GENERAL DESCRIPTION: Model Scale: 0.011

DRAWING NUMBER: 255 BJ 00050, Rev. B

DIMENSIONS:

FULL-SCALE

MODEL SCALE

TOTAL DATA

Area, ft ²		
Planform	5330.	.645
Wetted		
Span (equivalent), ft.	97.5	1.073
Aspect Ratio	1.68	1.68
Rate of Taper		
Taper Ratio	0.230	.230
Dihedral Angle, degrees	10.0	10.0
Incidence Angle, degrees	2.0	2.0
Aerodynamic Twist, degrees	0	0
Toe-In Angle	0	0
Cant Angle	0	0
Sweep Back Angles, degrees		
Leading Edge	55.0	55.0
Trailing Edge	0	0
0.25 Element Line	47.0	47.0
Chords: (ft.)		
Root (Wing Sta. 0.0)	90.43	.995
Tip, (equivalent)	20.80	.229
MAC	63.30	.696
Fus. Sta. of .25 MAC		
W.P. of .25 MAC		
Airfoil Section		
Root	0010-64	0010-64
Tip	0012-64	0012-64

EXPOSED DATA

Area, ft ²	3147.3	.381
Span, (equivalent), ft.	70.5	.776
Aspect Ratio	1.47	1.47
Taper Ratio		
Chords (ft.)		
Root	71.25	.784
Tip	20.80	.229
MAC	52.20	.574
Fus. Sta. of .25 MAC		
W.P. of .25 MAC		

Note: All units are ft., sq. ft. or degrees.

Table 1 - continued

MODEL COMPONENT: Rudder - MDAC Delta Wing Orbiter

GENERAL DESCRIPTION: Model Scale: 0.011

DRAWING NUMBER: 255 BJ 00050, Rev. B

DIMENSIONS:

	<u>FULL-SCALE</u>	<u>MODEL SCALE</u>
Area, ft. ²	<u>.213.9</u>	<u>.0259</u>
Span (equivalent), ft.	<u>27.5</u>	<u>.303</u>
Inb'd equivalent chord, ft.	<u>9.50</u>	<u>.105</u>
Outb'd equivalent chord, ft.	<u>6.10</u>	<u>.0671</u>
Ratio Elevator chord/horizontal tail chord		
At Inb'd equiv. chord	<u>.369</u>	<u>.369</u>
At Outb'd equiv. chord	<u>.369</u>	<u>.369</u>
Sweep Back Angles, degrees		
Leading Edge	<u>30.0</u>	<u>30.0</u>
Tailing Edge	<u>13.38</u>	<u>13.38</u>
Hingeline	<u>19.95</u>	<u>19.95</u>
Area Moment (Normal to hinge line)		

Note: All units are ft., sq. ft., or degrees.

MODEL COMPONENT: Vertical Tail - MDAC Orbiter

GENERAL DESCRIPTION: Model Scale: 0.011

DRAWING NUMBER: 255 BJ 00050, Rev. B

DIMENSIONS:

TOTAL DATA

Area, ft.²
Planform
Wetted
Span (equivalent), ft.
Aspect Ratio
Rate of Taper
Taper Ratio
Dihedral Angle, degrees
Incidence Angle, degrees
Aerodynamic Twist, degrees
Toe-In Angle
Cant Angle
Sweep Back Angles, degrees
Leading Edge
Trailing Edge
0.25 Element Line
Chords: (ft.)
Root (Wing Sta. 0.0)
Tip, (equivalent)
MAC
Fus. Sta. of .25 MAC
W.P. of .25 MAC
Airfoil Section
Root
Tip

FULL-SCALE

MODEL SCALE

580.0	.702
27.5	.303
1.30	1.30
.638	.638
0	0
0	0
0	0
0	0
0	0
30.0	30.0
13.4	13.4
26.2	26.2
25.75	.283
16.42	.181
21.43	.236
0009-64	0009-64
0009-64	0009-64

EXPOSED DATA

Area, ft.²
Span, (equivalent), ft.
Aspect Ratio
Taper Ratio
Chords (ft.)
Root
Tip
MAC
Fus. Sta. of .25 MAC
W.P. of .25 MAC

580	.702
27.5	.303
1.30	1.30
.638	.638
25.75	.283
16.42	.181
21.43	.236

Table 2

AECC (ARO, INC.) ARNOLD AFS, TENNESSEE
 VON KARMAN GAS DYNAMICS FACILITY
 50 INCH HYPERSONIC TUNNEL B

Y11162 B00

MODEL GEOMETRY OF MDAC-8 SIDE SURFACE - ALL DIMENSIONS IN INCHES - 27 JAN 72

STA NO. POINT NO.	X	Y	Z	X	Y	Z	X	Y	Z	X	Y	Z	X	Y	Z	X	Y	Z
1	0	0	0															
1	0	0	0															
2	.12																	
2	.04	-.20	0	-.20	.15	-.12	.21	0	.21	.01	.16	.16	.06	.20	0	.21		
3	.24																	
10	0	-.22	.10	-.27	.23	-.15	.29	0	.29	.01	.24	.17	.15	.23	0	.27		
4	.37																	
10	0	-.35	.13	-.31	.29	-.17	.37	0	.35	.01	.32	.15	.16	.28	0	.32		
5	.49																	
26	0	-.46	.06	-.40	.22	-.35	.37	-.18	.44	0	.44	.01	.40	.17	.24	.32		
0	.35																	
6	.61																	
35	0	-.49	.27	-.40	.44	-.17	.49	0	.49	.01	.45	.18	.38	.29	.23	.37		
0	.12	.30	0	.39														
7	.73																	
49	0	-.55	.20	-.50	.37	-.43	.49	-.24	.55	0	.55	.01	.51	.22	.39	.39		
0	.33	.48	.18	.48	.05	.51	0	.53										
8	.86																	
57	0	-.60	.16	-.57	.37	-.48	.55	-.24	.61	0	.62	.01	.59	.20	.50	.37		
0	.45	.42	.40	.50	.32	.59	.17	.60	0	.60								
9	.98																	
70	0	-.67	.22	-.60	.46	-.45	.61	-.24	.66	0	.66	.01	.64	.22	.54	.38		
0	.49	.46	.44	.53	.33	.60	.23	.64	.11	.65	0	.65						
10	1.22																	
84	0	-.73	.20	-.71	.48	-.57	.66	-.35	.76	0	.76	.01	.70	.31	.57	.51		
0	.45	.65	.27	.72	0	.76												
11	1.83																	
95	0	-.95	.28	-.92	.64	-.72	.89	-.38	.97	0	.97	.01	.93	.29	.79	.59		
0	.61	.82	.31	.93	0	.95												
12	2.44																	
106	0	-1.14	.34	-1.10	.75	-.88	1.10	-.38	1.16	0	1.16	.01	1.11	.38	.94	.72		
0	.77	.97	.46	1.12	.28	1.15	0	1.15										
13	3.06																	
119	0	-1.31	.33	-1.27	.87	-.99	1.23	-.50	1.34	0	1.34	.01	1.25	.49	1.05	.88		
0	.82	1.20	.60	1.30	.31	1.33	0	1.33										

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AEDCTARO, INC.) ARNOLD AFS, TENNESSEE
VON KARMAN GAS DYNAMICS FACILITY
50 INCH HYPERSONIC TUNNEL B
V11162 B00

MODEL GEOMETRY OF MDAC-B SIDE SURFACE - ALL DIMENSIONS IN INCHES - 27 JAN 72

STA NO.	X	Y	Z	X	Y	Z	X	Y	Z	X	Y	Z	X	Y	Z	X	Y	Z
POINT NO.	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
24	12.47	0	-2.15	.32	-2.13	.72	-2.04	1.03	-1.97	1.38	-1.96	1.59	-1.94	1.60	-1.93	1.55	-1.86	0
331	1.52	-1.01	1.50	-1.76	1.52	-1.67	1.58	-1.55	1.80	-1.25	1.99	-1.90	2.14	-1.44	2.20	1.58	0	0
	2.20	.01	2.18	.37	2.03	.88	1.78	1.34	1.63	1.61	1.45	1.91	1.32	2.07	1.19	2.15	0	0
	.91	2.21																
25	12.83	.13	-2.15	0	-2.15	.55	-2.09	.98	-1.94	1.41	-1.89	1.26	-1.89	1.42	-1.80	1.44	-1.70	0
356	1.53	-1.56	1.85	-1.14	2.11	-.69	2.20	0	2.20	.01	2.18	.40	2.02	.90	1.78	1.36	0	0
	1.54	1.15	1.41	1.97	1.32	2.07	1.19	2.15	1.03	2.20	.81	2.21						
26	13.44	0	-2.14	.20	-2.13	.44	-2.11	.66	-1.97	1.16	-1.82	1.25	-1.81	1.37	-1.70	1.50	-1.54	0
378	1.75	-1.26	2.00	-.83	2.14	-.38	2.20	0	2.20	.01	2.18	.38	1.94	1.94	1.65	1.58	0	0
	1.50	1.82	1.38	2.02	1.28	2.09	1.17	2.16	1.03	2.20	.43	2.21						
27	15.89	0	-2.15	.35	-2.11	1.01	-1.89	1.53	-1.53	1.91	-1.03	2.15	-.39	2.20	0	2.20	.01	0
400	2.16	.40	1.97	1.00	1.72	1.43	1.55	1.74	1.39	1.98	1.26	2.11	1.08	2.20	.89	2.21	0	0
28	18.33	0	-2.15	0	-2.14	.28	-2.11	.45	-2.10	.72	-2.02	.79	-2.00	1.23	-1.76	1.31	-1.74	0
416	1.81	-1.20	1.85	-1.16	2.13	-.53	2.15	-.44	2.21	0	2.20	.01	2.20	.01	2.21	.01	0	0
	2.18	.40	2.15	.50	2.09	.72	1.99	.95	1.86	1.23	1.72	1.44	1.74	1.45	1.56	1.71	0	0
	1.52	1.80	1.41	1.96	1.37	2.02	1.32	2.08	1.23	2.14	1.16	2.16	1.08	2.20	.83	2.21	0	0
	.88	2.21																
29	18.94	0	-2.18	.40	-2.13	1.00	-1.92	1.52	-1.56	1.94	-1.00	2.15	-.48	2.21	0	2.21	.01	0
449	2.19	.35	2.05	.83	1.93	1.23	1.85	1.43	1.75	1.67	1.63	1.80	1.50	1.91	1.37	2.03	0	0
	1.21	2.14	.97	2.20														
30	19.56	0	-2.16	.33	-2.14	.81	-2.00	1.38	-1.67	1.75	-1.28	2.14	-.51	2.21	0	2.21	.01	0
467	2.19	.35	2.11	.75	2.05	1.03	2.03	1.38	1.22	2.00	1.37	1.98	1.51	1.97	1.71	1.93	1.83	0
	1.86	1.93	1.70	1.99	1.47	2.03	1.30	2.09	1.10	2.19	.83	2.21						
31	20.78	0	-2.15	.32	-2.13	.75	-2.02	1.20	-1.80	1.65	-1.42	1.91	-1.06	2.13	-.53	2.21	.01	0
489	2.21	.01	2.20	.29	2.18	.64	2.14	1.05	2.13	1.38	2.13	1.50	2.16	1.63	2.25	1.74	0	0
	2.46	1.81	2.71	1.89	2.91	1.97	3.01	1.99	2.99	2.00	2.99	2.02	2.88	2.14	2.40	2.19	0	0
32	23.22	0	-2.14	.53	-2.08	.94	-1.96	1.39	-1.78	1.70	-1.60	1.91	-1.42	2.05	-1.21	2.15	-.94	0
513	2.20	-.49	2.21	0	2.21	.01	2.21	.51	2.21	.88	2.21	1.31	2.21	1.42	2.25	1.53	0	0
	2.33	1.55	3.02	1.63	3.75	1.74	4.40	1.87	4.97	2.00	5.34	2.13	5.48	2.20	5.54	2.22	0	0
	5.50	2.30	5.29	2.35	4.91	2.37												

AEDC(ARO, INC.) ARNOLD AFS, TENNESSEE
 VON KARMAN GAS DYNAMICS FACILITY
 50 INCH HYPERSONIC TUNNEL B
 Y11162 B00

MODEL GEOMETRY OF MDAC-8 SIDE SURFACE - ALL DIMENSIONS IN INCHES - 27 JAN 72

SID NO.	X	Y	Z	X	Y	Z	X	Y	Z	X	Y	Z	X	Y	Z	X	Y	Z
POINT NO.	Y	Z	Y	Z	Y	Z	Y	Z	Y	Z	Y	Z	Y	Z	Y	Z	Y	Z
33	28.11	0	-1.75	.64	-1.72	1.30	-1.67	1.72	-1.63	1.93	-1.55	2.07	-1.44	2.14	-1.31	2.19	-1.17	2.17
540	2.19	-0.93	2.20	2.20	2.29	1.66	3.10	1.70	4.03	1.76	5.78	1.91	6.97	2.08	7.65	2.25	1.30	2.20
	2.24	1.60	2.29	1.66	2.46	7.92	2.48	7.72	2.49	7.46	2.51	7.15	2.51	7.65	2.24	7.99	2.32	2.32
	8.04	2.42	0.03	2.46	7.92	2.48	7.72	2.49	7.46	2.51	7.15	2.51	7.65	2.24	7.99	2.32	2.32	2.32
34	28.97	0	-1.61	.92	-1.59	1.69	-1.58	1.92	-1.55	2.13	-1.39	2.18	-1.19	2.19	-1.03	2.19	-0.60	2.19
570	2.20	0	2.20	.01	2.21	2.21	1.50	2.22	1.11	2.22	1.33	2.20	1.50	2.21	1.67	2.22	1.72	2.22
	2.81	1.75	1.82	1.82	5.40	1.89	6.61	1.89	7.69	2.14	8.38	2.27	8.69	2.40	8.69	2.40	8.69	2.40
	8.92	2.54	8.85	2.54	8.67	2.55	8.20	2.57	7.69	2.14	8.38	2.27	8.69	2.40	8.69	2.40	8.69	2.40
35	29.58	2.29	1.85	4.36	1.87	6.03	1.96	7.59	2.09	8.75	2.27	9.33	2.41	9.48	2.47	9.55	2.50	2.50
596	9.53	2.66	4.36	1.87	6.03	1.96	7.59	2.09	8.75	2.27	9.33	2.41	9.48	2.47	9.55	2.50	2.50	2.50
36	30.56	5.23	1.98	6.49	2.03	8.18	2.15	9.24	2.26	9.41	2.29	9.51	2.32	9.59	2.38	9.69	2.57	2.57
607	9.85	2.90	10.00	3.26	10.07	3.44	10.08	3.56	9.41	2.29	9.51	2.32	9.59	2.38	9.69	2.57	2.57	2.57
37	31.78	7.58	2.15	8.41	2.19	9.25	2.25	9.39	2.26	9.52	2.30	9.62	2.42	9.75	2.68	10.02	3.15	3.15
619	10.28	3.62	10.52	4.12	10.71	4.57	10.73	4.68	10.74	4.75	9.62	2.42	9.75	2.68	10.02	3.15	3.15	3.15
38	32.08	8.14	2.20	8.64	2.22	9.15	2.25	9.36	2.26	9.52	2.31	9.61	2.43	9.81	2.80	10.13	3.36	3.36
632	10.39	3.84	10.68	4.42	10.84	4.83	10.89	4.95	10.90	5.04	9.61	2.43	9.81	2.80	10.13	3.36	3.36	3.36
39	32.69	9.44	2.33	9.53	2.40	9.62	2.53	9.95	3.10	10.27	3.67	10.62	4.31	10.89	4.83	10.95	4.93	4.93
645	10.95	4.99	9.53	2.40	9.62	2.53	9.95	3.10	10.27	3.67	10.62	4.31	10.89	4.83	10.95	4.93	4.93	4.93
40	33.00	9.84	2.95	10.08	3.36	10.35	3.85	10.61	4.31	10.63	4.73	10.85	4.94	10.85	4.94	10.85	4.94	4.94
654	9.84	2.95	10.08	3.36	10.35	3.85	10.61	4.31	10.63	4.73	10.85	4.94	10.85	4.94	10.85	4.94	4.94	4.94
41	33.37	10.34	3.86	10.57	4.28	10.78	4.64	10.88	4.84	10.93	4.94	10.93	4.94	10.93	4.94	10.93	4.94	4.94
660	10.34	3.86	10.57	4.28	10.78	4.64	10.88	4.84	10.93	4.94	10.93	4.94	10.93	4.94	10.93	4.94	4.94	4.94
42	33.73	10.90	4.95	10.90	4.95	10.90	4.95	10.90	4.95	10.90	4.95	10.90	4.95	10.90	4.95	10.90	4.95	4.95
665	10.90	4.95	10.90	4.95	10.90	4.95	10.90	4.95	10.90	4.95	10.90	4.95	10.90	4.95	10.90	4.95	4.95	4.95

AECTAARON, INC. ARNOLD AFB, TENNESSEE
 VON KARMAN GAS DYNAMICS FACILITY
 50 INCH HYPERSONIC TUNNEL B
 VT1162 800

MODEL GEOMETRY OF WDC-DRO BOTTOM SURFACE - DIMENSIONS IN INCHES - 27 JAN 72

STATION	Y	Z	Y	Z	Y	Z	Y	Z	Y	Z	Y	Z	Y	Z
POINT NO.														
1	.30	-.18	-.29	-.21	-.20	-.23	-.30	-.24	0	-.24	.10	-.23	.20	-.28
2	.35	-.11												
3	.40													
4	.30	-.19	-.29	-.23	-.19	-.25	-.30	-.26	0	-.26	.09	-.25	.19	-.23
5	.40	-.13												
6	.50													
7	.40	-.19	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
8	.30	-.21	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
9	.40	-.13												
10	.50													
11	.40	-.19	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
12	.30	-.21	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
13	.40	-.13												
14	.50													
15	.40	-.19	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
16	.30	-.21	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
17	.40	-.13												
18	.50													
19	.40	-.19	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
20	.30	-.21	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
21	.40	-.13												
22	.50													
23	.40	-.19	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
24	.30	-.21	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
25	.40	-.13												
26	.50													
27	.40	-.19	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
28	.30	-.21	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
29	.40	-.13												
30	.50													
31	.40	-.19	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
32	.30	-.21	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
33	.40	-.13												
34	.50													
35	.40	-.19	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
36	.30	-.21	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
37	.40	-.13												
38	.50													
39	.40	-.19	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
40	.30	-.21	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
41	.40	-.13												
42	.50													
43	.40	-.19	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
44	.30	-.21	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
45	.40	-.13												
46	.50													
47	.40	-.19	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
48	.30	-.21	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
49	.40	-.13												
50	.50													
51	.40	-.19	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
52	.30	-.21	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
53	.40	-.13												
54	.50													
55	.40	-.19	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
56	.30	-.21	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
57	.40	-.13												
58	.50													
59	.40	-.19	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
60	.30	-.21	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
61	.40	-.13												
62	.50													
63	.40	-.19	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
64	.30	-.21	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
65	.40	-.13												
66	.50													
67	.40	-.19	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
68	.30	-.21	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
69	.40	-.13												
70	.50													
71	.40	-.19	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
72	.30	-.21	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
73	.40	-.13												
74	.50													
75	.40	-.19	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
76	.30	-.21	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
77	.40	-.13												
78	.50													
79	.40	-.19	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
80	.30	-.21	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
81	.40	-.13												
82	.50													
83	.40	-.19	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
84	.30	-.21	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
85	.40	-.13												
86	.50													
87	.40	-.19	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
88	.30	-.21	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
89	.40	-.13												
90	.50													
91	.40	-.19	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
92	.30	-.21	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
93	.40	-.13												
94	.50													
95	.40	-.19	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
96	.30	-.21	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
97	.40	-.13												
98	.50													
99	.40	-.19	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23
100	.30	-.21	-.29	-.23	-.29	-.25	-.30	-.27	0	-.27	.10	-.27	.19	-.23

MODEL GEOMETRY OF W04C-0100 BOTTOM SURFACE - DIMENSIONS IN INCHES - 27 JAN 72

25

AECUTANO INC. ANNULD AFS. TENNESSEE
 VON KARMAN GAS DYNAMICS FACILITY
 50 INCH HYPERSONIC TUNNEL B
 VILLAGE 800

MODEL GEOMETRY OF PDAC-DNO BOTTOM SURFACE - DIMENSIONS IN INCHES - 27 JAN 72

STA NO.	X	Y	Z	X	Y	Z	X	Y	Z	X	Y	Z	X	Y	Z	X	Y	Z
POINT NO.	X	Y	Z	X	Y	Z	X	Y	Z	X	Y	Z	X	Y	Z	X	Y	Z
32	20.00	.10	-6.12	.10	-6.00	.10	-5.50	.01	-5.00	-.06	-6.00	-.14	-4.00	-.22	-3.50	-.30	-.30	-.30
524	-1.00	-.31	-2.07	-.03	-2.00	-.53	-1.25	-.60	-1.25	-.61	-1.00	-.61	-.50	-.61	0	-.50	-.50	-.50
	.50	-.60	1.07	-.62	1.25	-.62	1.50	-.61	2.00	-.54	2.50	-.45	3.00	-.37	3.50	-.30	-.30	-.30
	4.00	-.23	4.50	-.13	5.00	-.05	5.50	.02	6.00	.11	6.12	.17	6.20	.10				
33	21.00	.22	-6.00	.10	-5.50	.11	-5.00	.06	-4.50	-.02	-4.00	-.10	-3.50	-.17	-3.00	-.25	-.25	-.25
535	-6.25	-.32	-2.07	-.03	-1.50	-.48	-1.25	-.51	-1.00	-.53	-.50	-.53	0	-.53	-.50	-.50	-.50	-.50
	1.00	-.53	1.25	-.53	1.50	-.49	2.00	-.41	2.50	-.33	3.00	-.26	3.50	-.10	4.00	-.10	-.10	-.10
	4.50	-.02	5.00	.04	5.50	.12	6.00	.10	6.25	.22								
34	21.25	.22	-5.50	.10	-5.00	.07	-4.50	0	-3.99	-.07	-3.50	-.10	-3.00	-.21	-2.50	-.29	-.29	-.29
564	-6.00	-.36	-1.50	-.44	-1.25	-.47	-1.00	-.49	-.50	-.49	0	-.49	-.50	-.50	0	-.50	-.50	-.50
	1.25	-.48	1.50	-.45	2.00	-.38	2.50	-.30	3.00	-.23	3.50	-.15	4.00	-.07	4.50	-.05	-.05	-.05
	5.00	.07	5.50	.13	6.00	.22												

06/02/18

72

27

WILLIAM

9

28

MODEL GROWTH OF PUAU-UU - SIDE SURFACE - ALL DIMENSIONS IN INCHES - 27 JAN 72

[illegible]

MODEL GROMT 147 OF PUAC-11100 - SILE SLFACE - ALL DIMENSIONS IN INCHES - 27 JAN 72

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MODEL GEOMETRY OF MUAC-COU TOP SURFACE - ALL DIMENSIONS IN INCHES - 27 JAN 72

STATION NO.	POINT NO.
1	1
2	2
3	3
4	4
5	5
6	6
7	7
8	8
9	9
10	10
11	11
12	12
13	13
14	14
15	15
16	16
17	17
18	18
19	19
20	20
21	21
22	22
23	23
24	24
25	25
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30	30
31	31
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68	68
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73	73
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78	78
79	79
80	80
81	81
82	82
83	83
84	84
85	85
86	86
87	87
88	88
89	89
90	90
91	91
92	92
93	93
94	94
95	95
96	96
97	97
98	98
99	99
100	100

[illegible]

2	0.10	0	0.21	0.15	0.16	0.20	0.09	0.23	0
2	-0.14	0	-0.13	0.11	-0.09	0.16	0	0.21	0.15

[illegible][illegible][illegible][illegible][illegible][illegible]

Variable	Mean	SD	Min	Max	Skewness	Kurtosis	Shapiro-Wilk	Normality
Age	45.23	9.47	34	51	2.21	6.60	.15	.63
Gender	0.55	0.50	0	1	0.09	0.67	0	.68
Marital Status	0.47	0.50	0	1	0.09	0.67	0	.68
Education	12.34	2.34	9	15	0.00	0.00	0.00	1.00
Income	15.67	5.67	10	20	0.00	0.00	0.00	1.00
Health	1.23	0.47	1	2	0.00	0.00	0.00	1.00
Stress	3.45	1.23	1	5	0.00	0.00	0.00	1.00
Depression	2.12	0.89	1	4	0.00	0.00	0.00	1.00
Life Satisfaction	4.56	1.56	1	7	0.00	0.00	0.00	1.00

6.3	1.30	-0.12	-0.67	-0.04	-0.03	0.06	-0.53	-0.23	-0.41	0.34	-0.26	0.52	-0.16	0.60	0	0.12
6.3	1.30	-0.12	-0.67	-0.04	-0.03	0.06	-0.53	-0.23	-0.41	0.34	-0.26	0.52	-0.16	0.60	0	0.12

[illegible][illegible][illegible]

11	3.00	-1.15	-1.08	0	-1.06	0.3	-0.55	0.25	-0.85	0.45	-0.71	0.68	-0.58	0.85	-0.47	0.9
17	-1.12	-1.15	-1.08	0	-1.06	0.3	-0.55	0.25	-0.85	0.45	-0.71	0.68	-0.58	0.85	-0.47	0.9

	0	1	2	3	4	5	6	7	8	9
-0.2	1.01	0.19	1.01	0.15	0	0.05	0.16	0.15		
-0.4	0.67	1.09	0.15	1.12	0	0	0.16	0.15		

[illegible]

MOUL. DEFINITELY OF WUAC-UNU TOP SURFACE - ALL DIMENSIONS IN INCHES - 27 JAN 72

32

AECI/AMU(ING.) ARNOLD AFS, TENNESSEE
 WIND TUNNEL GAS DYNAMICS FACILITY
 50 INCH HYPERSONIC TUNNEL 4
 WILCOX H00

MULTI GEOMETRY OF WING-UPPER TOP SURFACE - ALL DIMENSIONS IN INCHES - 27 JAN 72

SIA NO.	X	Y	Z	X	Y	Z	X	Y	Z	X	Y	Z	X	Y	Z	X	Y	Z	X	Y	Z
POINT NO.																					
21	9.00	-6.02	-1.97	-1.15	-1.04	-0.08	-1.74	.06	-1.64	.24	-1.60	.40	-1.52	.64	-1.44	.94					
371	-1.33	1.35	-1.25	1.67	-1.13	1.72	-1.07	2.29	-.83	2.74	-2.95	-1.44	3.10	-1.17	3.21	.63					
0	3.22	.26	3.19	.54	3.04	.24	2.76	1.11	2.35	1.28	1.77	1.41	1.26	1.50	.83						
22	1.03	1.41	1.77	.14	1.83	-.03	2.02	-1.15	-2.04	-.21											
400	11.00	-6.13	-2.10	-1.15	-1.05	0	-1.83	.13	-1.74	.25	-1.63	.44	-1.54	.66	-1.44	1.03					
	-1.30	1.33	-1.24	1.66	-1.11	2.34	-.56	2.71	-.72	2.99	-1.48	3.14	-.22	3.22	.66	3.24					
	.30	3.21	.70	3.04	.24	2.62	1.04	2.52	1.19	2.23	1.31	1.74	1.40	1.37	1.48	1.03					
	1.26	.47	1.04	.60	1.04	.10	1.59	0	2.09	-.04	2.16	-.19									
23	11.00	-6.09	-2.00	-.04	-2.00	0	-1.95	.13	-1.78	.29	-1.66	.44	-1.57	.61	-1.51	.79					
430	-1.44	1.05	-1.35	1.43	-1.24	1.81	-1.13	2.32	-1.00	2.05	-1.37	2.95	-.50	3.13	-.25	3.22					
	0	3.22	.39	3.20	.74	3.04	1.61	2.69	1.18	2.24	1.31	1.74	1.40	1.33	1.46	1.08					
	1.22	.43	1.41	.59	1.04	.02	1.55	.23	2.02	.10	2.19	-.01	2.28	-.08	2.30	-.17					
24	12.00	-6.02	-2.51	-.06	-2.46	0	-2.35	.04	-2.21	.11	-2.04	.16	-1.89	.27	-1.77	.37					
462	-1.06	.53	-1.04	.71	-1.04	1.01	-1.27	1.34	-1.29	1.10	-1.21	2.03	-1.11	2.38	-1.00	2.65					
	1.22	2.04	1.22	1.63	1.22	1.22	1.44	.92	1.55	.73	1.63	.56	1.76	.40	1.94	.25					
	2.13	.10	2.32	.09	2.44	.04	2.51	-.01	2.53	-.07											
25	13.00	-6.05	-2.91	.05	-2.71	.11	-2.61	.14	-2.41	.18	-2.26	.21	-2.10	.24	-1.92	.30					
498	-1.03	.46	-1.12	.44	-1.03	.53	-1.44	.65	-1.42	1.15	-1.29	1.68	-1.20	2.08	-1.07	2.50					
	1.22	2.77	1.22	1.63	1.22	1.22	1.44	.92	1.55	.73	1.63	.56	1.76	.40	1.94	.25					
	2.13	.10	2.32	.09	2.44	.04	2.51	-.01	2.53	-.07											
26	14.00	-6.05	-3.24	.14	-3.12	.23	-2.95	.27	-2.82	.26	-2.64	.29	-2.57	.30	-2.49	.32					
537	-1.06	.46	-1.12	.44	-1.03	.53	-1.44	.65	-1.42	1.15	-1.29	1.68	-1.20	2.08	-1.07	2.50					
	1.22	2.77	1.22	1.63	1.22	1.22	1.44	.92	1.55	.73	1.63	.56	1.76	.40	1.94	.25					
	2.13	.10	2.32	.09	2.44	.04	2.51	-.01	2.53	-.07											
27	15.00	-6.05	-3.24	.14	-3.12	.23	-2.95	.27	-2.82	.26	-2.64	.29	-2.57	.30	-2.49	.32					
574	-1.06	.46	-1.12	.44	-1.03	.53	-1.44	.65	-1.42	1.15	-1.29	1.68	-1.20	2.08	-1.07	2.50					
	1.22	2.77	1.22	1.63	1.22	1.22	1.44	.92	1.55	.73	1.63	.56	1.76	.40	1.94	.25					
	2.13	.10	2.32	.09	2.44	.04	2.51	-.01	2.53	-.07											

MODEL GEOMETRY OF MUAC-000 TOP SURFACE - ALL DIMENSIONS IN INCHES - 27 JAN 72

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ABU (AND) INC.) AMULI AFS, TENNESSEE
 VON KARMAN GAS DYNAMICS FACILITY
 50 INCH HYPERSONIC TUNNEL #
 VILLIARD HALL

MODEL GEOMETRY OF PHAC-DEU TOP SURFACE - ALL DIMENSIONS IN INCHES - 27 JAN 72

STA NO.	X	Y	Z	X	Y	Z	X	Y	Z	X	Y	Z	X	Y	Z	X	Y	Z	X	Y	Z
POINT NO.	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
34	20.24																				
920	-6.36	.42	-6.29	.44	-6.14	.51	-6.04	.51	-5.78	.47	-5.33	.40	-4.92	.33	-4.38	.25					
	-3.14	.14	-2.90	.0	-2.61	-.04	-1.62	-.19	-1.44	-.21	-1.38	-.18	-1.35	-.10	-1.33	.03					
	-1.24	.27	-1.20	.41	-1.07	1.44	-1.00	1.49	-.91	2.33	-.79	2.43	-.54	3.14	-.33	3.26					
	-.18	.31	-.13	3.35	-.12	5.01	-.12	4.34	-.12	3.63	-.12	3.40	-.11	5.73	-.09	6.34					
	-.05	6.42	-.03	6.43	.0	8.44	.05	6.44	.09	6.79	.12	3.38	.12	3.60	.13	4.03					
	.13	4.61	.13	5.22	.13	5.43	.13	6.36	.14	3.35	.12	3.32	.12	3.25	.13	3.09					
	.43	2.43	.43	2.34	.43	1.02	1.10	1.33	1.20	.73	1.27	.29	1.34	-.12	1.40	-.17					
	1.47	-.17	2.17	-.07	2.44	.03	4.07	.22	5.01	.37	5.54	.46	5.95	.50	6.12	.51					
	6.23	.44	6.28	.44	6.31	.38															
35	20.30																				
927	-2.44	.41	-2.39	.44	-2.31	.50	-2.12	.44	-1.82	.41	-1.73	.31	-1.18	.16	-1.09	.01					
	-2.61	-.13	-1.84	-.25	-1.34	-.25	-1.35	-.22	-1.32	-.07	-1.23	.42	-1.18	.77	-1.09	1.28					
	-.46	2.43	-.41	2.44	-.04	3.43	-.34	3.45	-.14	3.31	-.12	5.94	-.12	5.25	-.12	4.62					
	-.12	4.17	-.12	3.32	-.11	6.44	-.11	3.73	-.10	6.85	-.12	3.33	-.08	6.97	.0	7.04					
	.44	6.23	.10	3.35	.10	3.40	.11	4.02	.12	4.71	.12	5.56	.12	6.29	.12	6.16					
	.24	3.31	.43	3.21	.34	3.04	.77	2.40	.08	2.30	.97	1.40	1.06	1.29	1.16	.66					
	1.24	.15	1.24	-.13	1.33	-.14	1.42	-.22	1.44	-.14	2.77	-.02	3.81	.14	4.64	.27					
	5.40	.34	5.45	.45	6.11	.44	6.24	.44	6.32	.46	6.37	.39									
36	21.00																				
1042	-6.34	.34	-6.32	.44	-6.25	.44	-6.05	.41	-5.67	.35	-4.95	.24	-4.02	.09	-3.35	-.01					
	-2.44	-.13	-1.75	-.26	-1.24	-.31	-1.0	5.45	-.09	6.46	-.09	6.32	-.09	4.63	-.07	6.97					
	-.07	3.44	-.04	3.44	.0	7.02	.04	3.47	.04	3.54	.08	3.43	.08	6.97	.09	4.45					
	.44	5.45	.10	6.07	.10	6.43	1.35	-.24	1.45	-.20	3.15	-.01	4.29	.16	5.15	.30					
	2.44	.32	6.11	.44	6.27	.44	6.37	.39													
37	21.36																				
1045	-6.34	.34	-5.47	.32	-5.24	.23	-4.46	.10	-3.77	-.01	-3.05	-.12	-2.33	-.23	-1.74	-.32					
	-.37	-.04	6.73	-.04	5.34	-.04	6.94	-.06	4.21	-.03	3.54	-.03	6.98	.05	3.53	-.37					
	.46	3.47	.06	4.14	.07	4.01	.07	5.42	.07	6.43	.08	6.16	.08	6.73	1.28	-.37					
	1.34	-.24	2.71	-.17	3.33	-.08	4.34	.07	5.13	.20	5.45	.28									
38	21.50																				
1115	-6.34	.34	-6.34	.34	-6.34	.34	-6.34	.34	-6.34	.34	-6.34	.34	-6.34	.34	-6.34	.34					
	.42	3.41	.42	3.73	.42	4.00	.45	4.16	.45	5.43	.46	6.41	.47	6.74	.07	6.26					
39	21.64																				
1131	6.44																				

Table 3

PHASE CHANGE COATING TEST DATA SUMMARY SHEET

TEST TITLE: Ascent Heat Transfer Test of the MDAC Configurations

TEST NUMBER: VT1162-9

TEST FACILITY: VKF Tunnel B

TEST DATE: June 1971

TEST ENGINEER: R. K. Matthews & W. R. Martindale

Run No.	Model Configuration Identification	Model Scale	Free Stream Mach Number	Total Pressure (psia)	Total Temp. (°R)	T_{aw} / T_{total}	RNX10 ⁶ Fr	Phase Change Temp. (°F)	Model Position (degrees)			Model Surface
194	MDAC-B + DMO	0.011	8.0	150	1180	1.0	0.8	400	0	0	0	Side
195								250	0			
196								150	0			
201								113/400	0			
197								250	-5			
198								113/500	-5			
199								250/400	5			
200								113	5			
202		0.011	8.0	555	1310	1.0	2.5	300/500	0			
203								125/500	0			
208								200	0			
204								250/500	5			
205								150	5			

* T_{aw} = adiabatic wall temperature

+ Post-test photograph

PHASE CHANGE COATING TEST DATA SUMMARY SHEET

TEST TITLE: Ascent Heat Transfer Test of the MDAC Configurations

TEST NUMBER: VT1162-9 TEST FACILITY: VKF Tunnel 8

TEST DATE: June 1971 TEST ENGINEER: R. K. Matthews & W. R. Martindale

Run No.	Model Configuration Identification	Model Scale	Free Stream Mach Number	Total Pressure (psia)	Total Temp. (°R)	T_{aw}^* Total	RNX10 ⁶ Ft	Phase Change Temp. (°F)	Model Position (degrees)			Model Surface
									α	β	ϕ	
206	MDAC-B + DMO	0.011	8.0	555	1310	1.0	2.5	250/500	-5	0	0	Side
207		"	"	"	"	"	"	150	-5			
209		0.011	8.0	860	1340	1.0	3.7	300/500	0			
210		"	"	"	"	"	"	200	0			
222		0.011	8.0	555	1310	N/A	2.5	0 [†] Flow	0			Top/Side
221									-5			
220									5			
224									Shado	0	0	0
227									0	0	90	N/A
225									5		0	
226									-5			

* T_{aw} = adiabatic wall temperature

+ Post-test photograph

TABLE 4. SUMMARY DATA INDEX

CONFIGURATION	MODEL SURFACE	DATA PRESENTED	PAGES	REYNOLDS NUMBER $\times 10^6$ / FT			ANGLE OF ATTACK - DEGREES		
				0.8	2.5	3.7	-5	0	5
BOOSTER - ORB	SIDE	A	40 - 41	X				X	
			43 - 44	X				X	
			46 - 47	X				X	
			48	X				X	
			50 - 51	X				X	
			52	X				X	
			54 - 55	X			X		
			57 - 58	X			X		
			59	X			X		
			61 - 62	X					X
			64 - 65	X					X
			67 - 68	X					
			69		X			X	
			71 - 72		X			X	
BOOSTER - ORB	SIDE	A	73		X			X	
			75 - 76		X			X	
			78 - 79		X			X	
			81 - 82		X			X	
			84 - 85		X			X	
			86		X			X	
			88 - 89		X			X	
			91 - 92		X			X	
			93			X		X	
			95 - 96			X		X	
			98		X			X	
			99		X			X	
			101		X			X	
			102		X			X	
BOOSTER - ORB	SIDE	C	104		X				
			105		X				
			106		X				
			107		X				
			108		X				
			109		X				
							X		
								X	
								X	
								X	
								X	
								X	
								X	
								X	
BOOSTER - ORB	SIDE	B							

PRESENTED DATA SCHEDULE

A: PHASE - CHANGE PAINT PHOTOGRAPHS
 B: SHADOWGRAPH PHOTOGRAPHS
 C: OIL FLOW PHOTOGRAPHS

AEDEC (ARO, INC.) ARNOLD AFS, TENNESSEE
VON KARMAN GAS DYNAMICS FACILITY
50 INCH HYPERSONIC TUNNEL B
V11162

(DEC R) (P51A)	(P51A)	(F7/SEC)	(SUGS/F12)	(LB-SEC/F12)	(F7-1)	(R= .011FT)	(R= .011FT)
27.0	.016	.720	3670	1.570E-05	7.005E-08	8.17E 05	2.014E-02
							5.70E-02

SIZE (US)	AVERAGE IN	•000(SQUARE ROOT DEL TIME) + 0.11
400	76 (B)	
SIZE(LS)	AVERAGE IN =	
400	77 (C)	

AVERAGE TM = 76 (G)
AVERAGE TM = 77 (G)

0.000 (SQUARE ROOT OF TIME) • 0.11

Abbreviations of the 1000 Genomes project are explained in the supplementary

[illegible][illegible][illegible][illegible]

US 4485	(400)	31.24	30.20	0	9.79E-03	.3567	1.402E-02	.5374	1.903E-02	.7296	2.019E-02	84	75	118
US 4486	(400)	31.24	30.20	8	9.70E-03	.3564	1.403E-02	.5378	1.905E-02	.7341	2.021E-02	84	75	118

[illegible]

US 4712	(465)	43.24	42.24	0	6.01E-03	.2653	1.043E-02	.4093	1.416E-02	.5474	1.50E-02	09	75	133
US 4712	(460)	43.24	42.20	0	6.01E-03	.2653	1.043E-02	.4093	1.416E-02	.5474	1.50E-02	09	75	133
US 4712	(460)	43.24	42.20	0	6.01E-03	.2653	1.043E-02	.4093	1.416E-02	.5474	1.50E-02	09	75	133

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1. The first part of the document is a title page. It contains the title of the report, the author's name, and the date of the report. The title is "The Role of the State in the Development of the Economy". The author is "John Doe". The date is "January 1, 2023".

2. The second part of the document is an abstract. It provides a brief summary of the main findings of the report. The abstract states that the report examines the role of the state in the development of the economy, focusing on the impact of government intervention on economic growth and development. It also mentions that the report includes a literature review, a methodology section, and a conclusion.

3. The third part of the document is the introduction. It provides a more detailed overview of the report's content. The introduction states that the report is a comprehensive analysis of the role of the state in the development of the economy. It discusses the various ways in which the state can influence economic growth and development, and it provides a detailed overview of the report's structure and findings.

4. The fourth part of the document is the literature review. It provides a detailed overview of the existing literature on the role of the state in the development of the economy. The literature review discusses the various theories and models that have been developed to explain the relationship between the state and the economy, and it provides a critical analysis of the strengths and weaknesses of these theories and models.

5. The fifth part of the document is the methodology section. It describes the methods used to collect and analyze data for the report. The methodology section states that the report uses a combination of qualitative and quantitative methods to analyze the data. It also describes the various sources of data that were used, including government statistics, academic journals, and interviews with experts in the field.

6. The sixth part of the document is the conclusion. It provides a summary of the main findings of the report and discusses the implications of these findings for policy-making. The conclusion states that the report found that the state plays a crucial role in the development of the economy, and that government intervention is necessary to promote economic growth and development. It also discusses the various policy options that are available to governments to promote economic growth and development, and it provides recommendations for the most effective policies.

7. The seventh part of the document is the references section. It lists the various sources of information that were used in the report. The references section includes a list of academic journals, books, and government reports that were consulted during the research process.

8. The eighth part of the document is the appendix. It contains additional information that is related to the report but is not included in the main body of the text. The appendix includes a list of abbreviations, a list of acronyms, and a list of footnotes.

9. The ninth part of the document is the index. It provides a detailed overview of the report's content, including a list of the main topics and sub-topics that are covered. The index is designed to help readers find the information they are looking for quickly and easily.

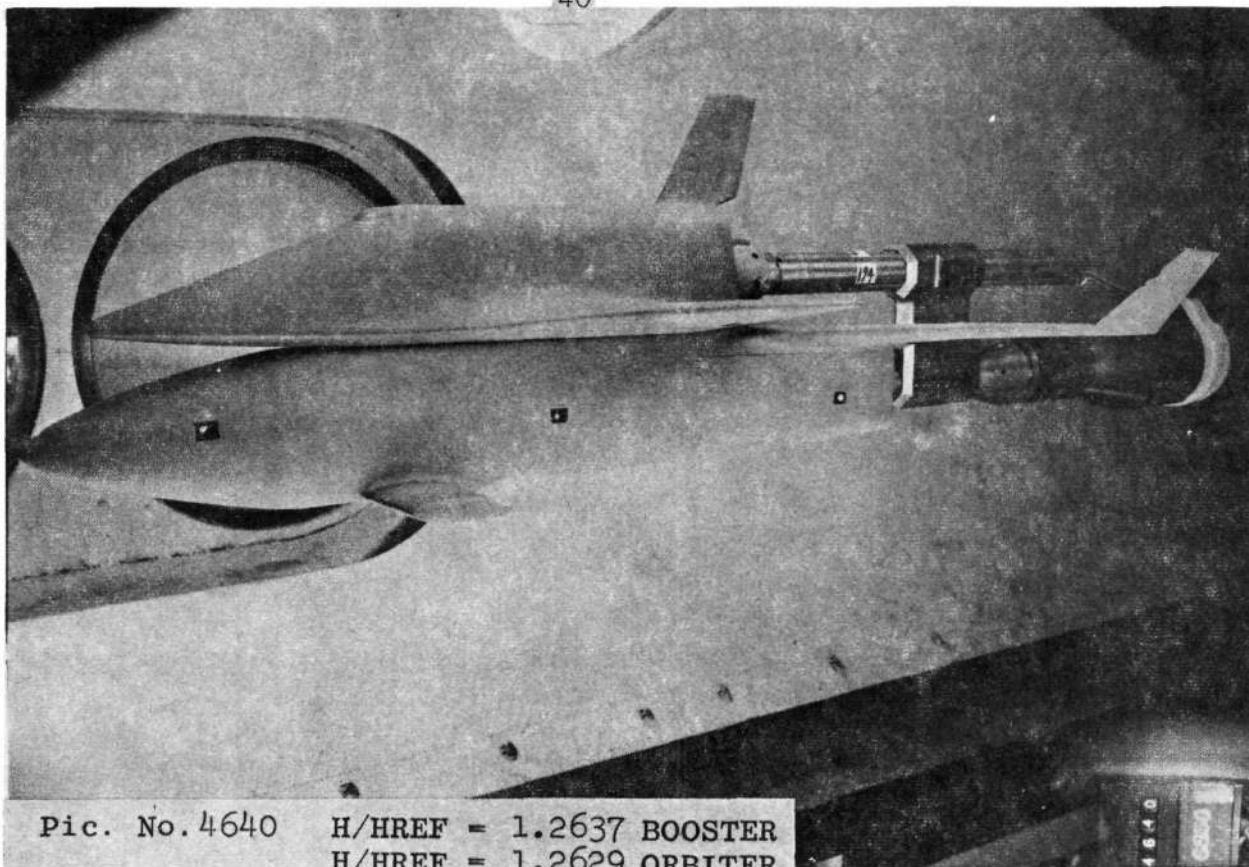
10. The tenth part of the document is the cover page. It contains the title of the report, the author's name, and the date of the report. The cover page is designed to be visually appealing and to provide a clear overview of the report's content.

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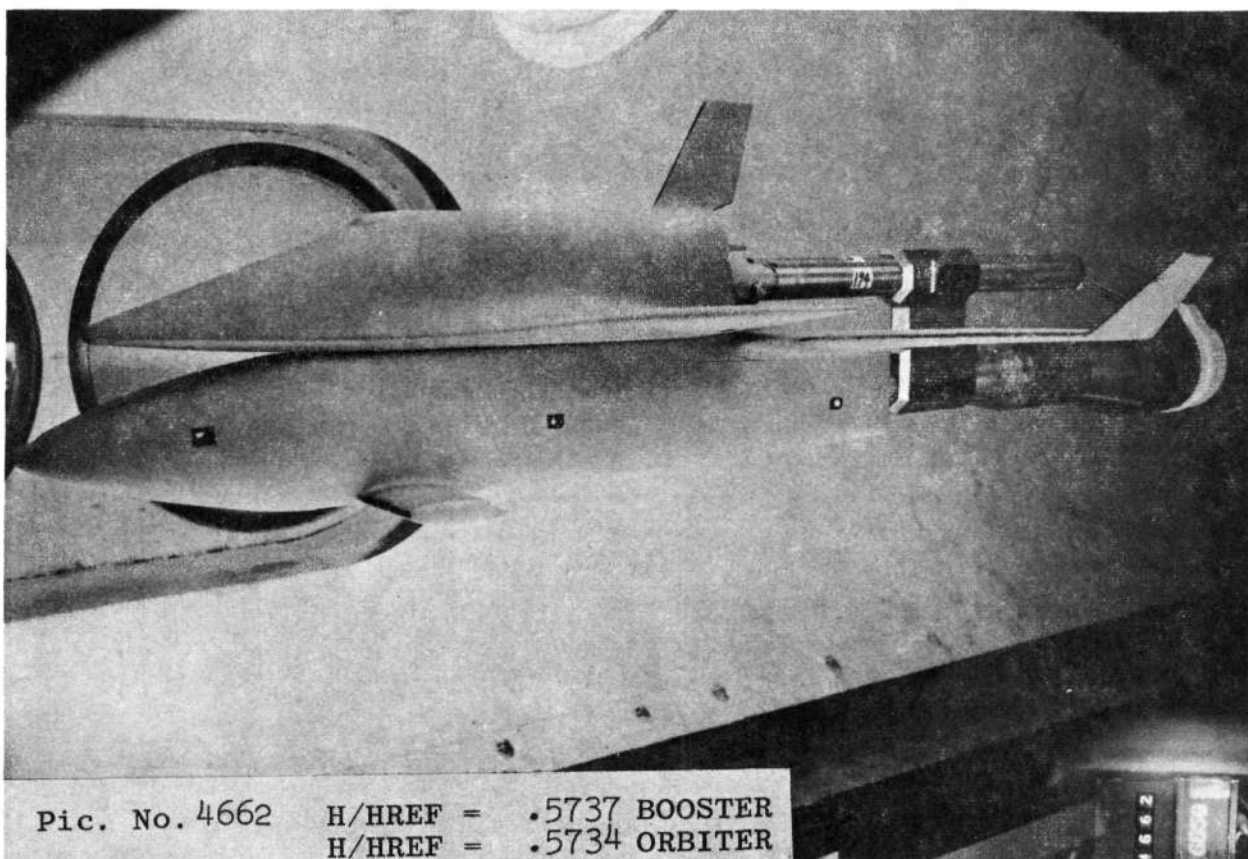
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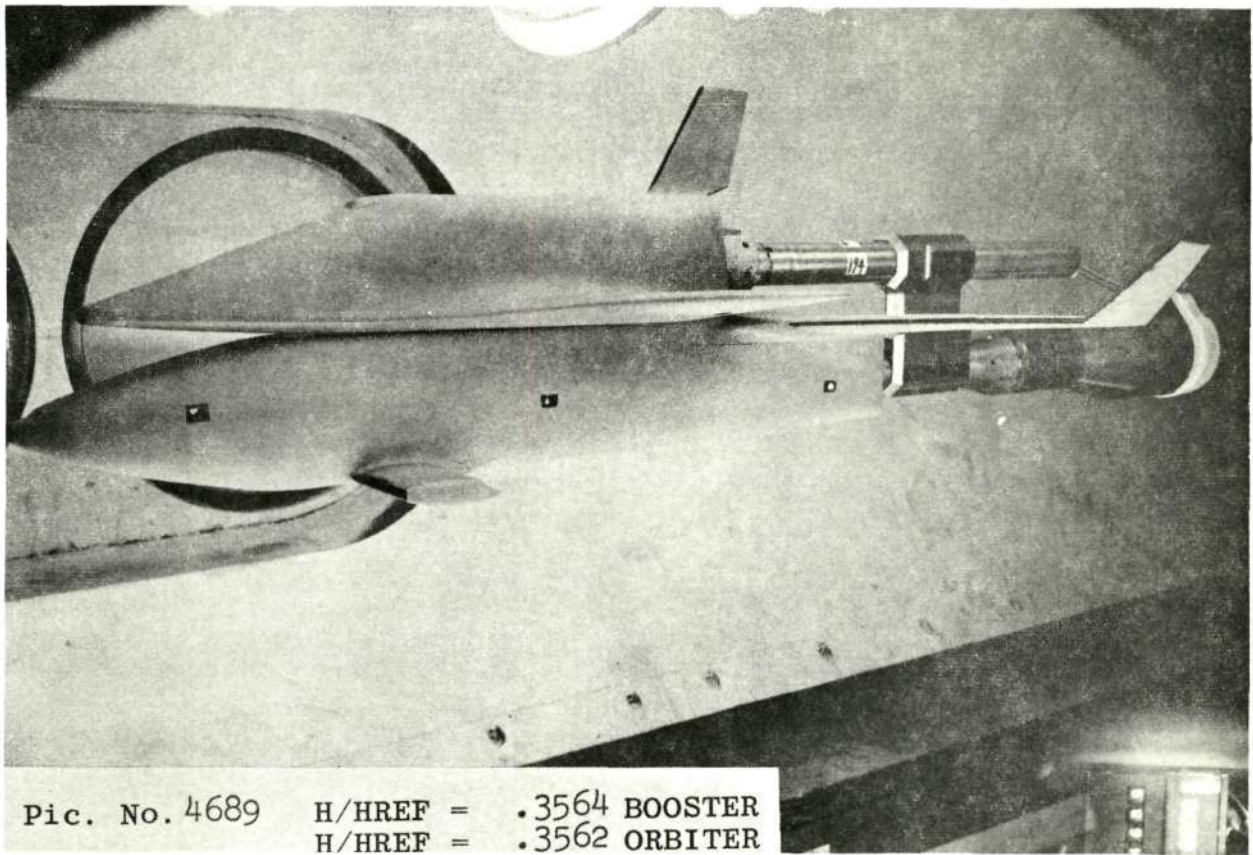
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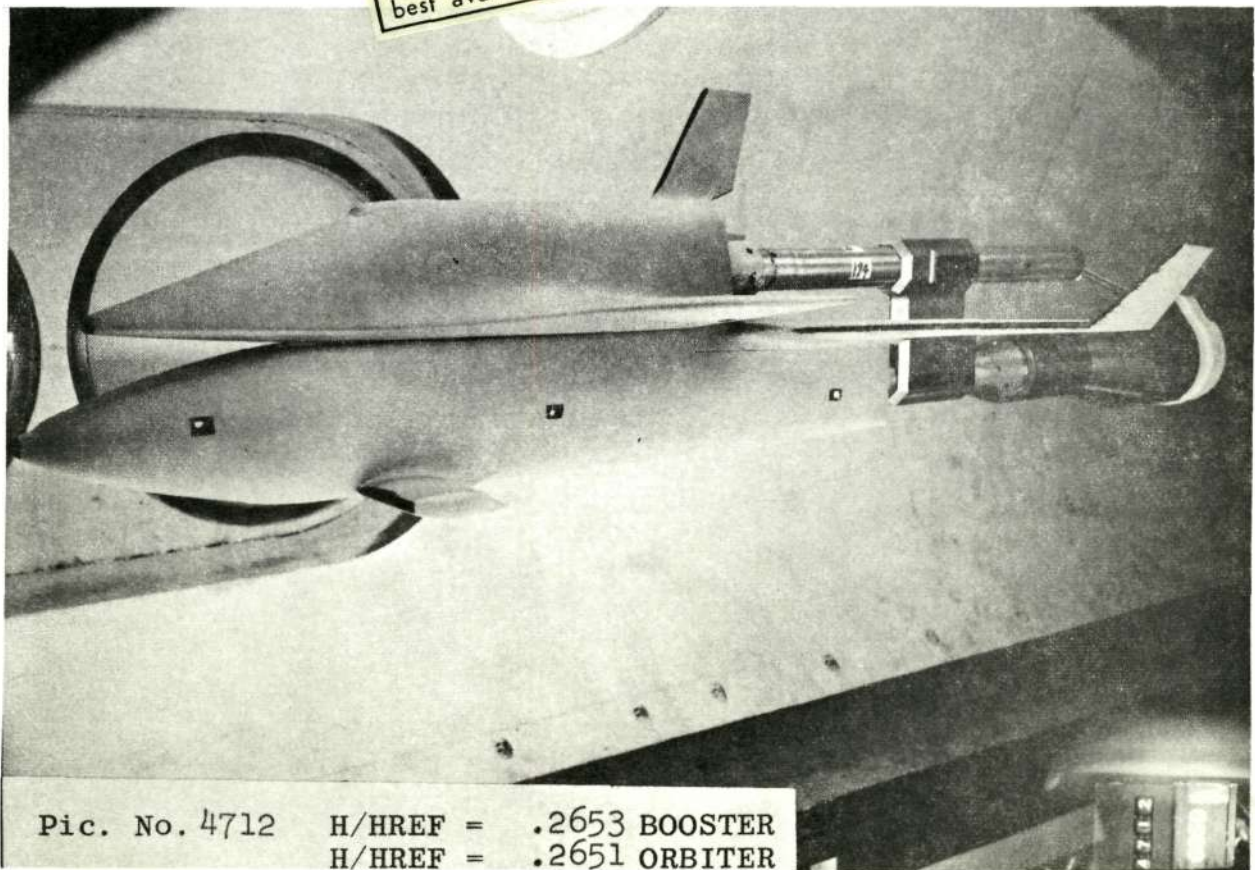


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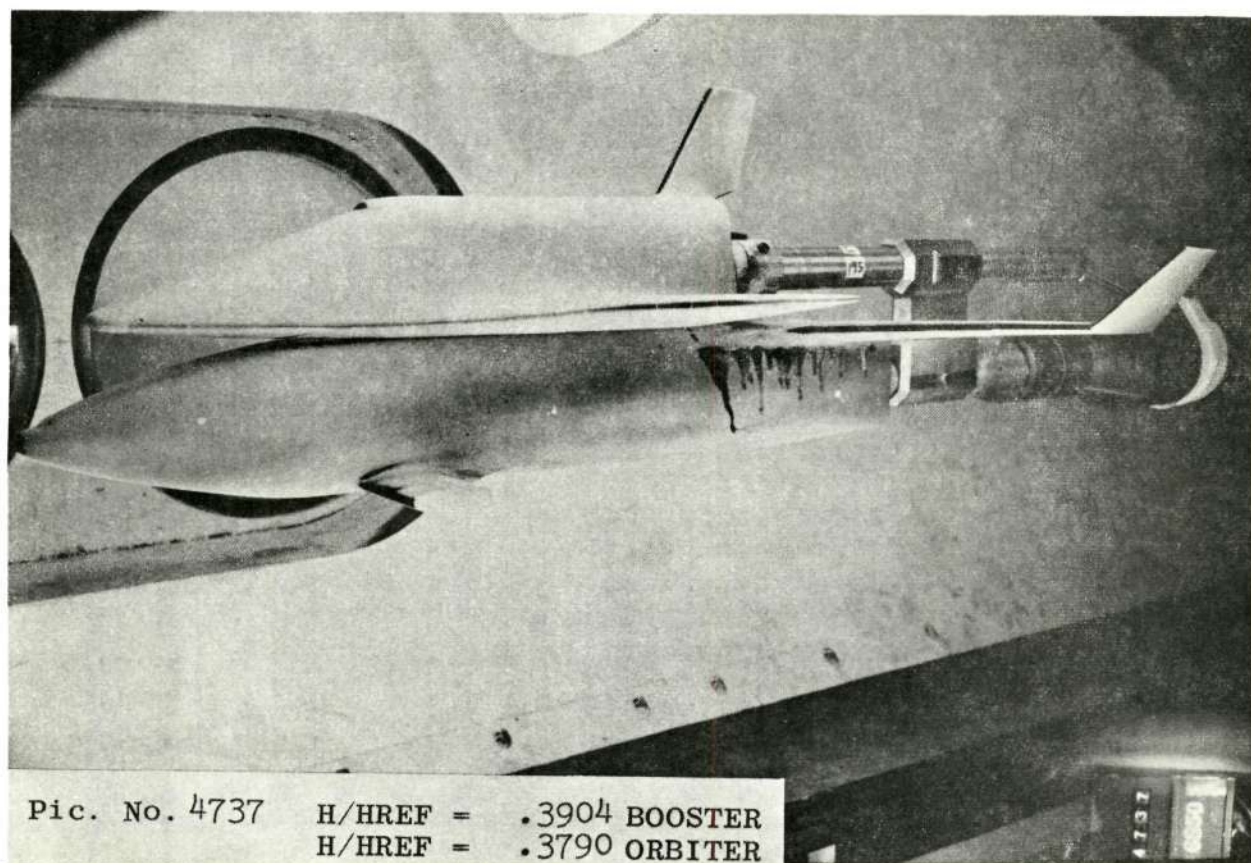
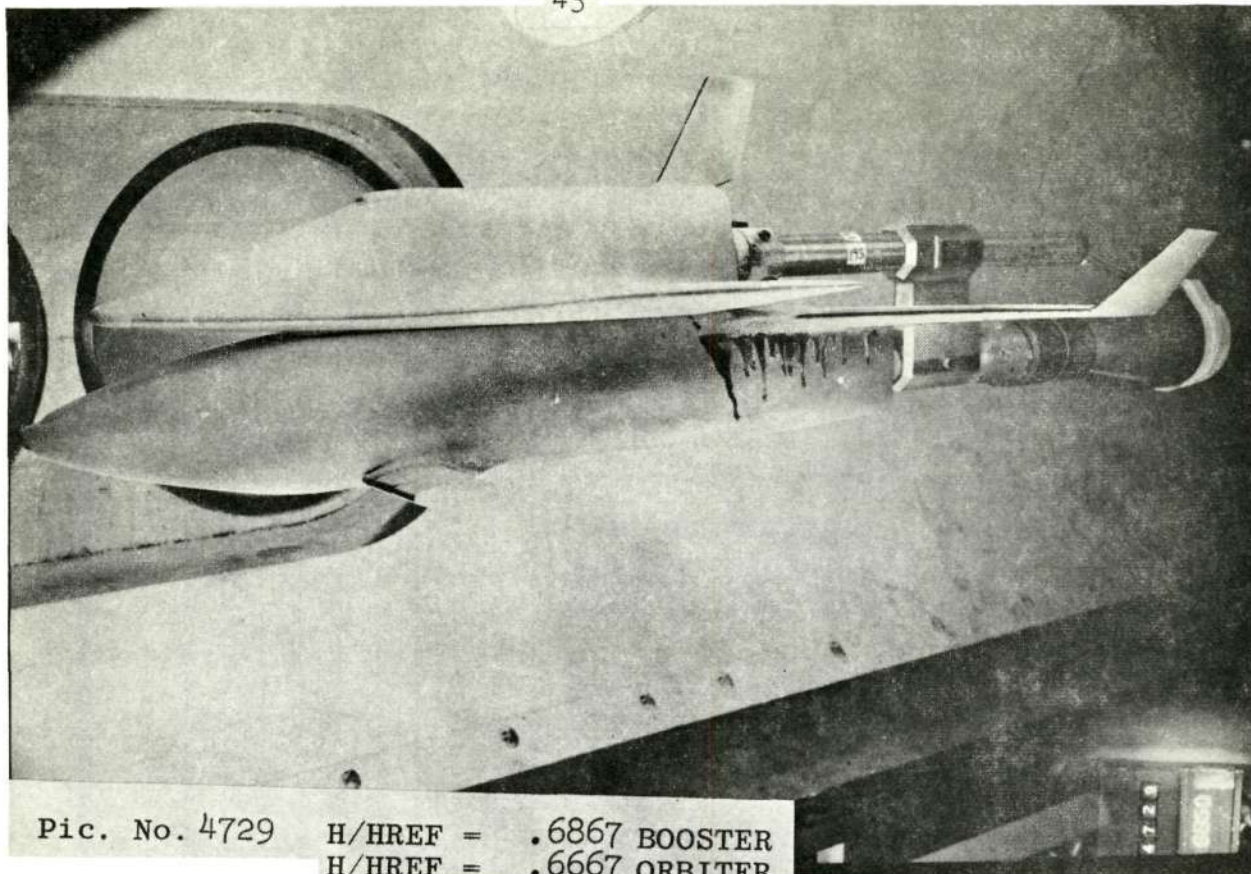
AFDC/ARO-INC.1 ARNOLO AFS, TENNESSEE
VON KARMAN GAS DYNAMICS FACILITY
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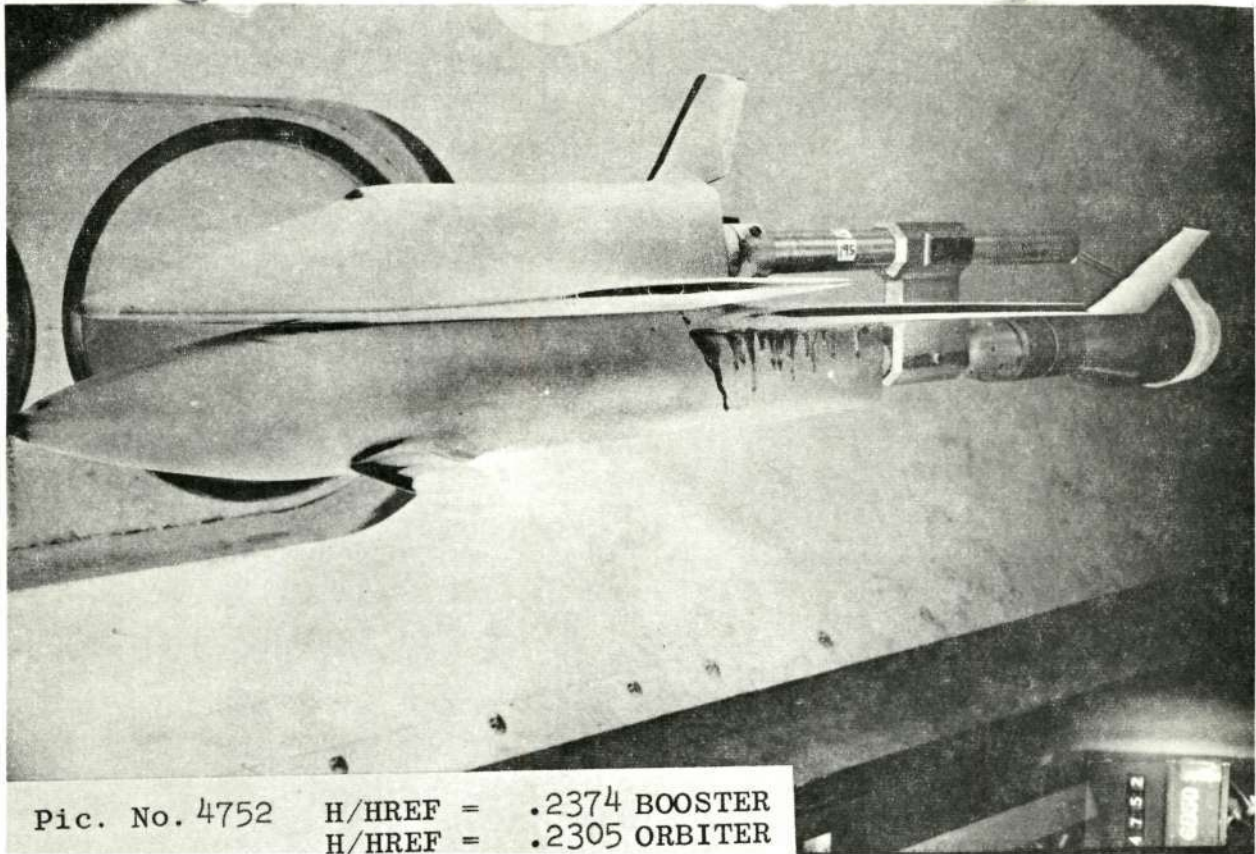
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195	3122	PD-C-8+DNC	7.03		152.6					.00	.00			

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67.0	.017	.728	3424	1.596E-05	7.002E-08	0.20E 05	2.630E-02	5.697E-02

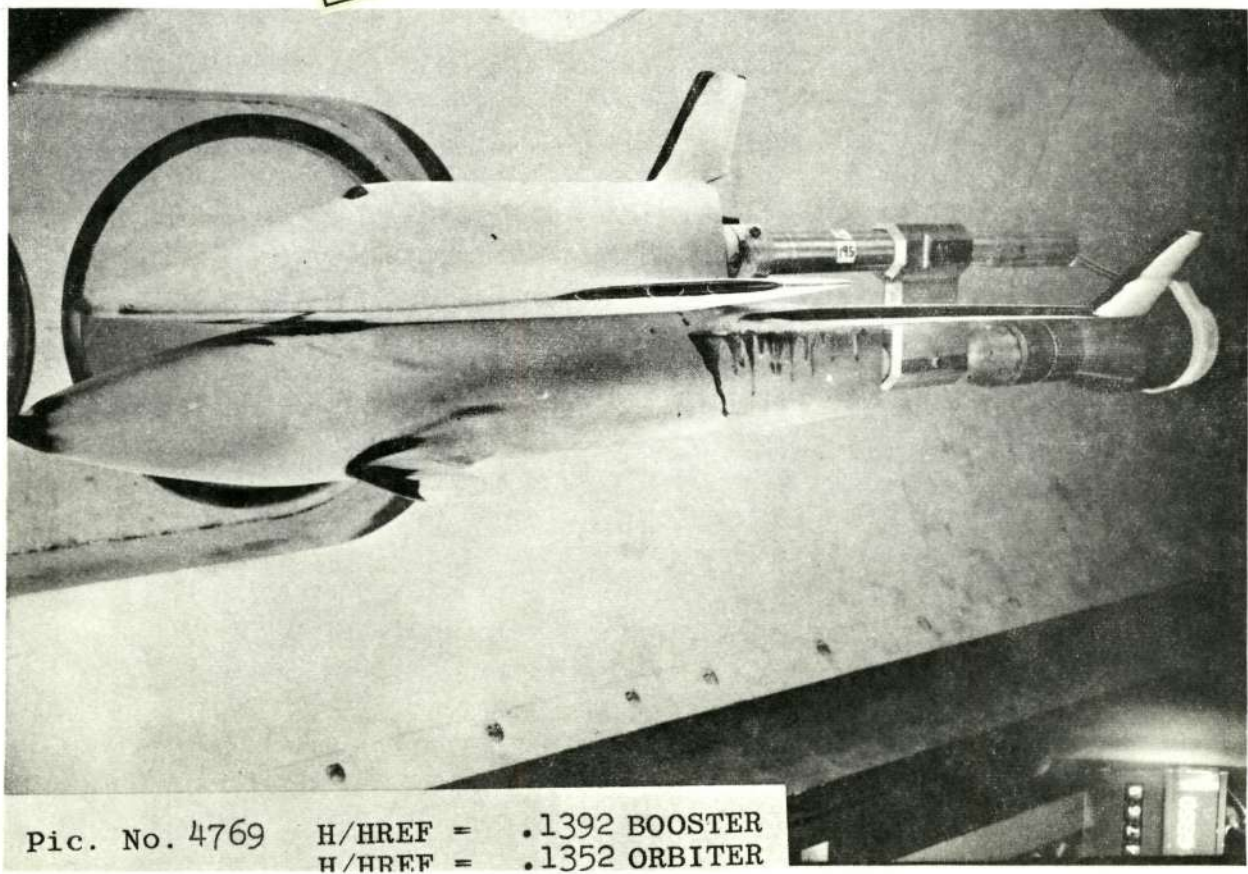
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TOP(FT)	256		
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US 4726	(250)	3.65	2.61	8 1.91E-02	.6667	2.368E-02	.9007	2.808E-02	1.0640	3.894E-02	01	77	85
US 4728	(250)	3.65	2.61	8 1.91E-02	.6667	2.368E-02	.9007	2.808E-02	1.0640	3.894E-02	01	77	85
US 4729	(250)	3.65	2.61	0 1.75E-02	.6667	2.300E-02	.8748	2.728E-02	1.0376	3.780E-02	01	77	85
US 4737	(250)	7.85	6.81	0 9.97E-03	.3790	1.368E-02	.4973	1.596E-02	.6071	2.213E-02	01	77	88
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US 4737	(250)	7.85	6.81	0 9.97E-03	.3790	1.368E-02	.4973	1.596E-02	.6071	2.213E-02	01	77	88
US 4737	(250)	7.85	6.81	0 9.97E-03	.3790	1.368E-02	.4973	1.596E-02	.6071	2.213E-02	01	77	88
US 4732	(250)	15.65	14.61	0 6.06E-03	.2305	8.192E-03	.3113	9.714E-03	.3692	1.345E-02	03	76	98
US 4732	(250)	15.65	14.61	8 6.25E-03	.2374	8.192E-03	.3113	9.714E-03	.3692	1.345E-02	03	76	98
US 4732	(250)	15.65	14.61	0 6.06E-03	.2305	7.957E-03	.3024	9.437E-03	.3546	1.306E-02	03	76	98
US 4769	(250)	30.74	29.71	0 3.46E-03	.1392	4.664E-03	.1774	5.534E-03	.2145	7.663E-03	08	76	119
US 4769	(250)	30.74	29.71	8 3.46E-03	.1392	4.664E-03	.1826	5.696E-03	.2145	7.663E-03	08	76	119
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US 4769	(250)	30.74	29.71	8 3.46E-03	.1392	4.664E-03	.1826	5.696E-03	.2145	7.663E-03	08	76	119





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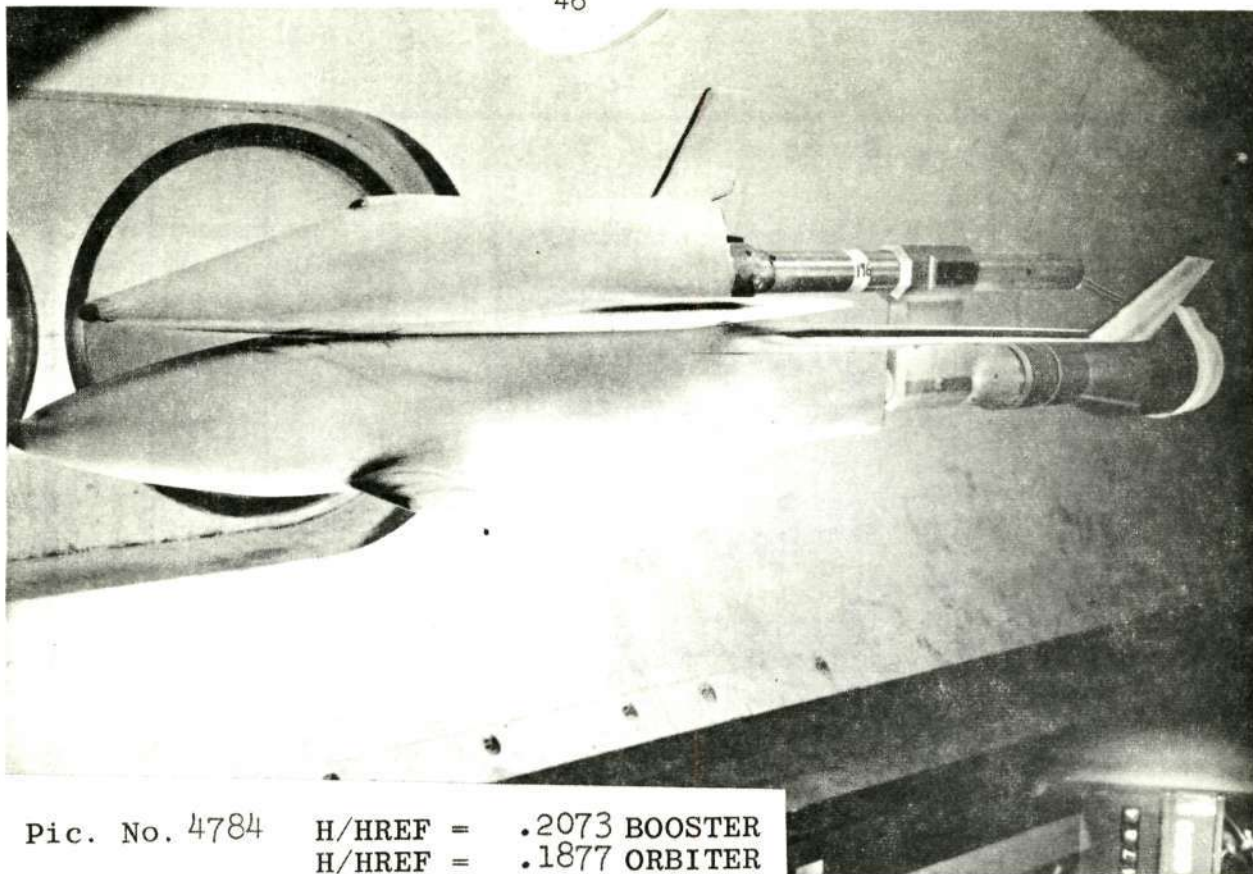


AEDICARCO INC.) ARNOLD AFS, TENNESSEE
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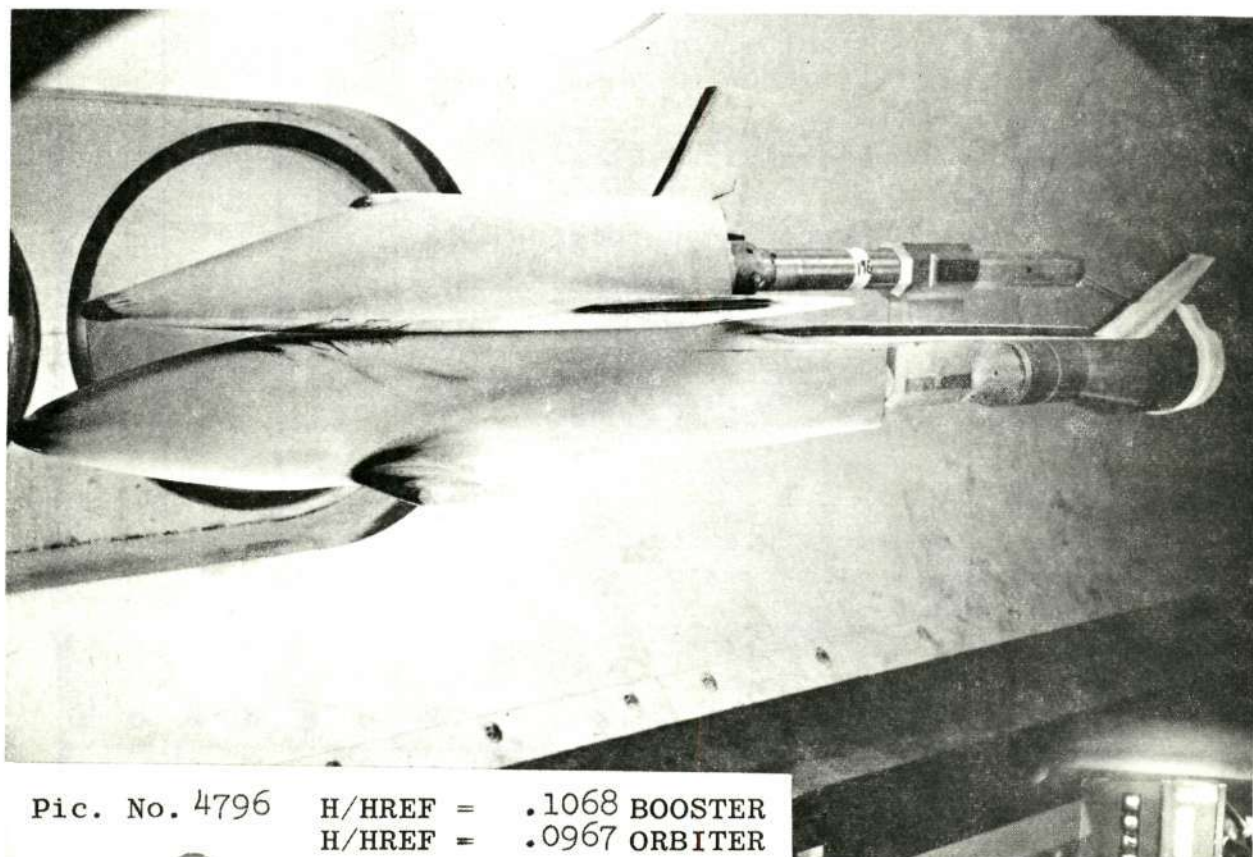
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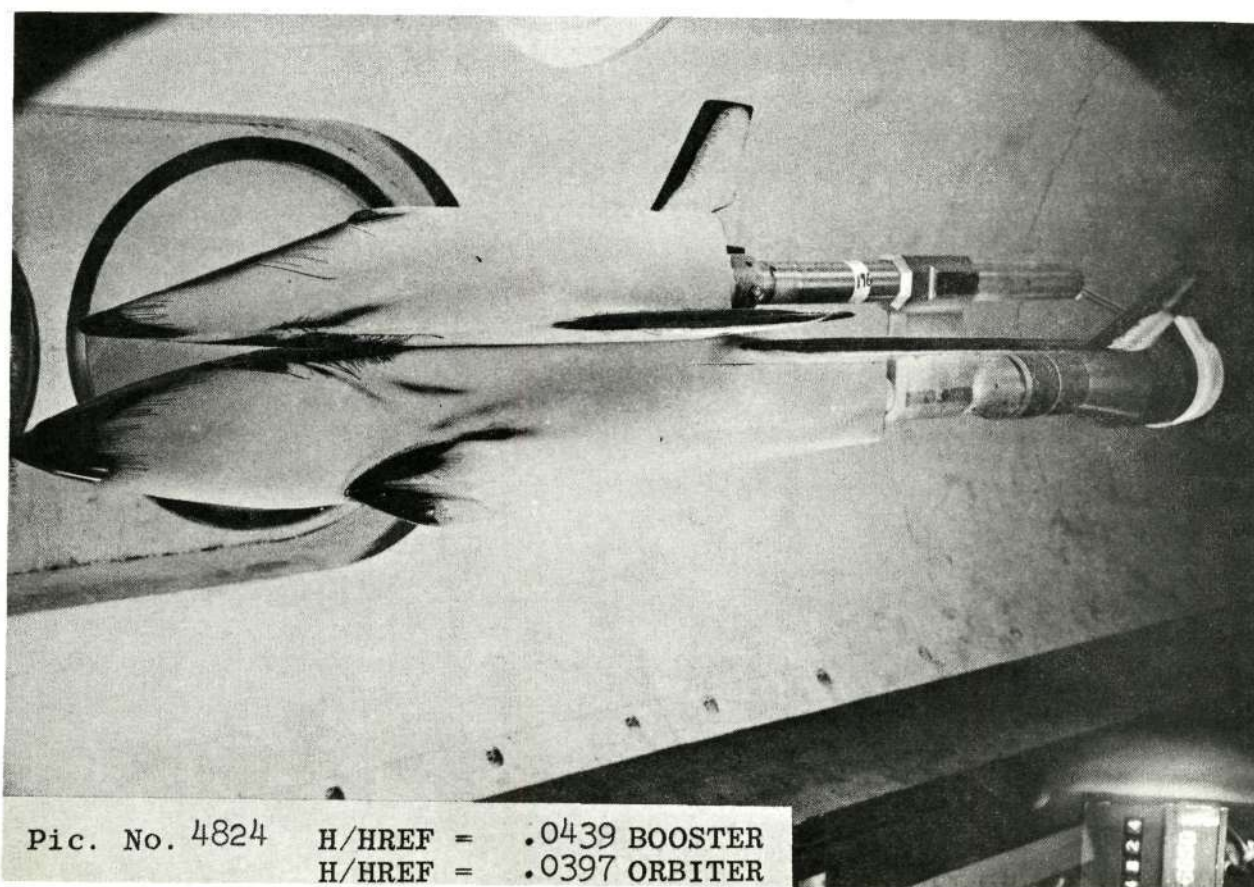
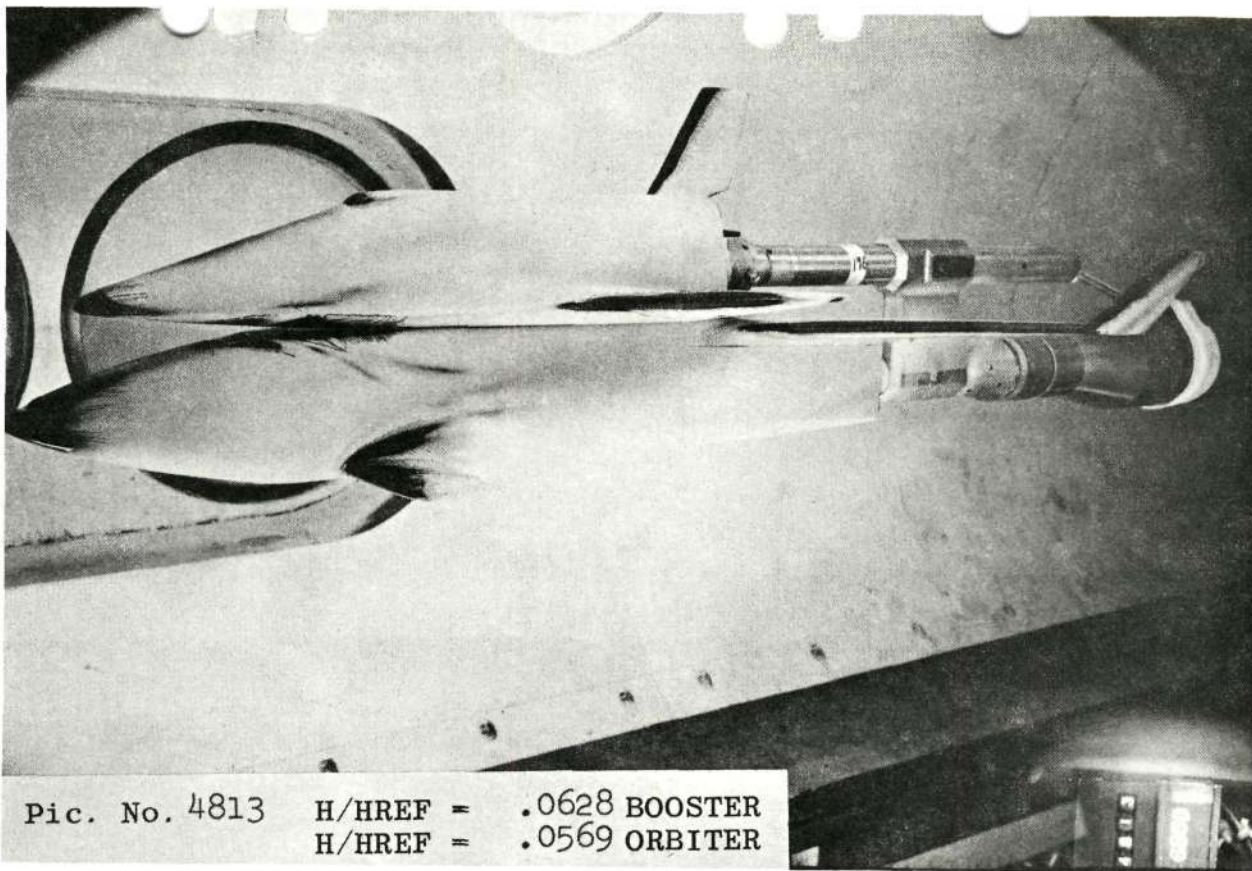
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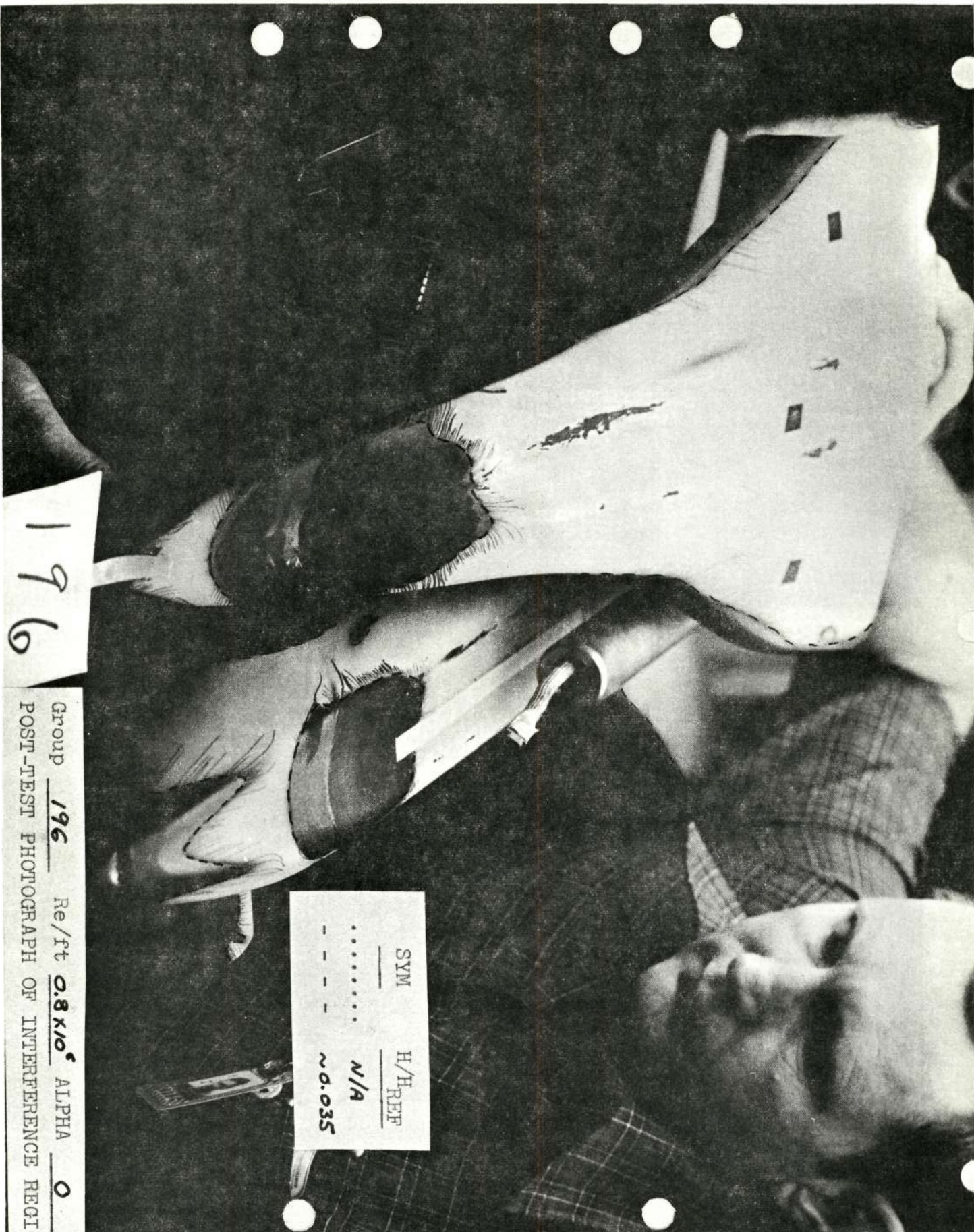


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Pic. No. 4796 H/HREF = .1068 BOOSTER
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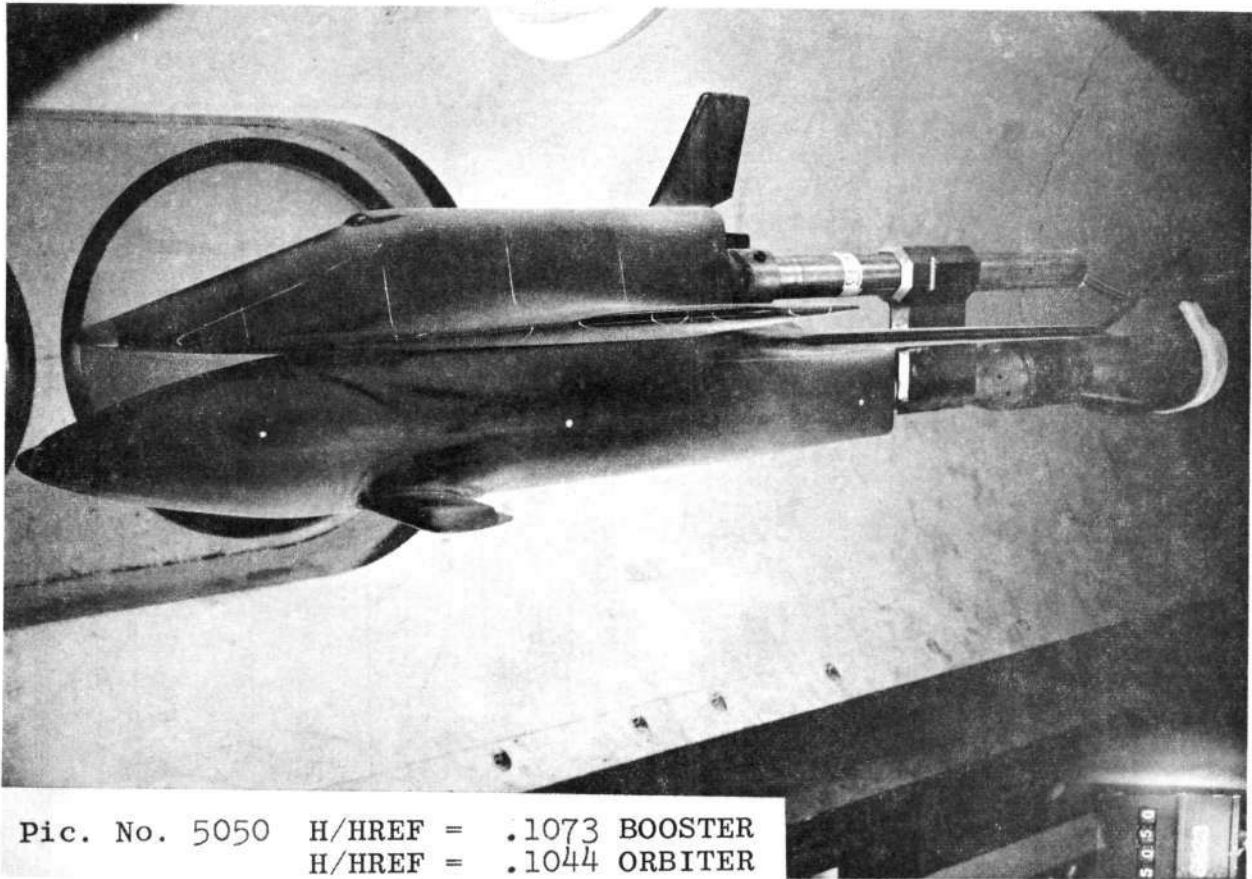
Group 196 Re/ft 0.8x10' ALPHA 0
POST-TEST PHOTOGRAPH OF INTERFERENCE REGION

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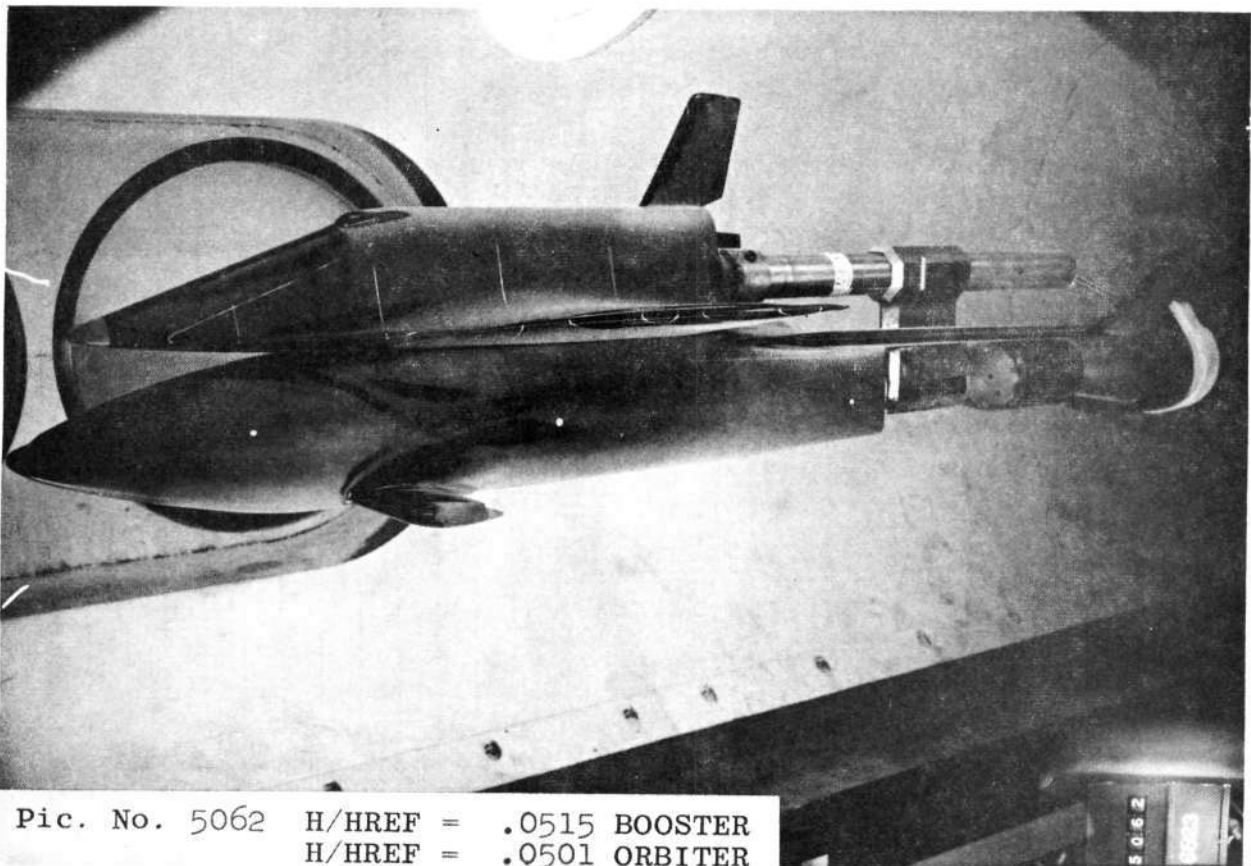
AEDC(ARO, INC.) ARNOLD AFS, TENNESSEE
VON KARMAN GAS DYNAMICS FACILITY
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GROUP	CONFID	MODEL	MACH NO	PO PSIA	TO DEG R	ALPHA-DEG	ALPHA-SECTION	ALPHA-PREBEND	ROLL-MODEL	YAW
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T-1NF P-1NF O-1NF V-1NF RHO-1NF MU-1NF RE/FT HREF STREF (NEG R) (PSIA) (PSIA) (FT/SEC) (SLUGS/FT3) (LB-SEC/FT2) (FT-1) (R-01FT) (R-01FT) P7.3 .016 .707 .3630 1.543E-05 7.027E-08 7.97E 05 2.591E-02 5.796E-02										
CAMERA PAINT TEMP (DEG F) INITIAL TEMP (DEG F) SQUARE ROOT (RHO/CX) 117 400 400 AVERAGE T _W = 01 (R) AVERAGE T _W = 02 (O)										

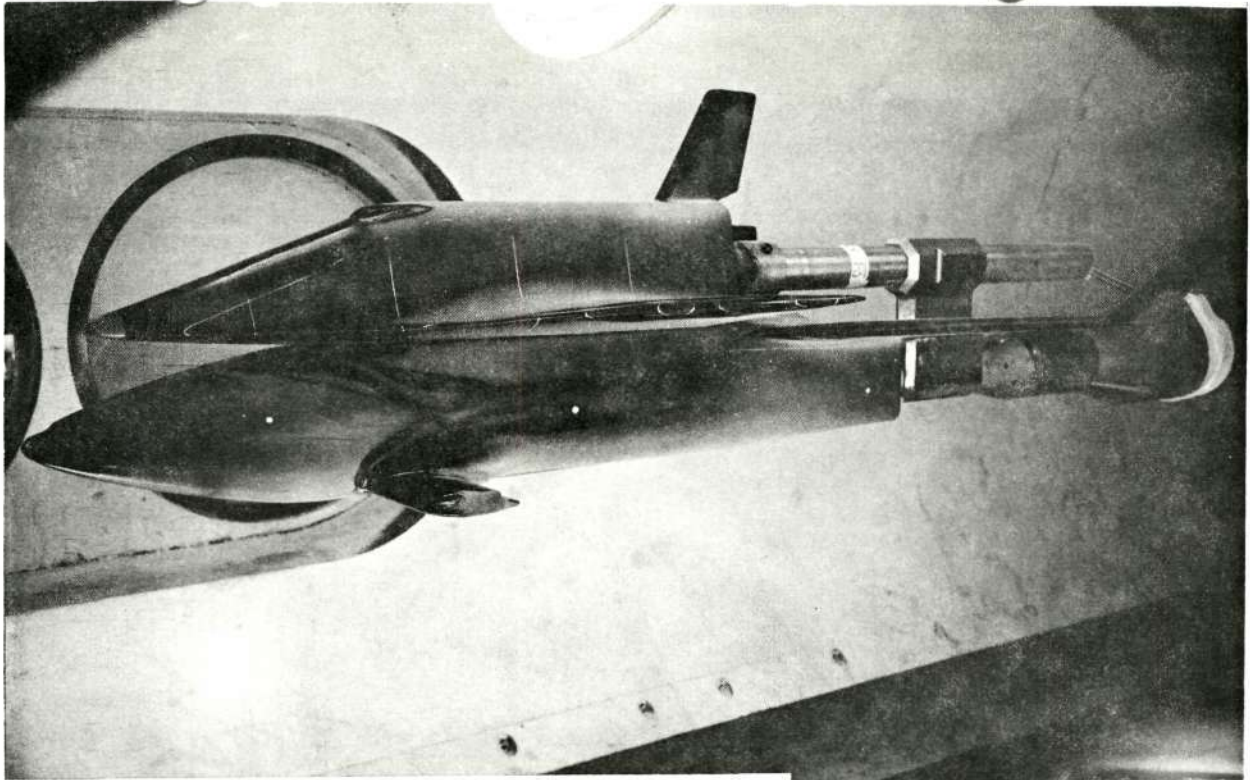
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US 5059 (117)	3.65	2.61	0.278E-03	.1073	3.439E-03	.1326	3.900E-03	.1546	6.241E-03	82 79 85 78
US 5056 (1400)	3.65	2.61	0.454E-02	1.7536	6.824E-02	2.6346	9.217E-02	3.5546	1.004E-01	82 79 85 78
US 5050 (117)	3.65	2.61	0.278E-03	.1044	3.340E-03	.1292	3.796E-03	.1446	6.071E-03	82 79 85 78
US 5062 (1400)	9.95	8.91	0.218E-02	.0644	3.269E-02	1.2656	4.416E-02	1.1044	4.815E-02	82 79 91 78
US 5062 (117)	9.95	8.91	0.173E-03	.0515	1.650E-03	.0637	1.813E-03	.0723	2.999E-02	82 79 91 78
US 5062 (1400)	9.95	8.91	0.218E-02	.0624	1.277E-02	1.2656	4.427E-02	1.1044	4.827E-02	82 79 91 78
US 5062 (117)	9.95	8.91	0.170E-03	.0501	1.601E-03	.0621	1.823E-03	.0746	2.918E-02	82 79 91 78
US 5076 (1400)	17.25	16.21	0.146E-02	.0346	2.190E-02	.0452	2.957E-02	.0746	3.223E-02	82 80 103 78
US 5076 (117)	17.25	16.21	0.894E-04	.0346	1.105E-03	.0427	1.254E-03	.0444	2.008E-03	82 80 103 78
US 5076 (1400)	17.25	16.21	0.894E-02	.0346	2.190E-02	.0452	2.957E-02	.0746	3.223E-02	82 80 103 78
US 5076 (117)	17.25	16.21	0.894E-04	.0346	1.105E-03	.0427	1.254E-03	.0444	2.008E-03	82 80 103 78
US 5090 (1400)	31.24	30.24	0.946E-03	.0346	1.076E-03	.0415	1.221E-03	.0471	1.953E-03	82 80 124 78
US 5090 (117)	31.24	30.24	0.946E-04	.0215	1.362E-02	.0255	1.839E-02	.0709	2.003E-02	82 81 124 80
US 5090 (1400)	31.24	30.24	0.946E-03	.0215	1.362E-02	.0255	1.839E-02	.0709	2.003E-02	82 81 124 80
US 5090 (117)	31.24	30.24	0.946E-04	.0215	1.362E-02	.0255	1.839E-02	.0709	2.003E-02	82 81 124 80
US 5090 (117)	31.24	30.24	0.541E-04	.0209	6.603E-04	.0258	7.594E-04	.0293	1.214E-03	82 81 124 80



Pic. No. 5050 H/HREF = .1073 BOOSTER
H/HREF = .1044 ORBITER

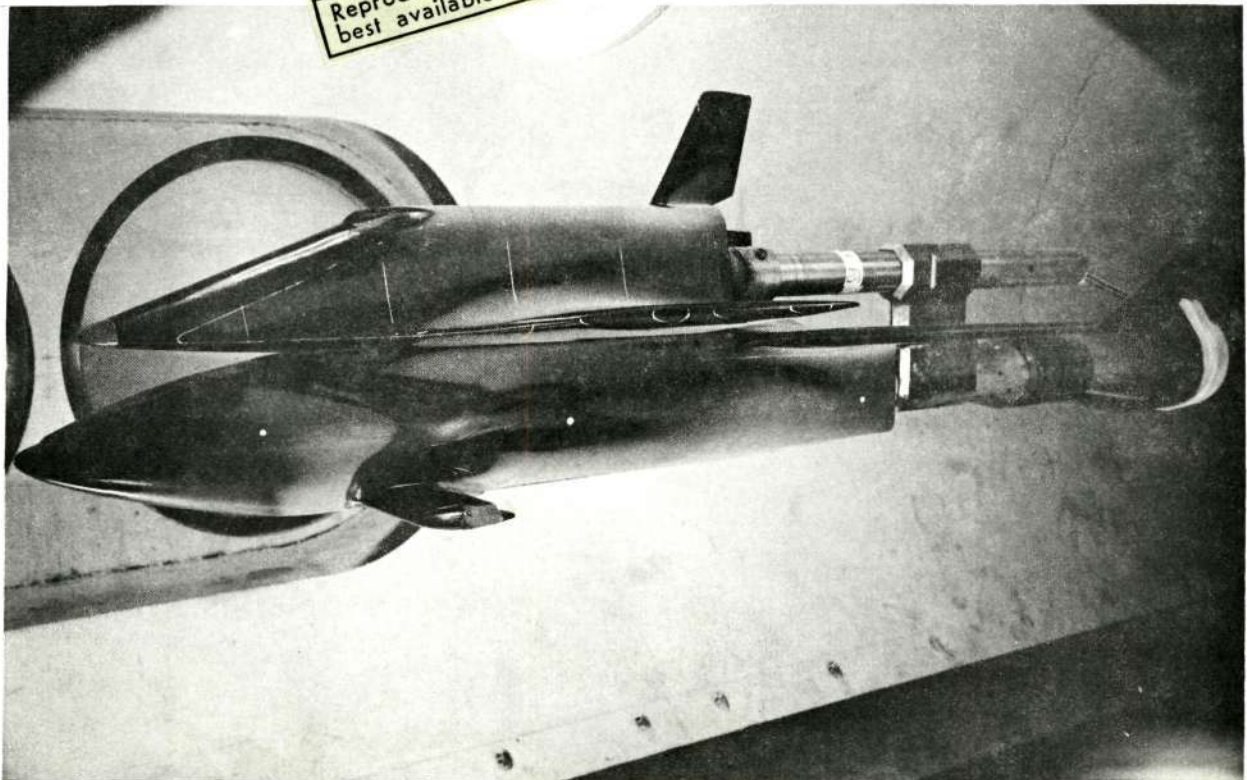


Pic. No. 5062 H/HREF = .0515 BOOSTER
H/HREF = .0501 ORBITER

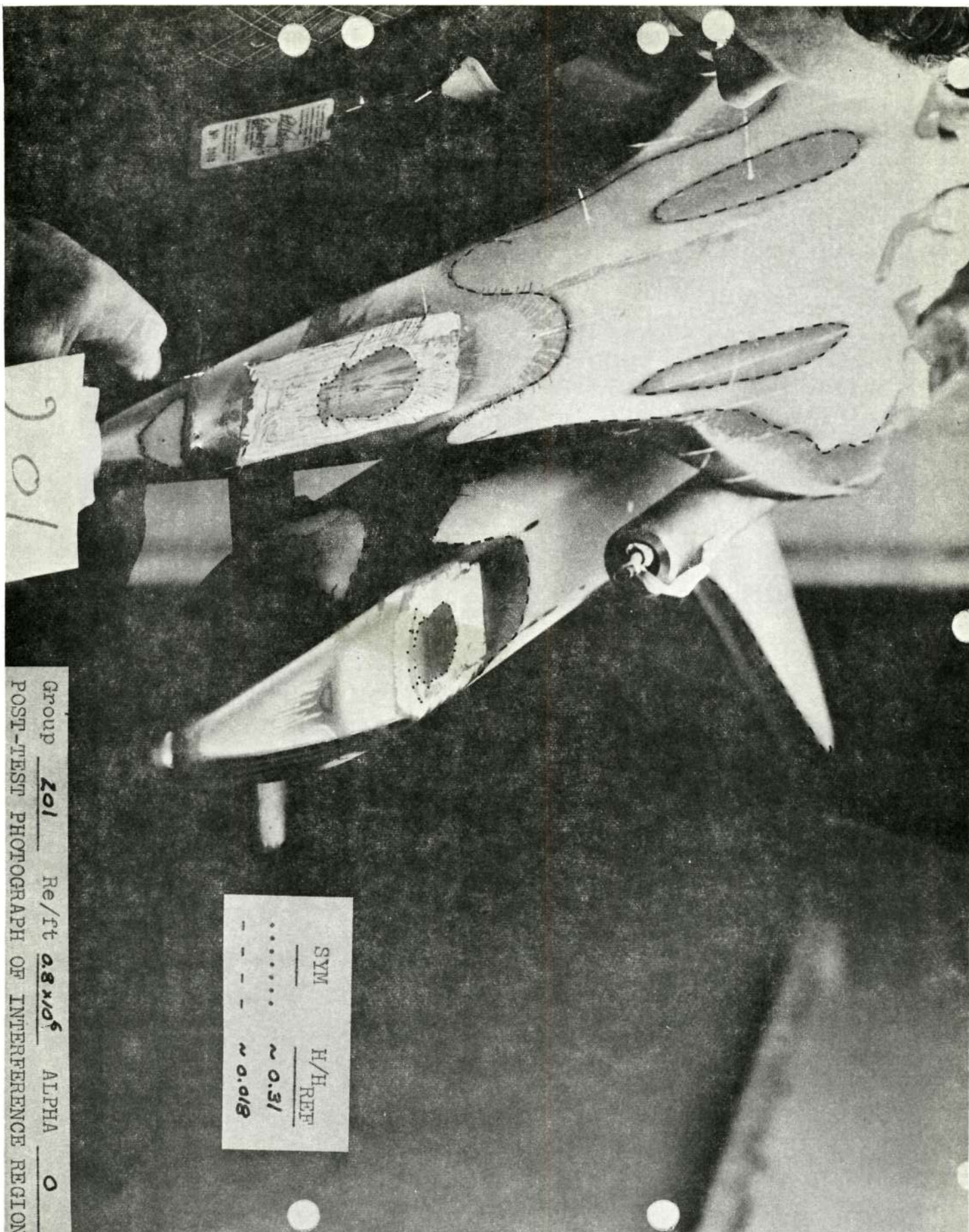


Pic. No. 5076 H/HREF = .0345 BOOSTER
 H/HREF = .0336 ORBITER

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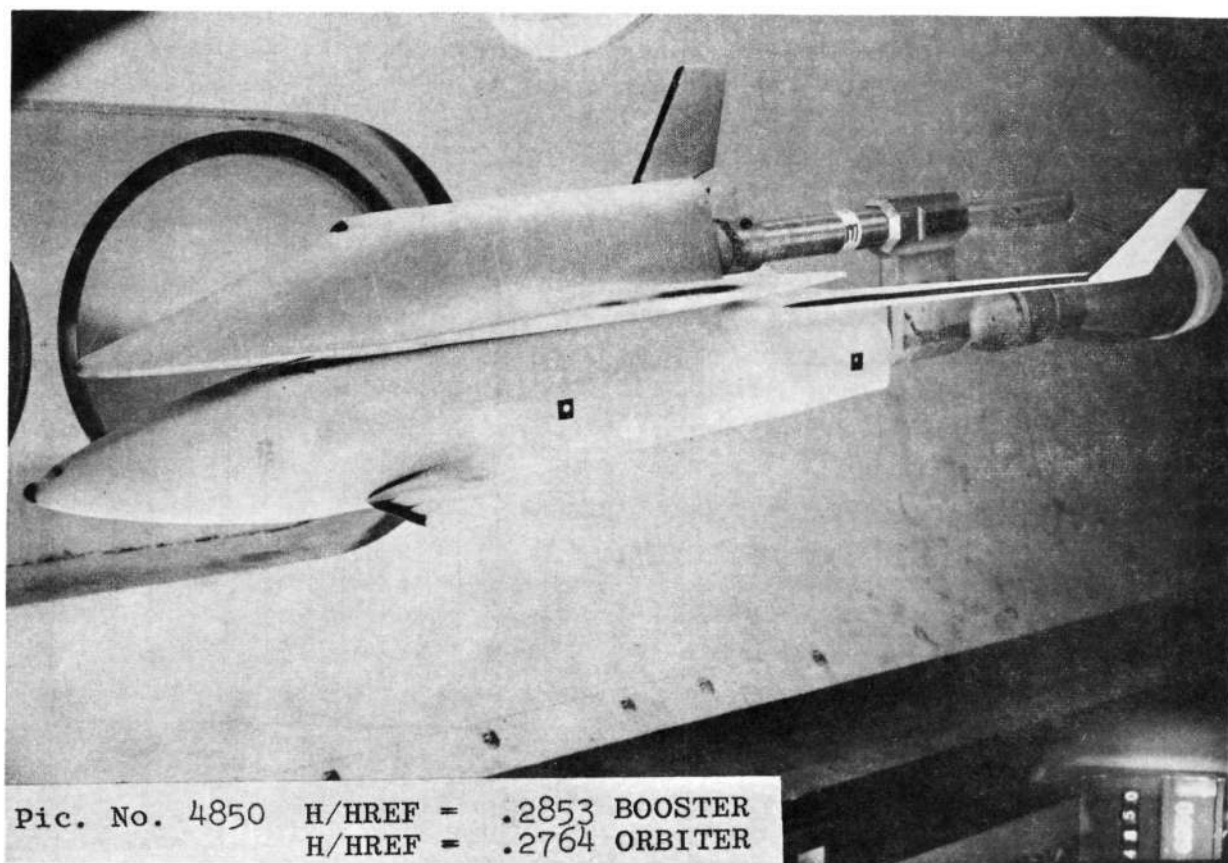
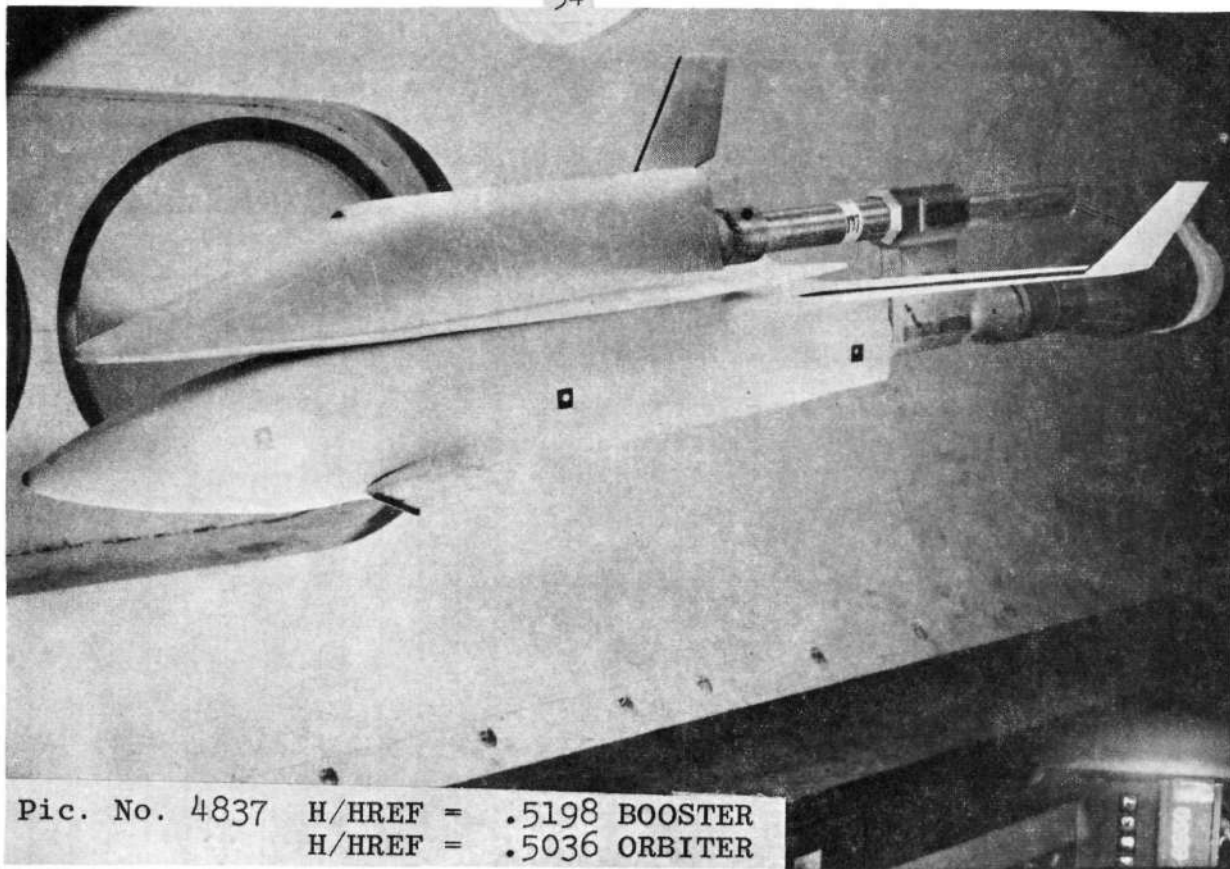


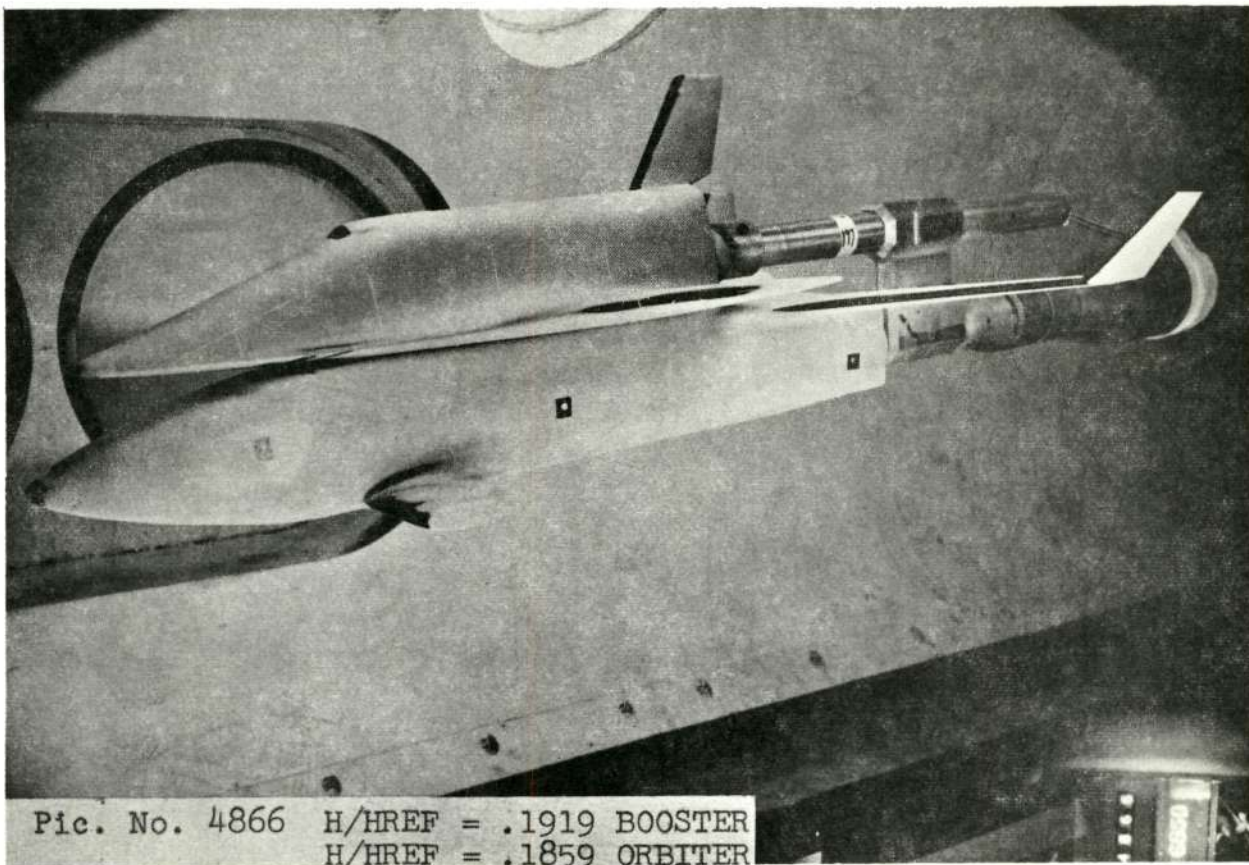
Pic. No. 5090 H/HREF = .0215 BOOSTER
 H/HREF = .0209 ORBITER



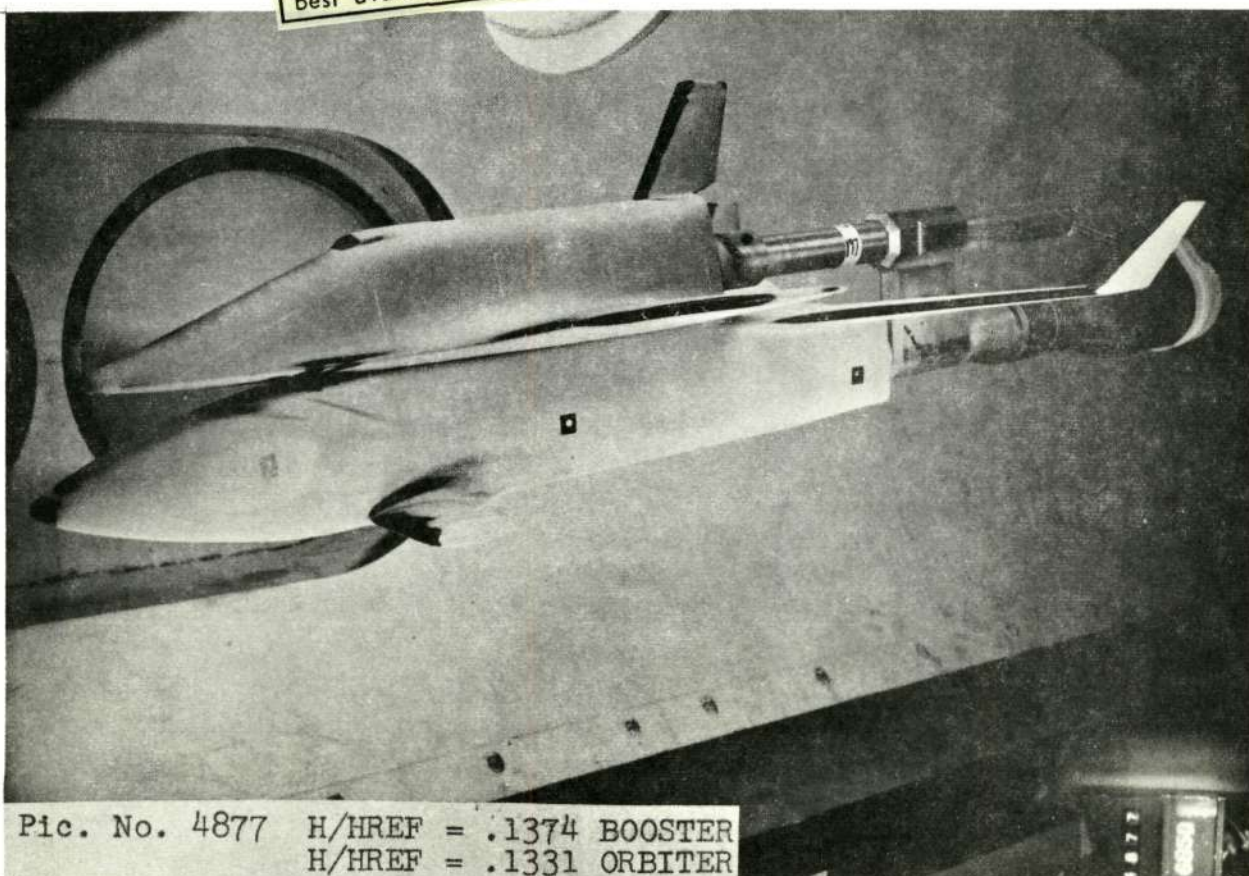
Group 201 Re/ft 0.8x10⁶ ALPHA 0
 POST-TEST PHOTOGRAPH OF INTERFERENCE REGION

SYM	H/H _{REF}
.....	~ 0.31
- - - -	~ 0.018





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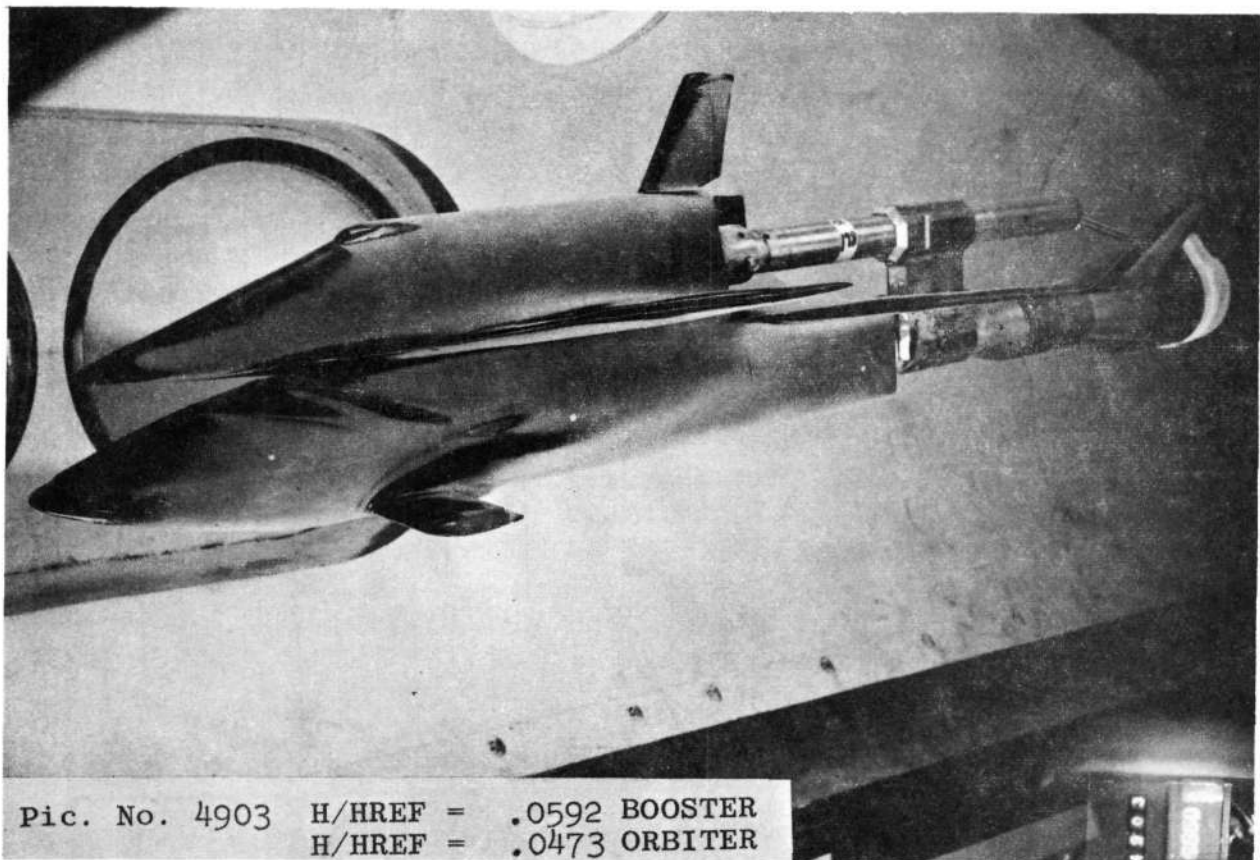
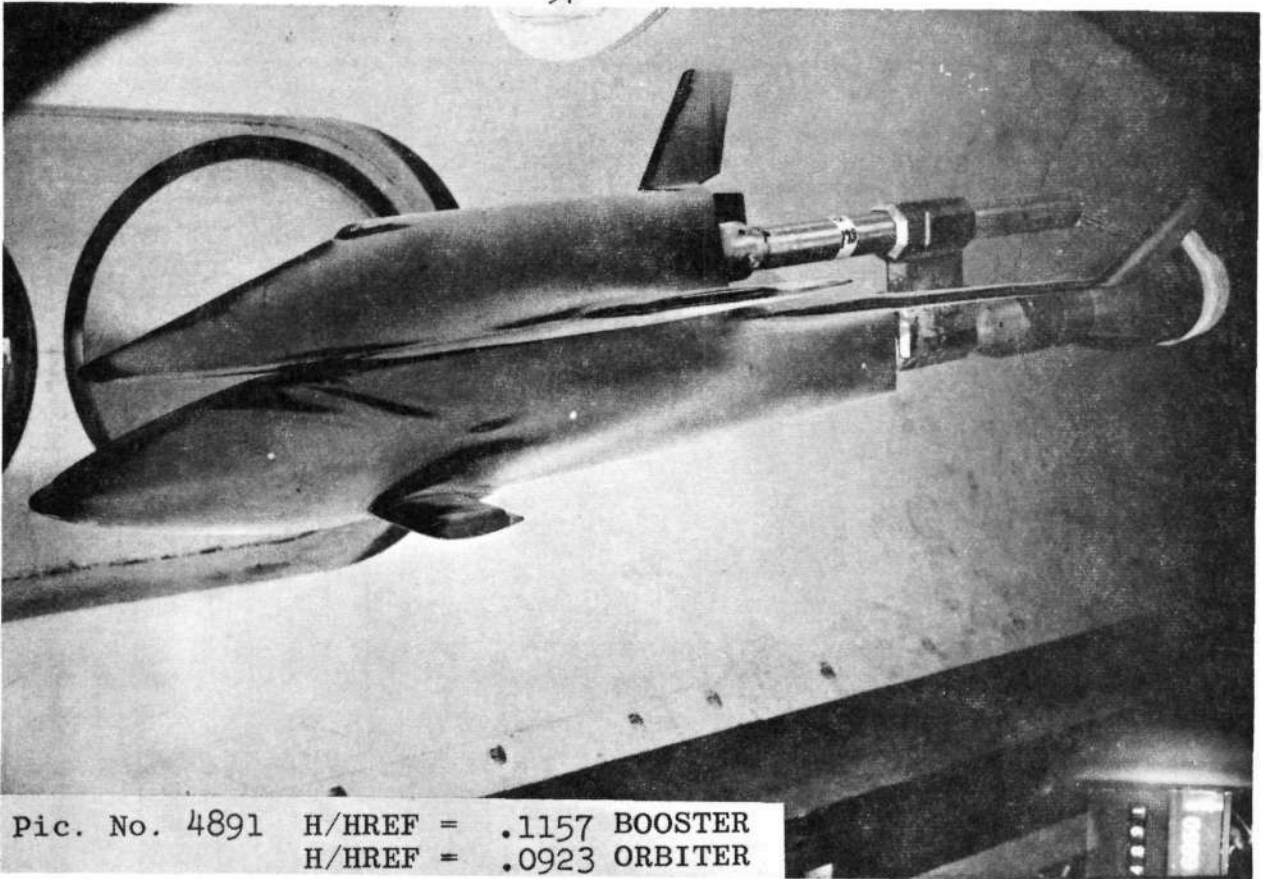


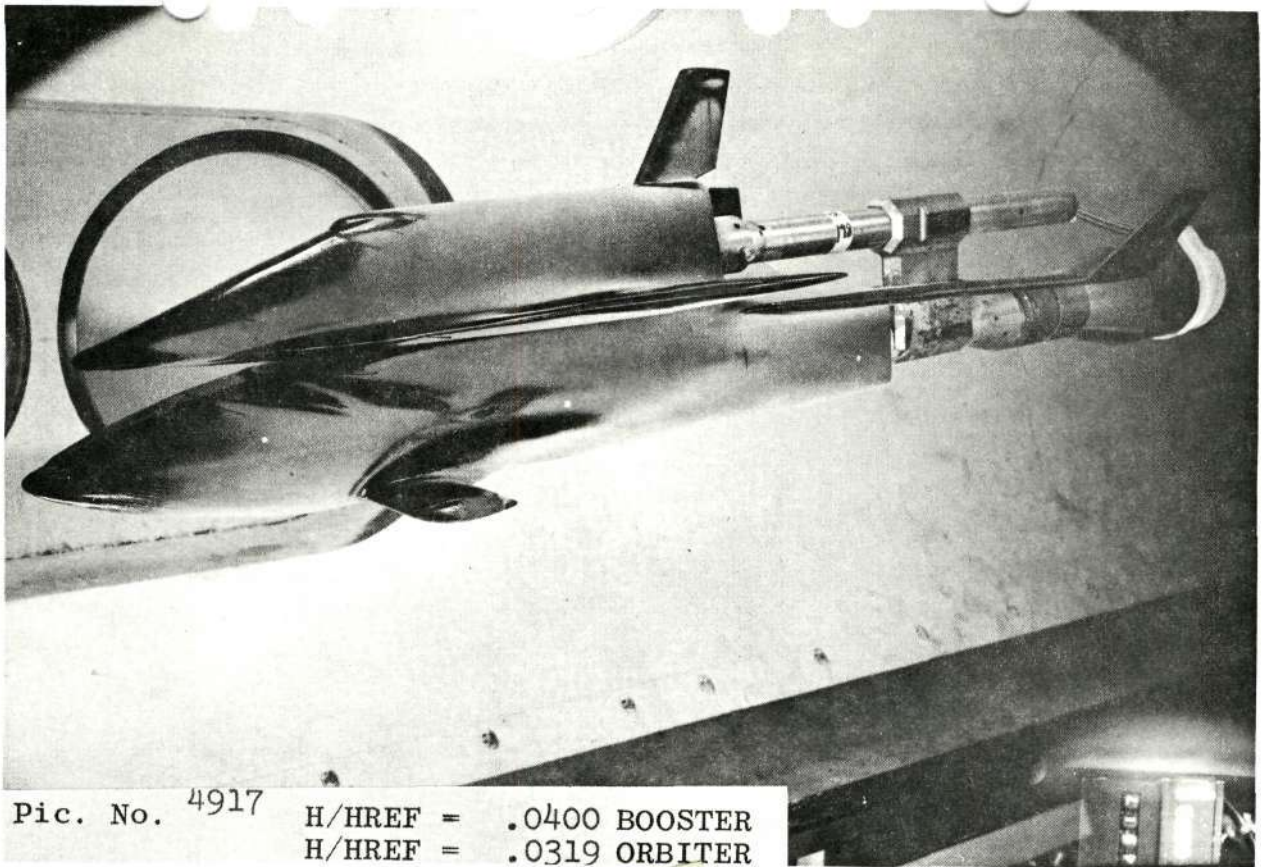
6/ 3/71

AEDC(ARO,INC.) ARNOLD AFS, TENNESSEE
VON KARMAN GAS DYNAMICS FACILITY
50 INCH HYPERSONIC TUNNEL
VT1162

GROUP	CONFID	MODEL	MACH NO	PO PSIA	TO DEG R	ALPHA-ANGLE	ALPHA-SECTOR	ALPHA-PREREMO	ROLL-MODEL	YAW
198	3221	MOAC-8-DVC	7.93	152.4	1192	-5.00	-5.00	0	0	0
T-1NF P-1NF Q-1NF V-1NF RHO-1NF MU-1NF RE/FT HREF STREF (DEG R) (PSIA) (FT/SEC) (SLUGS/FT3) (LB-SEC/FT2) (FT-1) (IN-01FT) (IN-01FT) 87.0 .017 .727 3641 1.579E-05 7.089E-08 0.13E 05 2.633E-02 5.733E-02										
CAMERA PAINT TEMP (DEG F) INITIAL TEMP (DEG F) SQUARE ROOT (RHOXCHK) TOP(1) 117 SIDE(US) 500 SIDE(LS) 500										
AVERAGE TW = 73 (R) AVERAGE TW = 81 (L)										
-0.008(SQUARE ROOT DEL TIME) * 0.11										

PIC NO	TIME DELTIME	H(TO)	H(TO)/HREF	M(.910)	M(.910)/HREF	M(.8510)	M(.8510)/HREF	ST(TO)	MODEL TEMP F
US 4991 (500)	4.20 3.13	0 7.07E-02	2.6944	1.344E-01	5.1052	2.52E-01	9.54E2	1.511E-01	72 73 84 88
US 4991 (113)	4.20 3.13	8 3.35E-03	.1157	3.70E-03	.1428	4.61E-03	.1519	6.651E-03	72 73 84 88
US 4991 (500)	4.20 3.13	8 7.19E-02	2.7318	1.368E-01	5.1943	2.524E-01	9.58E2	1.537E-01	72 73 84 88
US 4991 (113)	4.20 3.13	0 2.43E-03	.0923	3.00E-03	.1140	3.403E-03	.1203	5.305E-03	72 73 84 88
US 4903 (500)	10.55 9.44	0 3.62E-02	1.3749	6.882E-02	2.6138	1.292E-01	4.9074	7.738E-02	73 74 94 81
US 4903 (113)	10.55 9.44	8 1.56E-03	.0592	1.925E-03	.0731	2.182E-03	.0829	3.405E-03	73 74 94 81
US 4903 (500)	10.55 9.44	8 3.58E-02	1.3947	7.402E-02	2.6594	1.292E-01	4.9074	7.738E-02	73 74 94 81
US 4903 (113)	10.55 9.44	0 1.74E-03	.0473	1.636E-03	.0593	1.742E-03	.0642	2.716E-03	73 74 94 81
US 4917 (500)	18.05 16.94	0 2.44E-02	.9277	4.640E-02	1.7637	8.713E-02	.0939	5.224E-02	74 75 109 84
US 4917 (113)	18.05 16.94	8 1.05E-03	.0400	1.298E-03	.0493	1.471E-03	.0539	2.299E-03	74 75 109 84
US 4917 (500)	18.05 16.94	8 2.48E-02	.9438	4.721E-02	1.7944	8.713E-02	.0939	5.224E-02	74 75 109 84
US 4917 (113)	18.05 16.94	0 8.39E-04	.0319	1.036E-03	.0394	1.17E-03	.0447	1.834E-03	74 75 109 84
US 4931 (500)	32.89 31.82	0 1.70E-02	.5719	2.855E-02	1.0872	1.17E-03	.0447	1.834E-03	74 75 109 84
US 4931 (113)	32.89 31.82	8 6.47E-04	.0246	7.985E-04	.0304	9.051E-04	.0345	1.420E-03	76 77 132 87
US 4931 (500)	32.89 31.82	8 1.53E-02	.5818	2.905E-02	1.1061	5.360E-02	2.0012	3.682E-02	76 77 132 87
US 4931 (113)	32.89 31.82	0 5.16E-04	.0197	6.373E-04	.0263	7.220E-04	.0275	1.133E-03	76 77 132 87

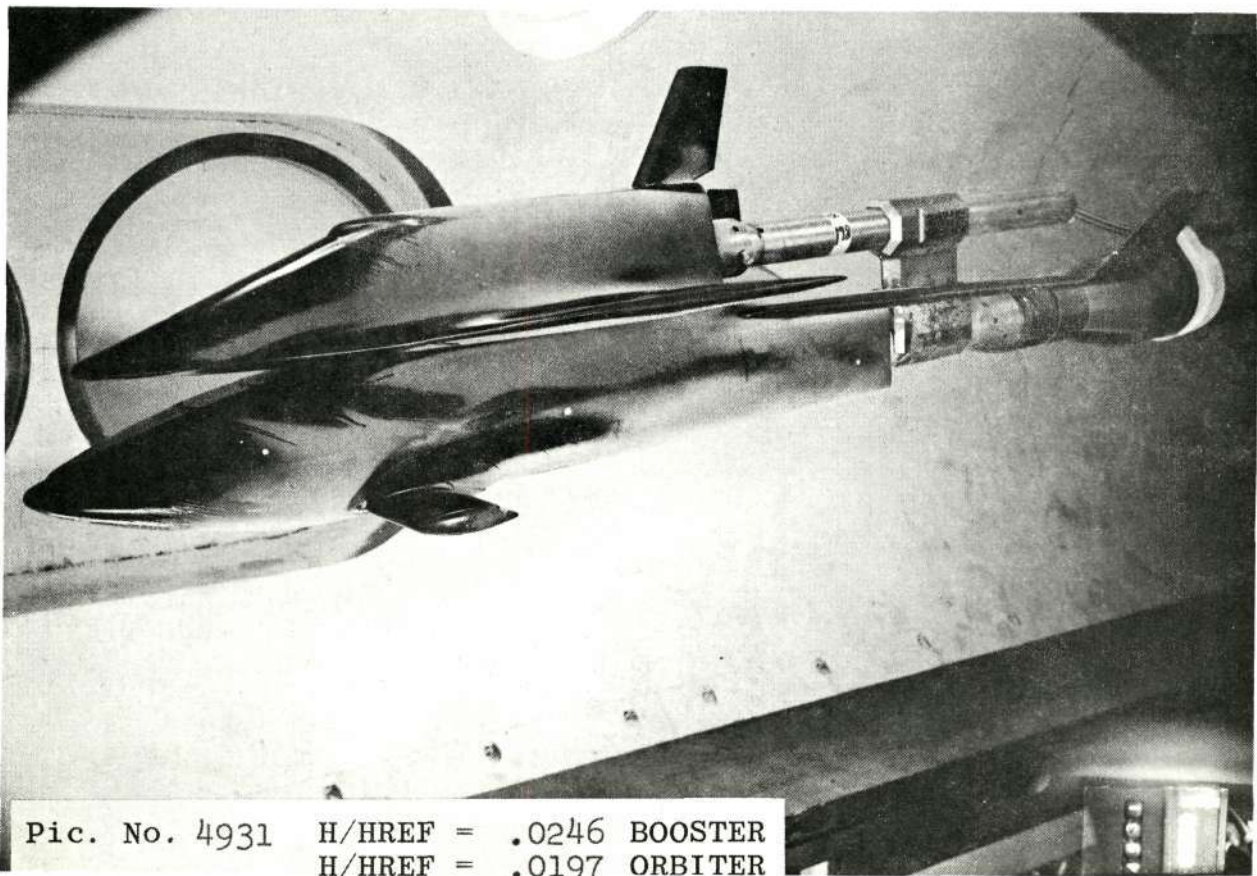




Pic. No. 4917

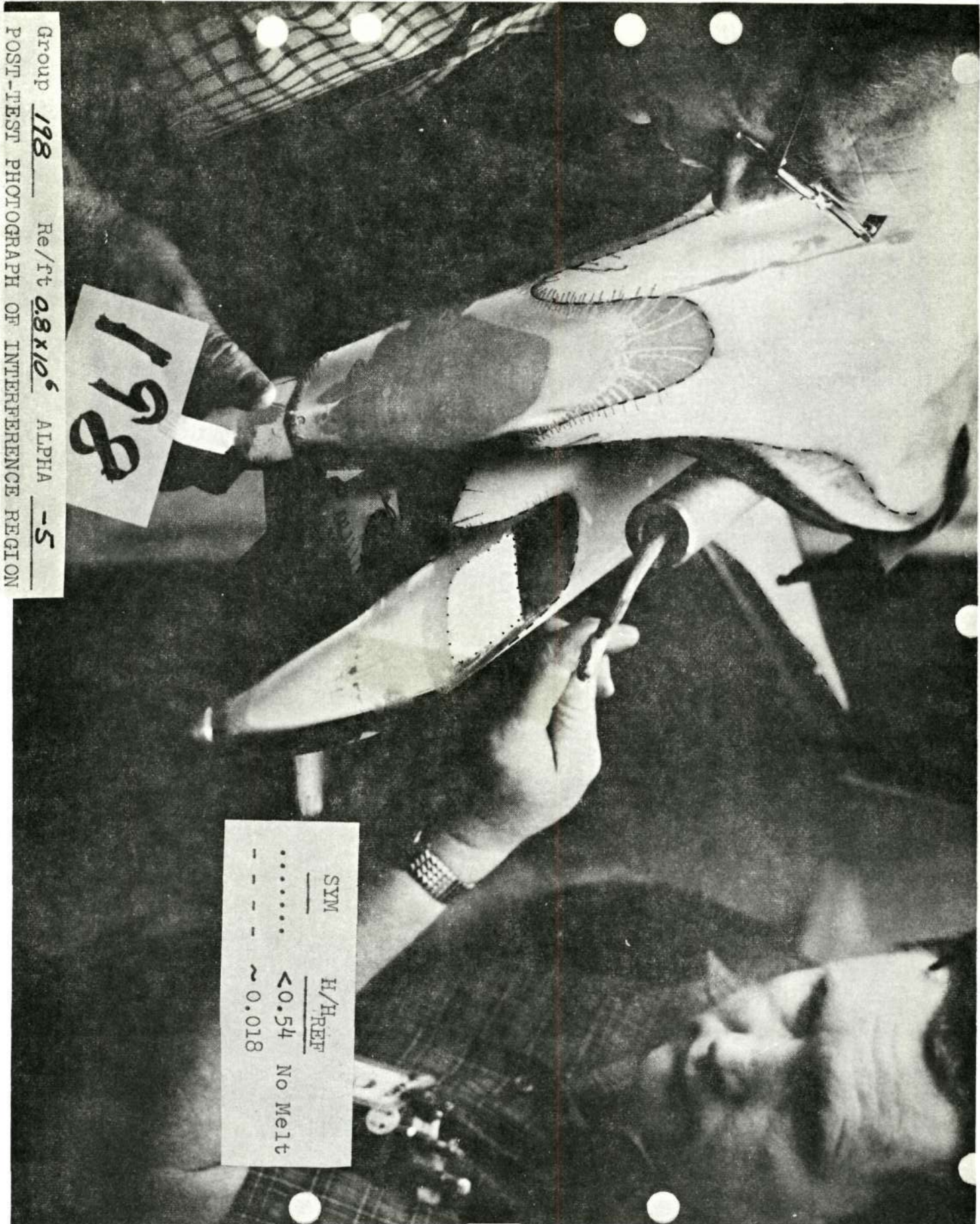
H/HREF = .0400 BOOSTER
H/HREF = .0319 ORBITER

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Pic. No. 4931

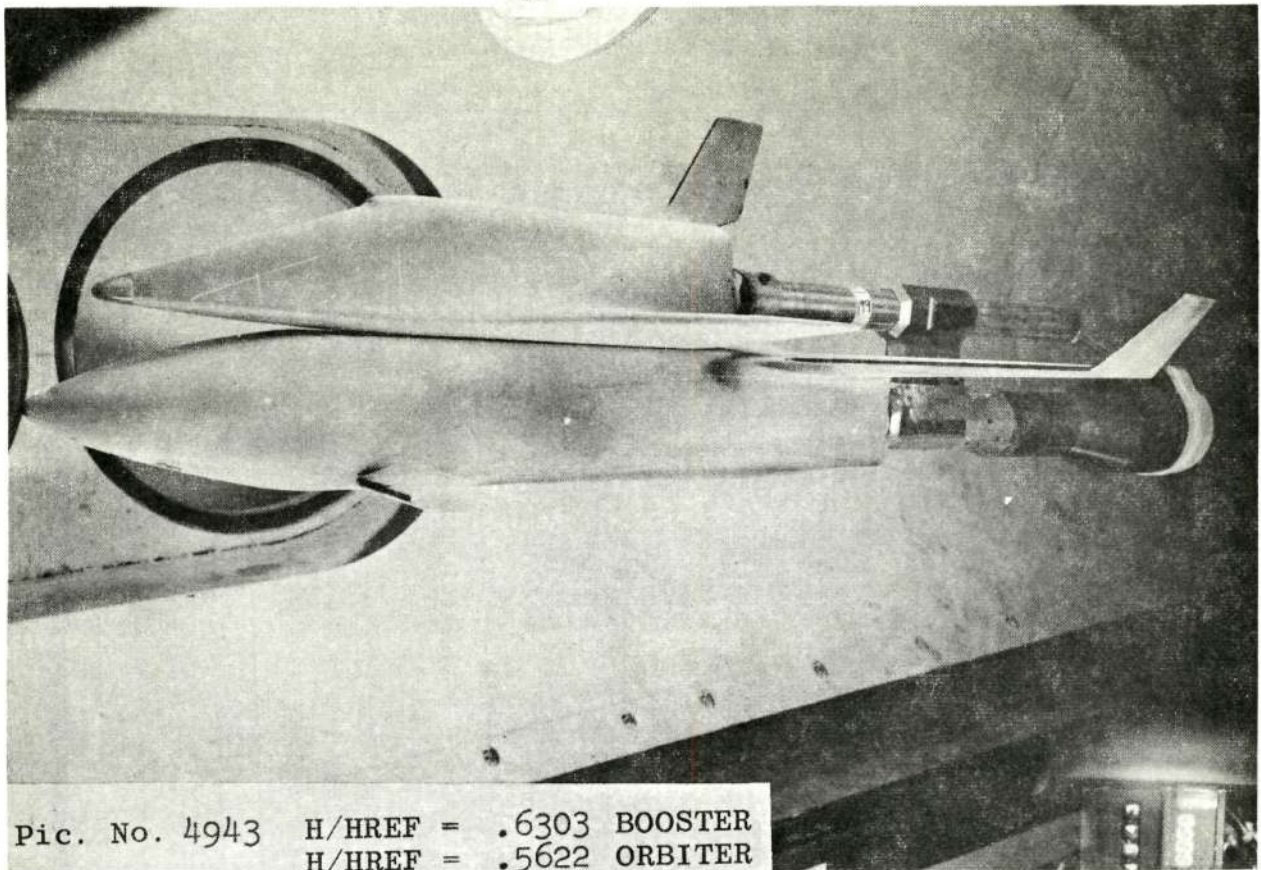
H/HREF = .0246 BOOSTER
H/HREF = .0197 ORBITER



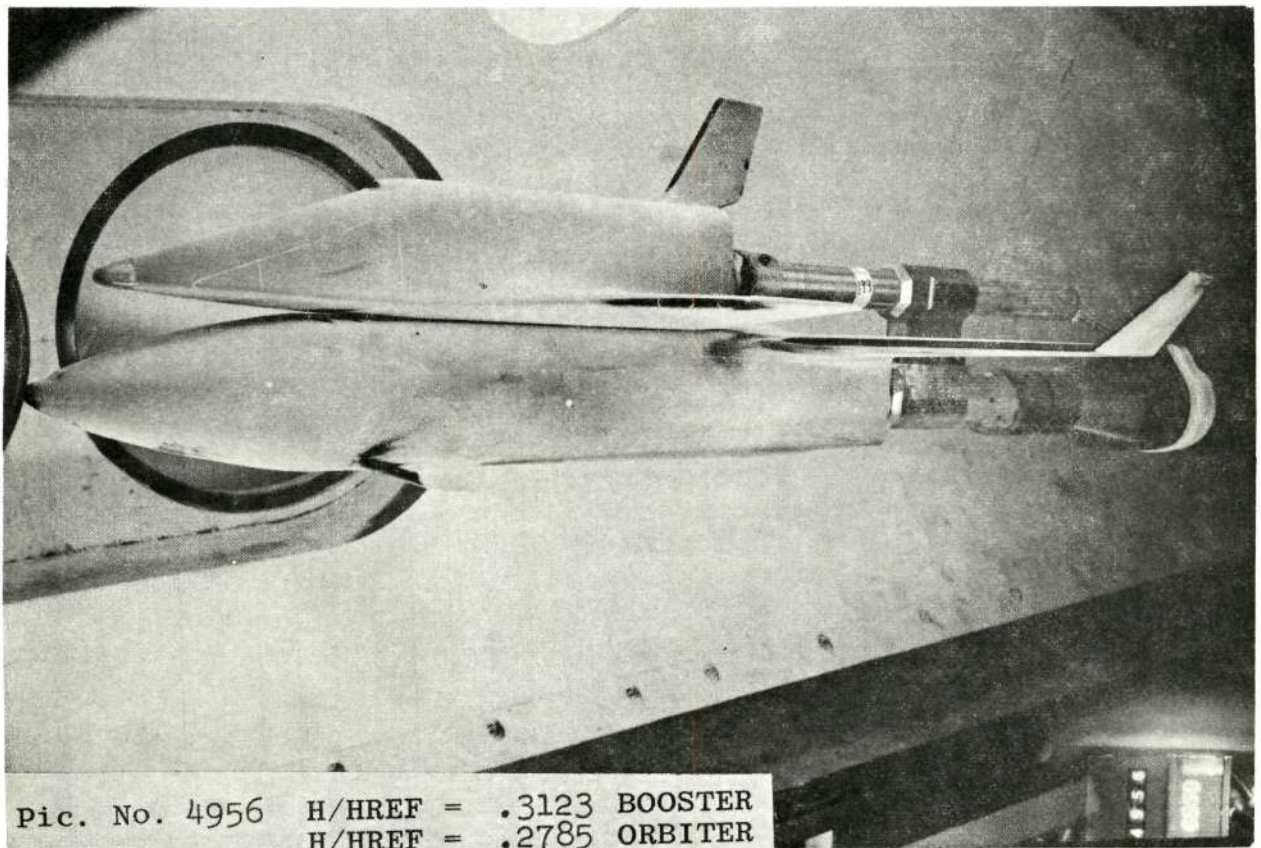
Group 198 Re/ft 0.8x10⁵ ALPHA -5
POST-TEST PHOTOGRAPH OF INTERFERENCE REGION

198

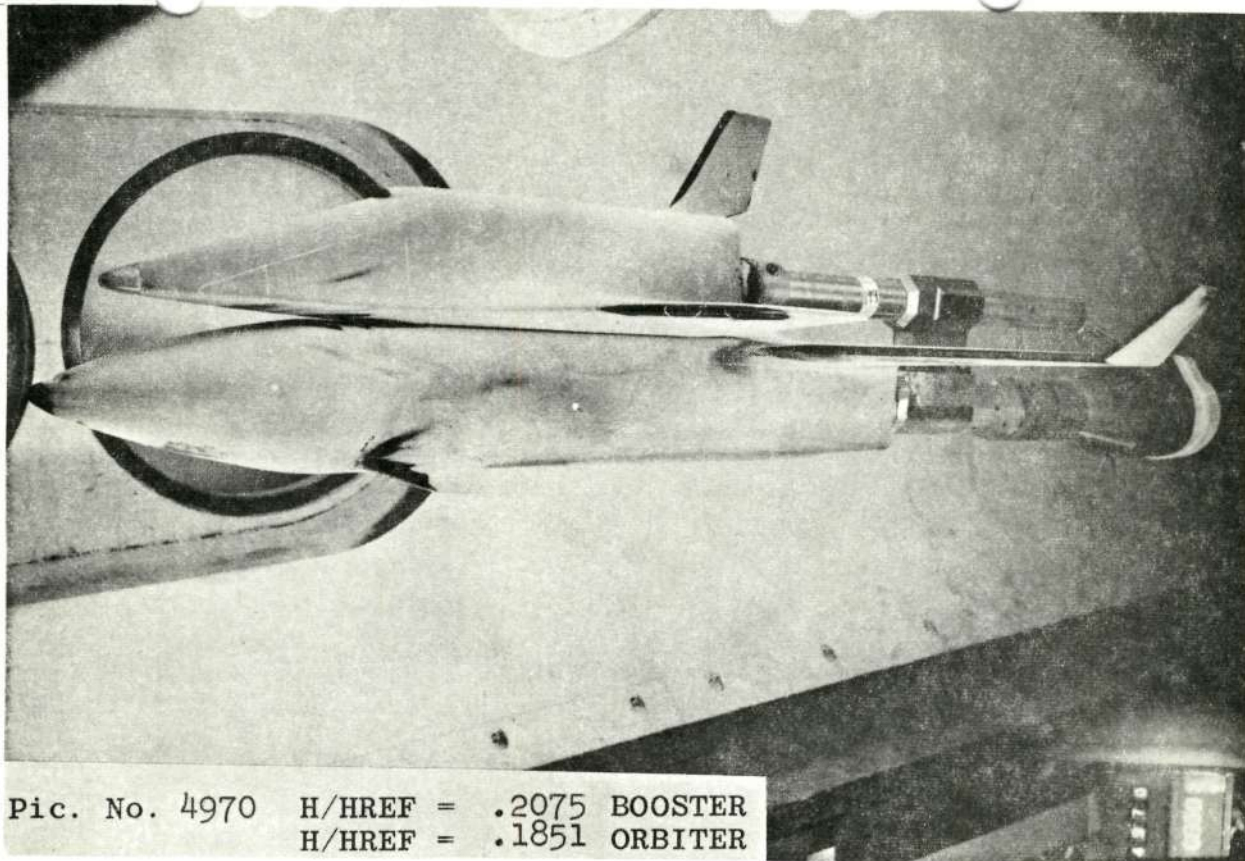
SYM	H/H _{REF}
.....	<0.54
- - - -	~ 0.018
	No Melt



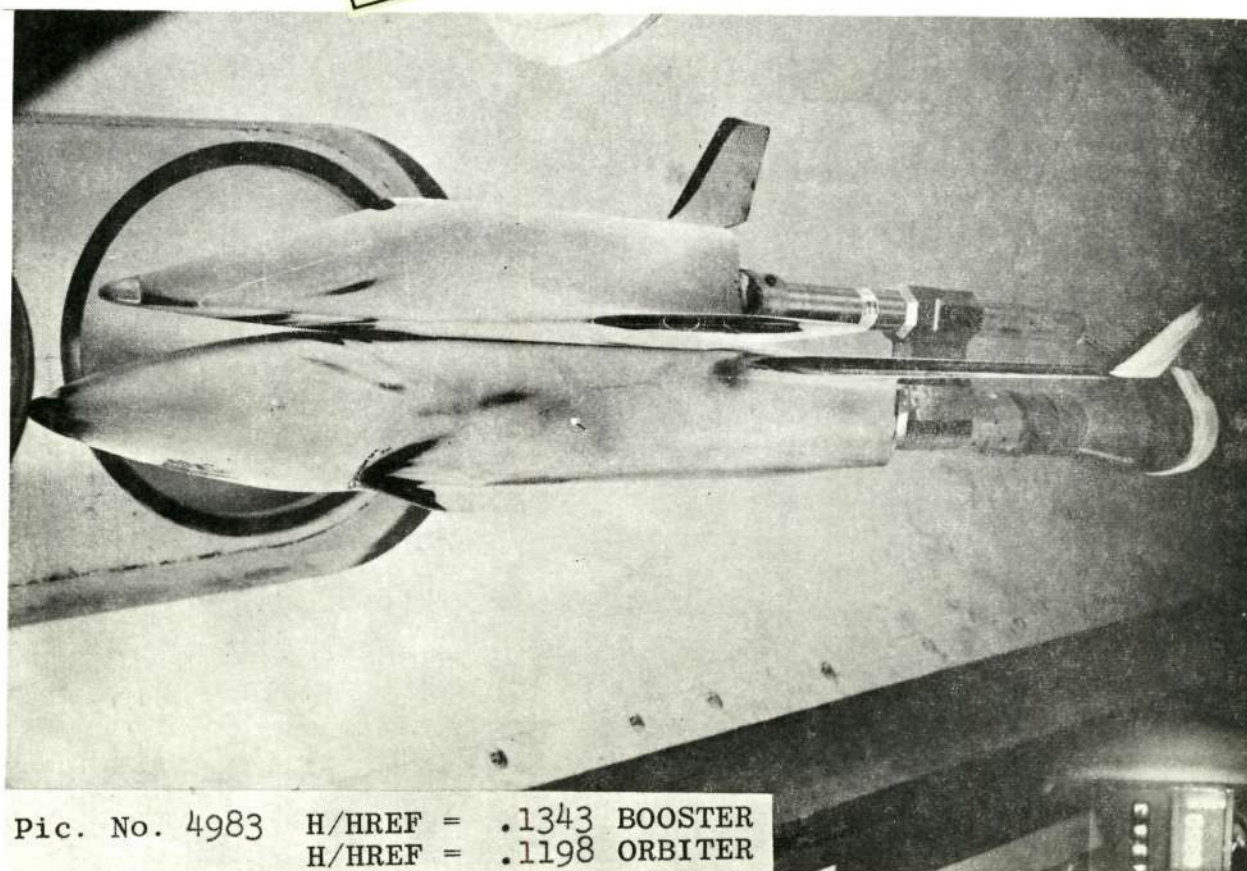
Pic. No. 4943 $H/HREF = .6303$ BOOSTER
 $H/HREF = .5622$ ORBITER

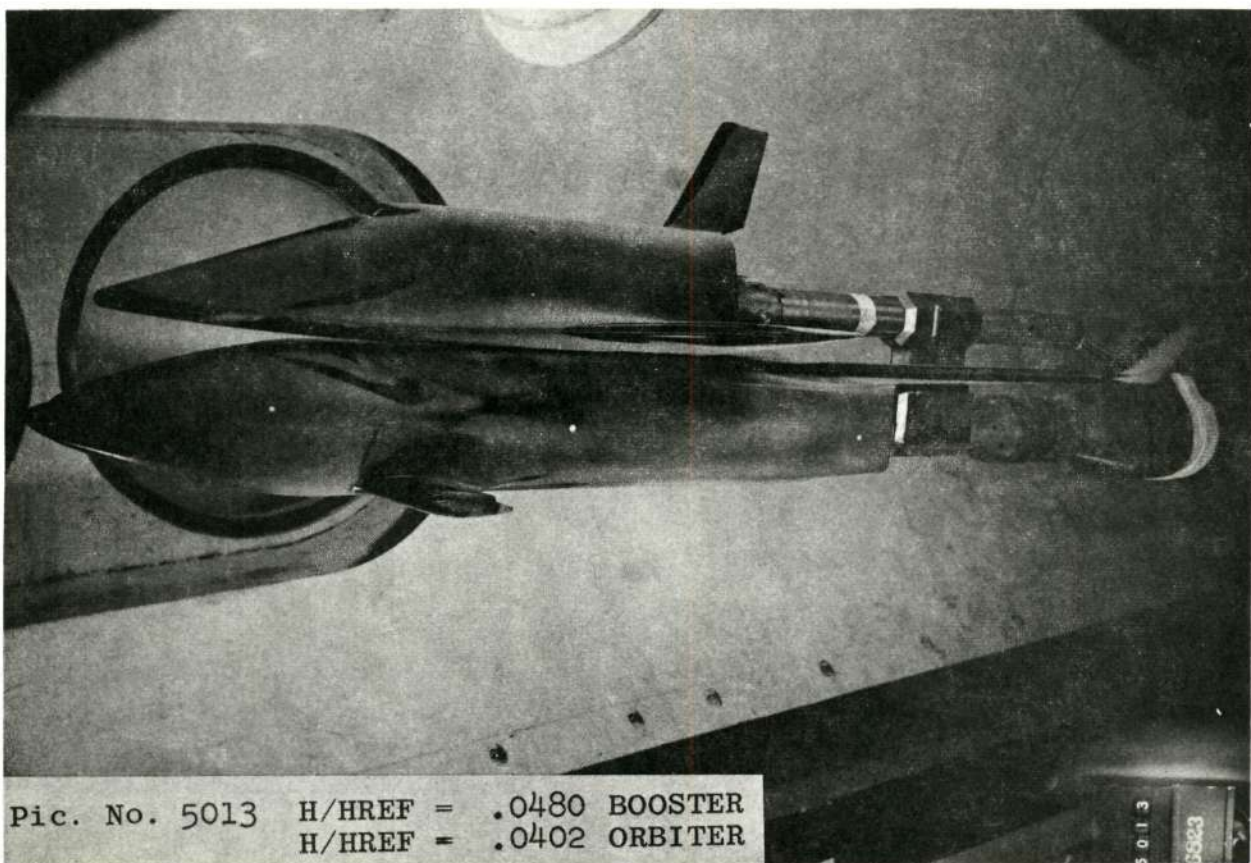
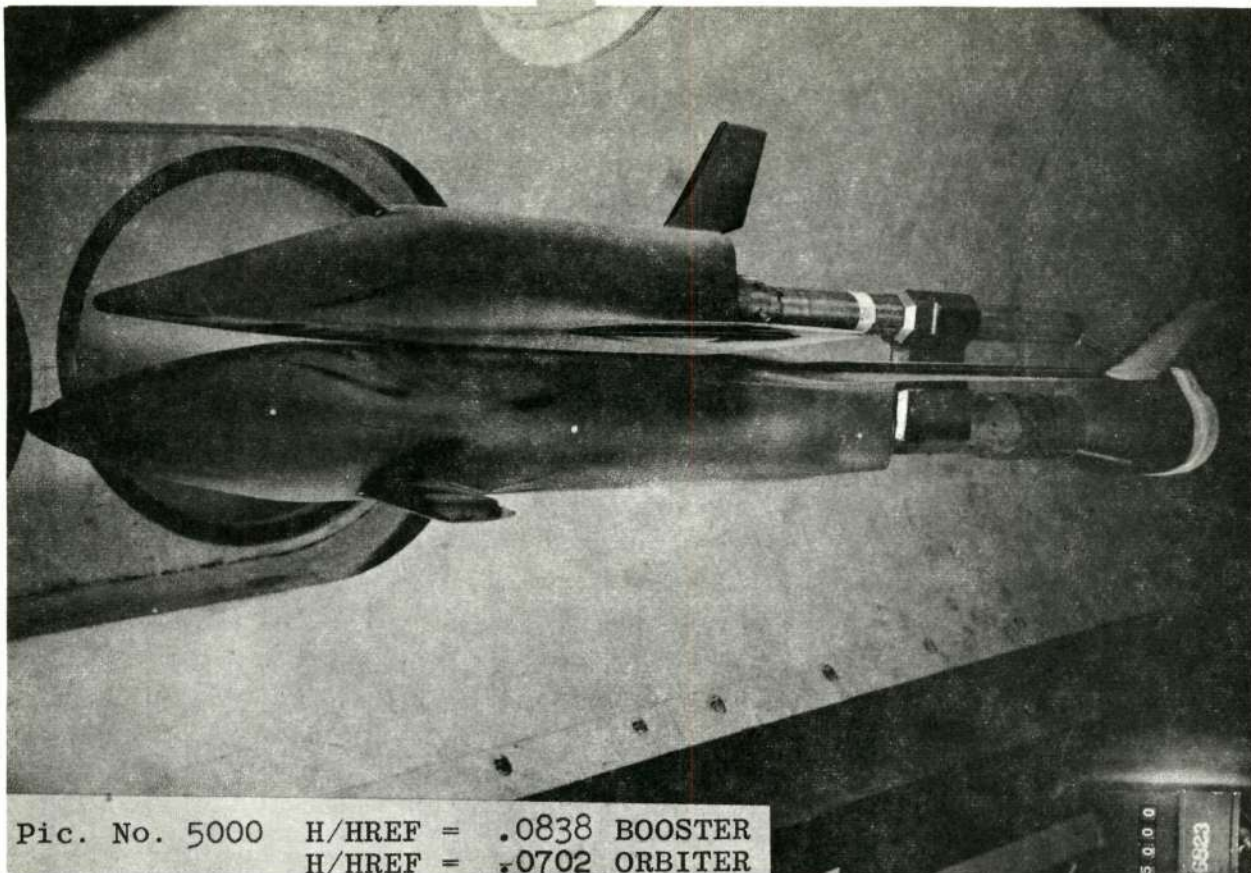


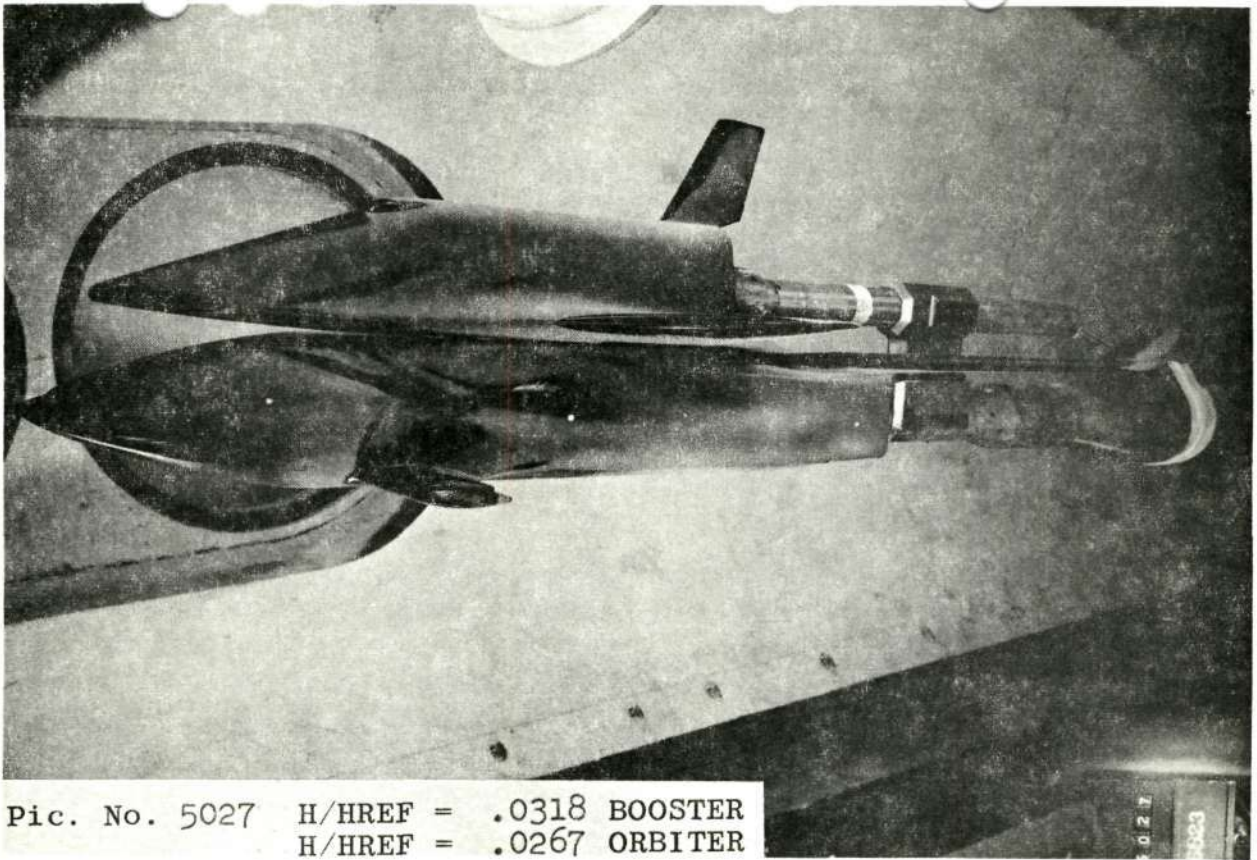
Pic. No. 4956 $H/HREF = .3123$ BOOSTER
 $H/HREF = .2785$ ORBITER



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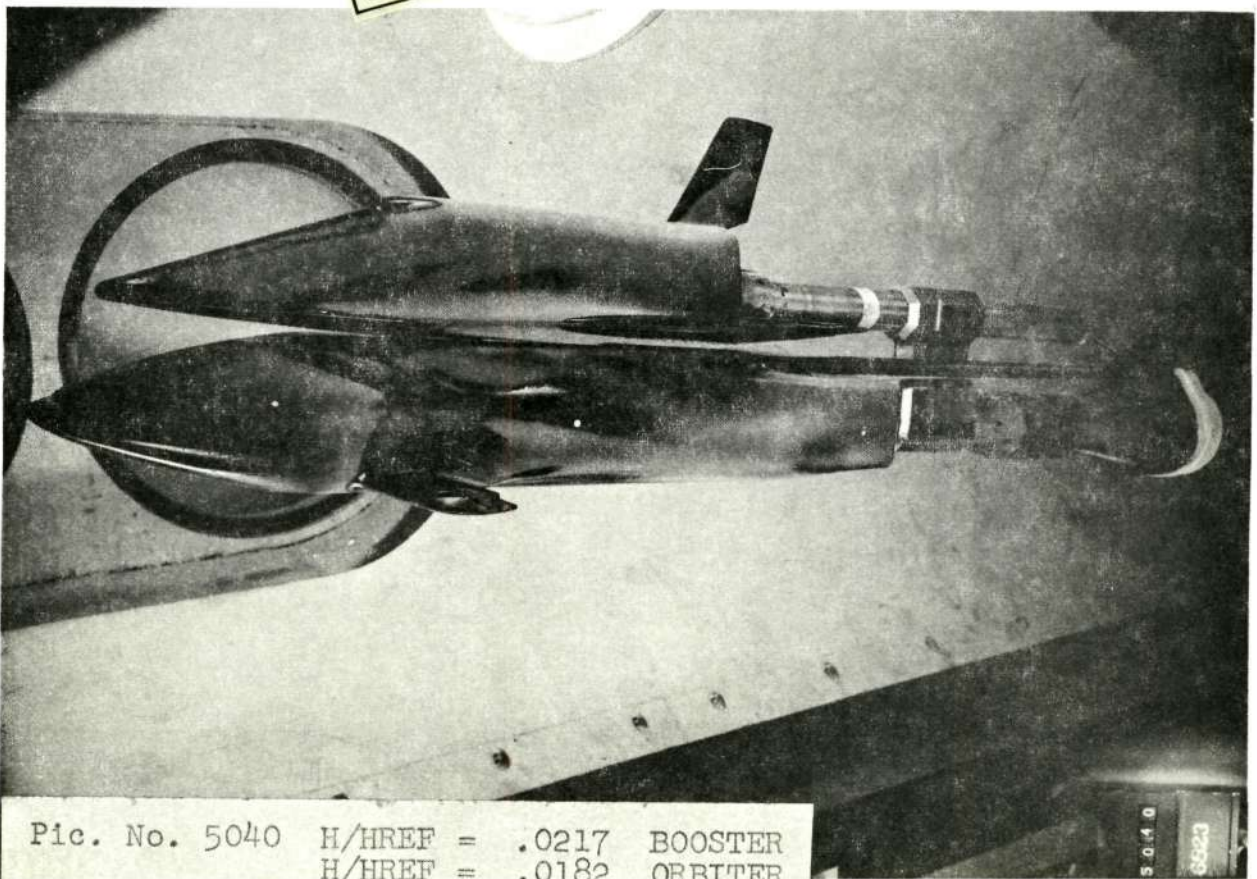




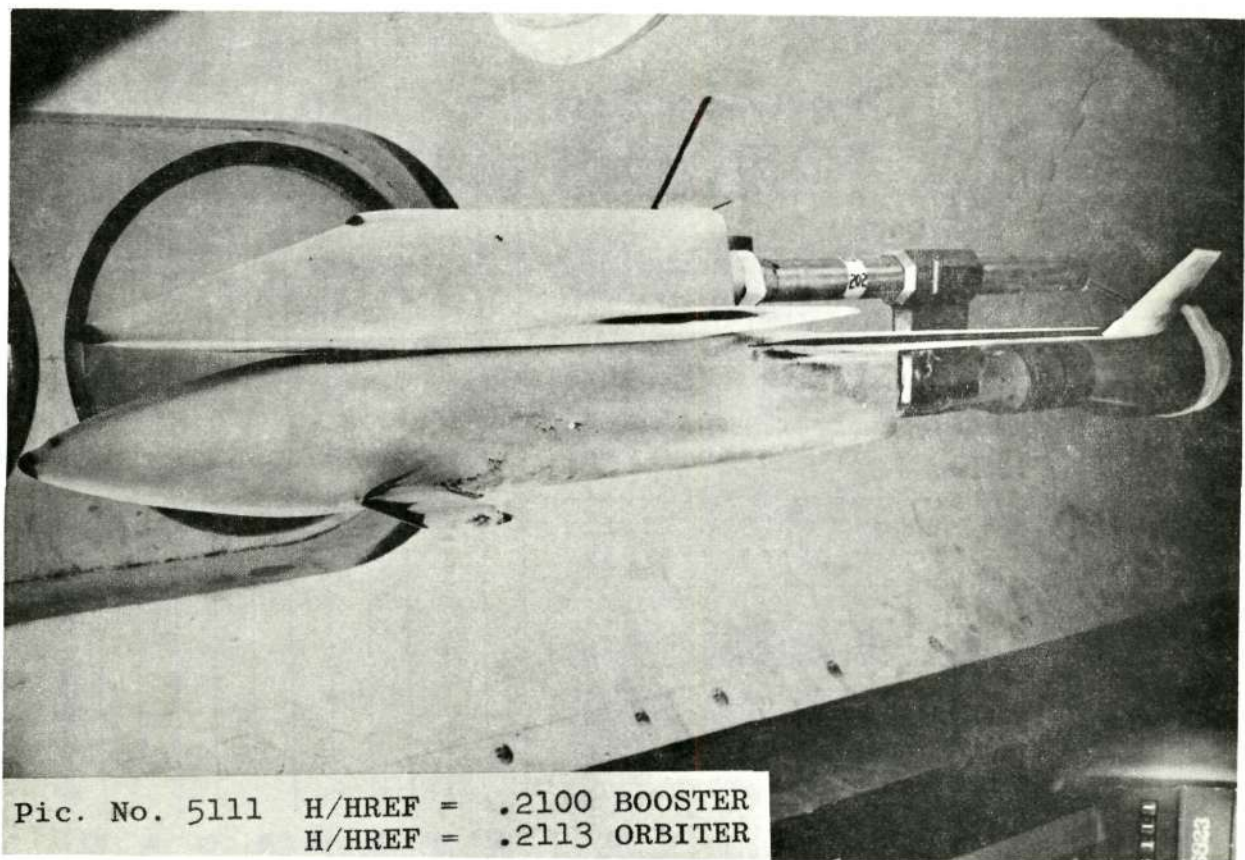
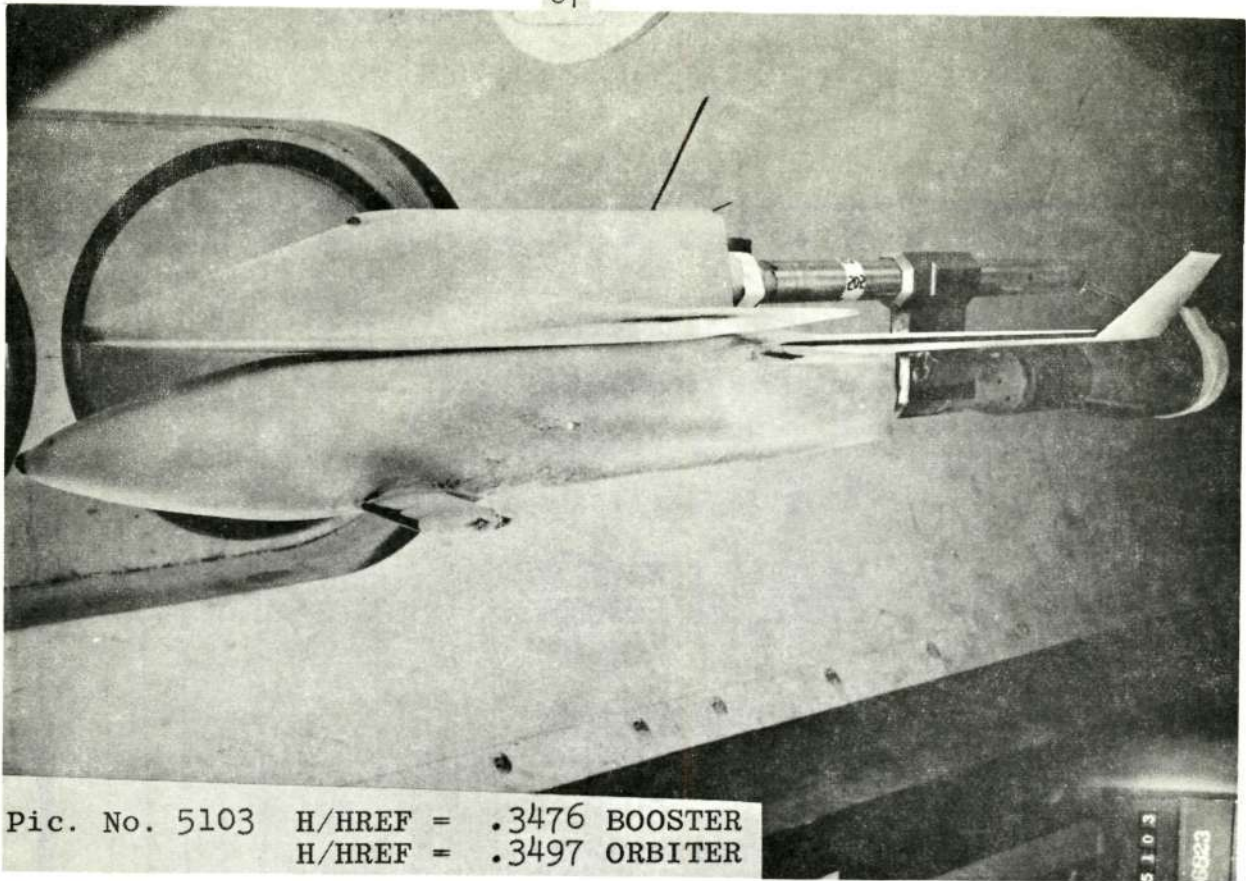


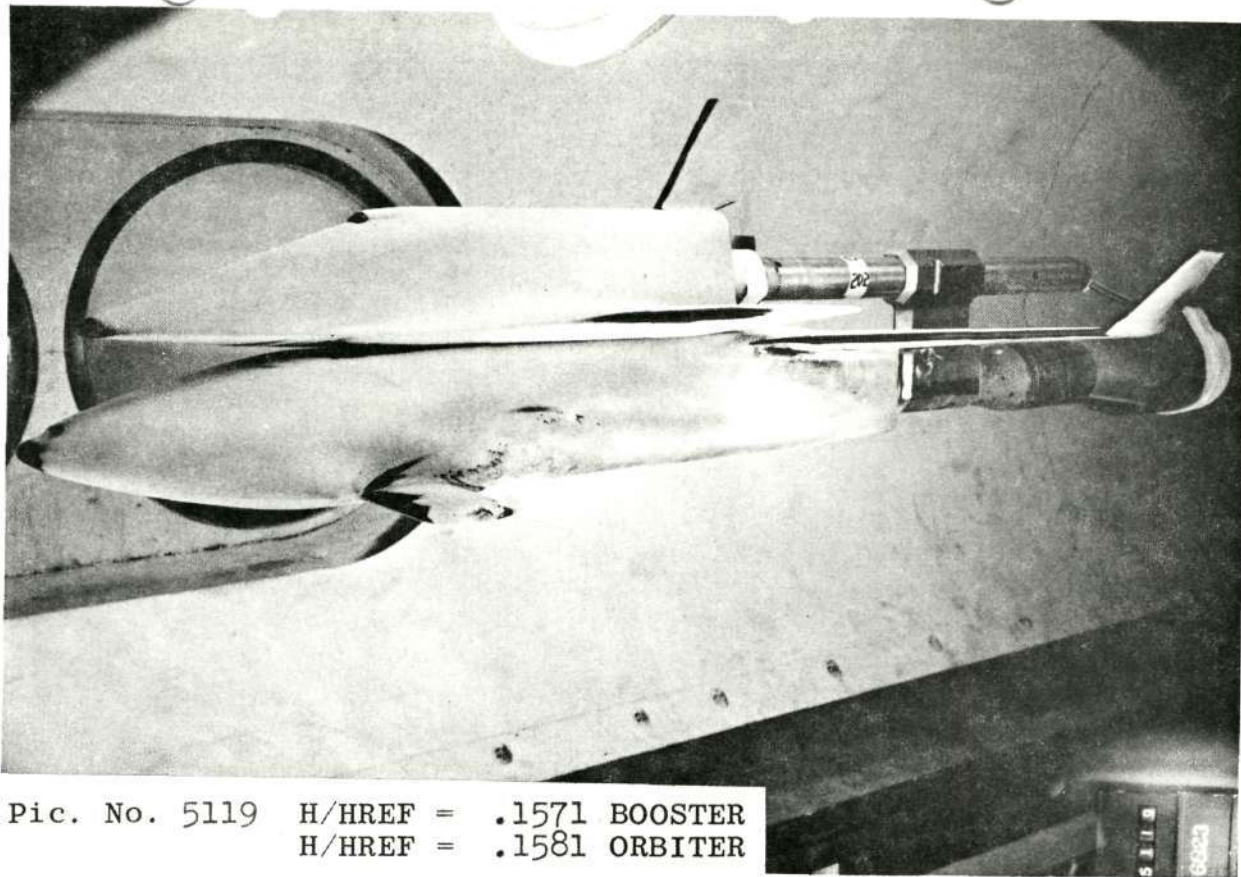
Pic. No. 5027 H/HREF = .0318 BOOSTER
H/HREF = .0267 ORBITER

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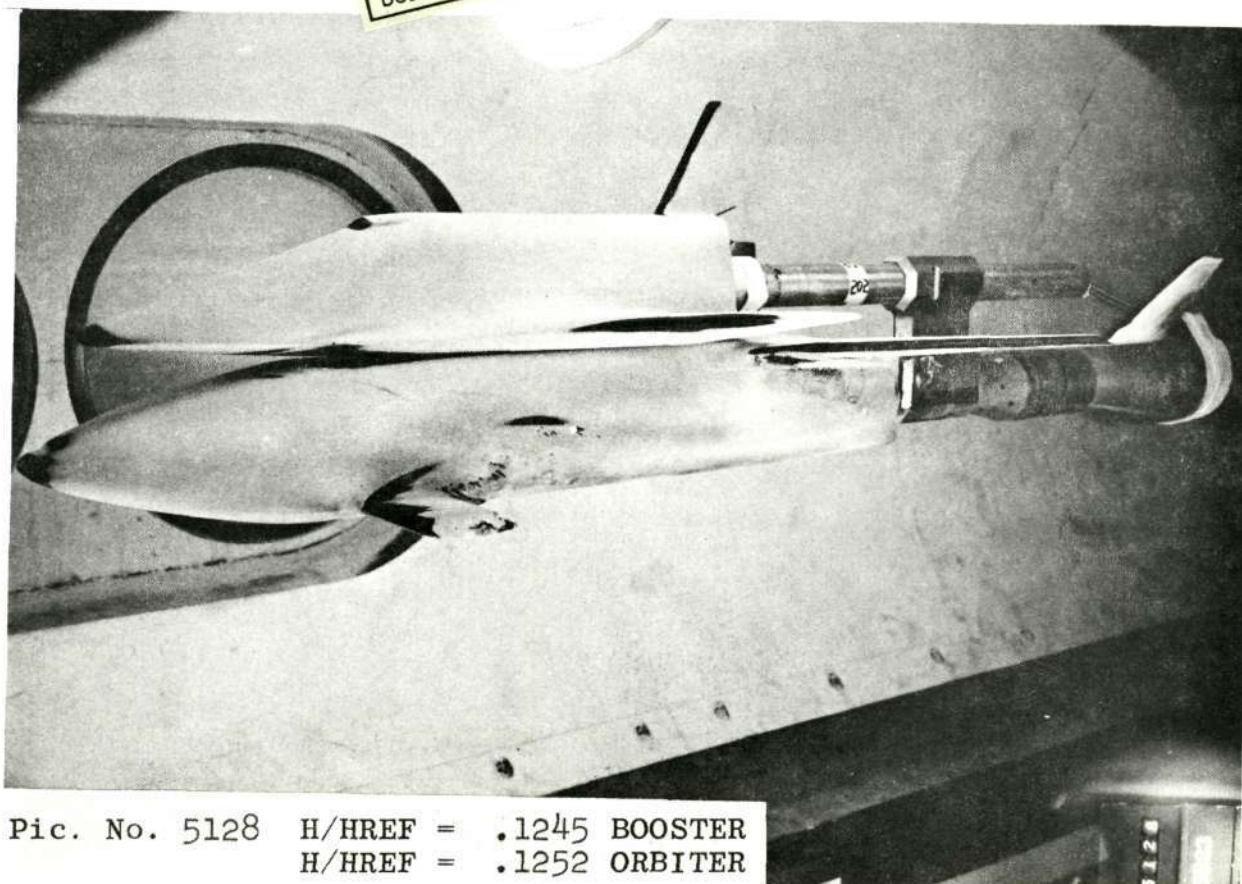
Pic. No. 5040 H/HREF = .0217 BOOSTER
H/HREF = .0182 ORBITER





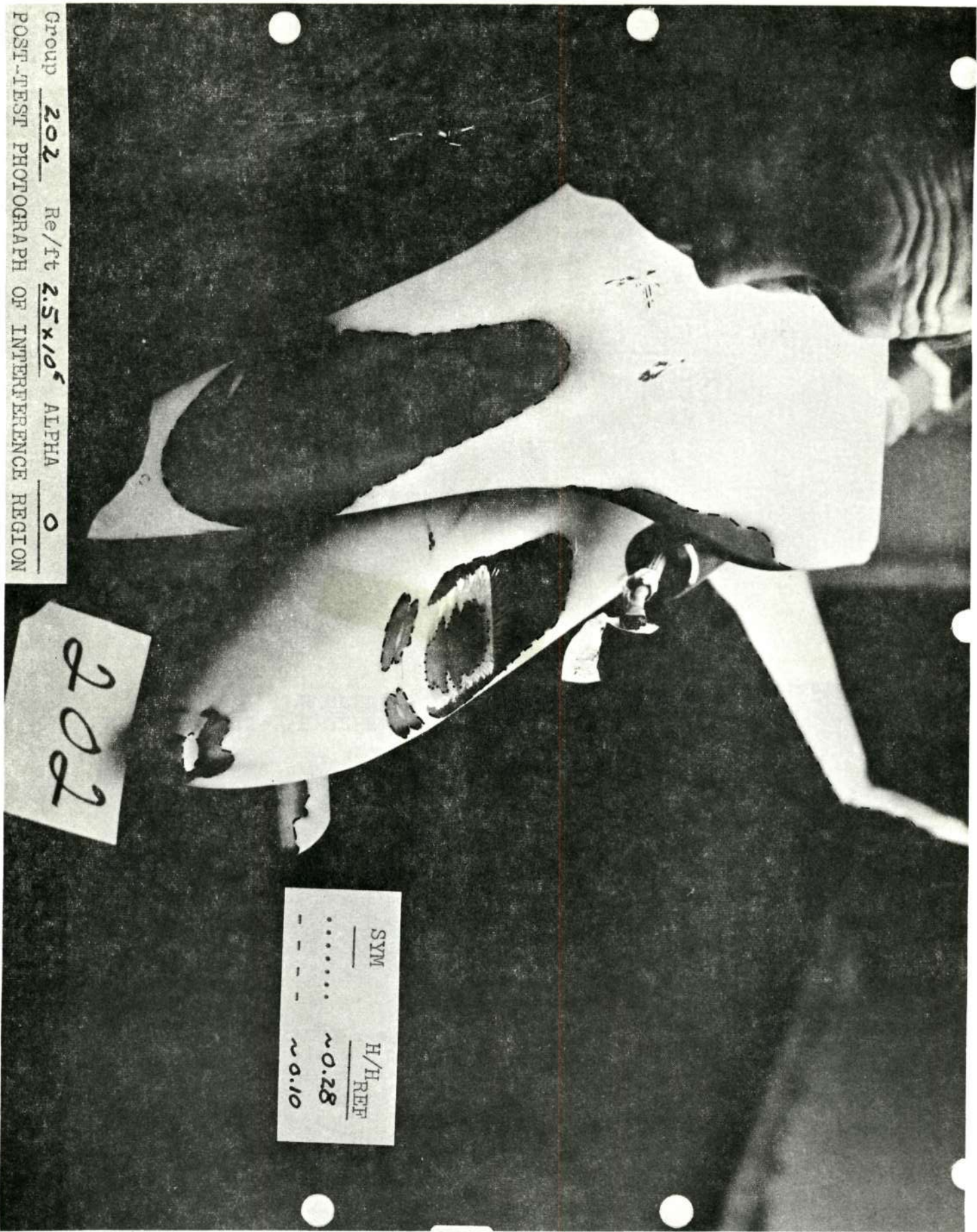
Pic. No. 5119 H/HREF = .1571 BOOSTER
 H/HREF = .1581 ORBITER

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Pic. No. 5128 H/HREF = .1245 BOOSTER
 H/HREF = .1252 ORBITER

Group 202 Re/ft 2.5x10⁶ ALPHA 0
 POST-TEST PHOTOGRAPH OF INTERFERENCE REGION



202

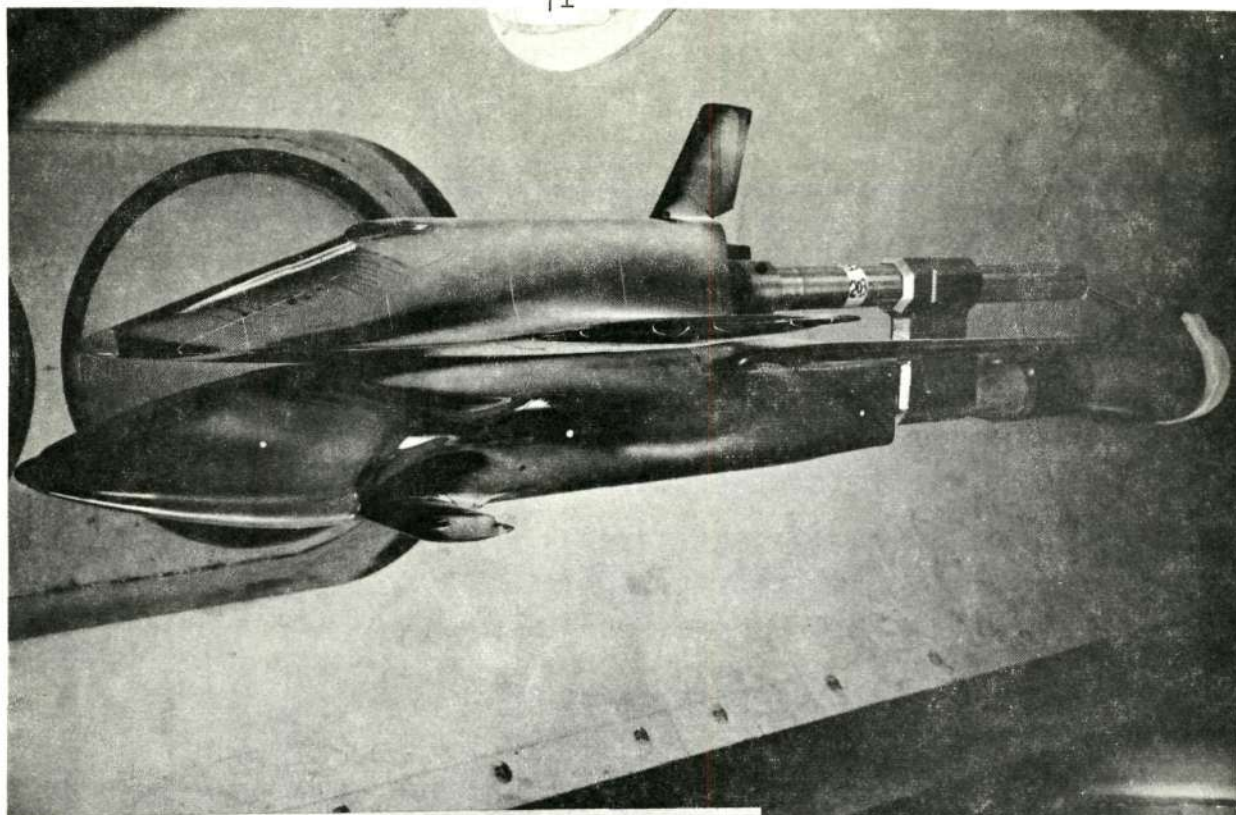
SYM	H/H _{REF}
.....	~0.28
---	~0.10

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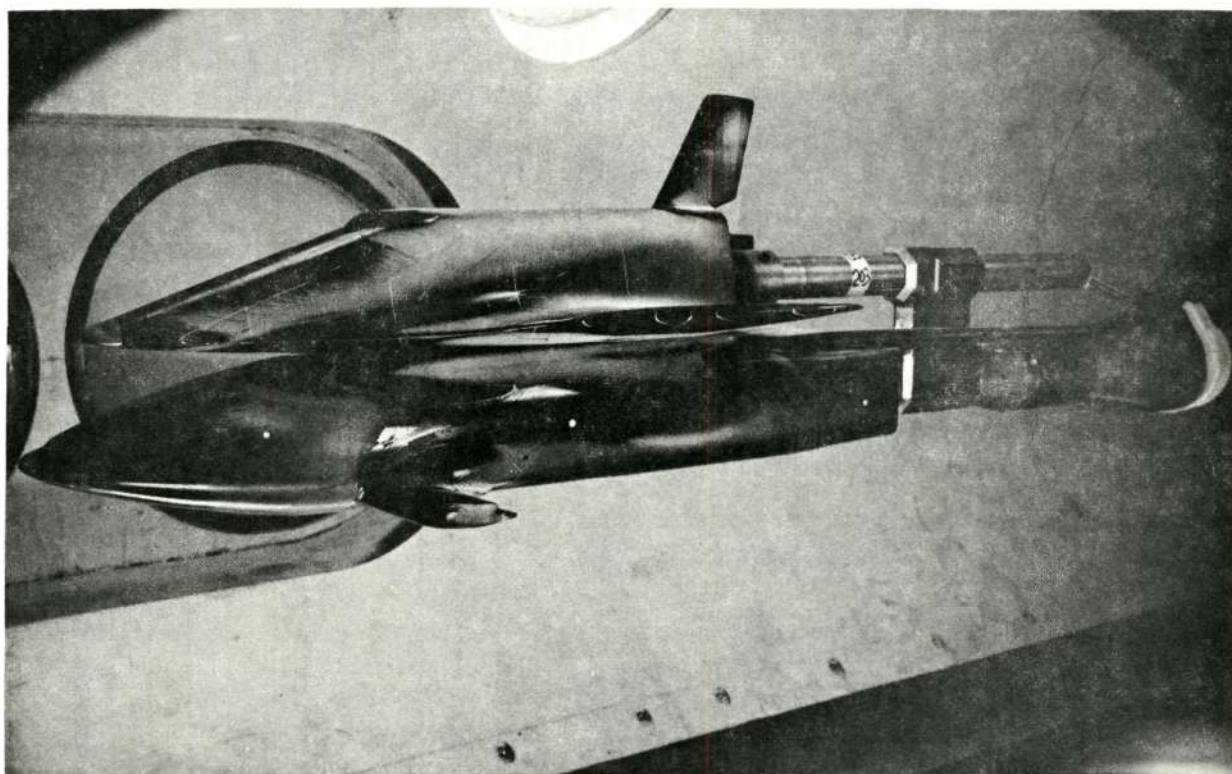
AFDC(ARNO, INC.) ARNOLO AFS, TENNESSEE
VON KARMAN GAS DYNAMICS FACILITY
50 INCH HYPERSONIC TUNNEL B
V11162

GROUP	CONFID	MODEL	WACV NO	PO PSIA	TO DEG R	ALPHA-DEG	ALPHA-SECTOR	ALPHA-DEG	ROLL-MODEL	YAW
203	1222	WACV-B-00C	R.08	549.15	1329	.03	.03	.03		
T-1NF P-1NF 0-1NF V-1NF QMO-1NF WU-1NF PE/FT WREF STREF (DEG R) (PSIA) (FT/SEC) (SLUGS/FT ³) (LB-SEC/FT ²) (FT/L) (R=.011FT) (R=.011FT) 96.3 .096 2.522 3066 4.985E-05 7.751E-08 2.43E 06 4.992E-02 3.290E-02 CAMERA PAINT TEMP (DEG F) INITIAL TEMP (DEG F) SQUARE ROOT (IN/SEC) (DEG F) 124 SIDE(US) 506 AVERAGE TV = 84 (R) -0.00815 SQUARE ROOT DEL TIME) = 0.11 SIDE(LS) 500 AVERAGE TV = 88 (C)										

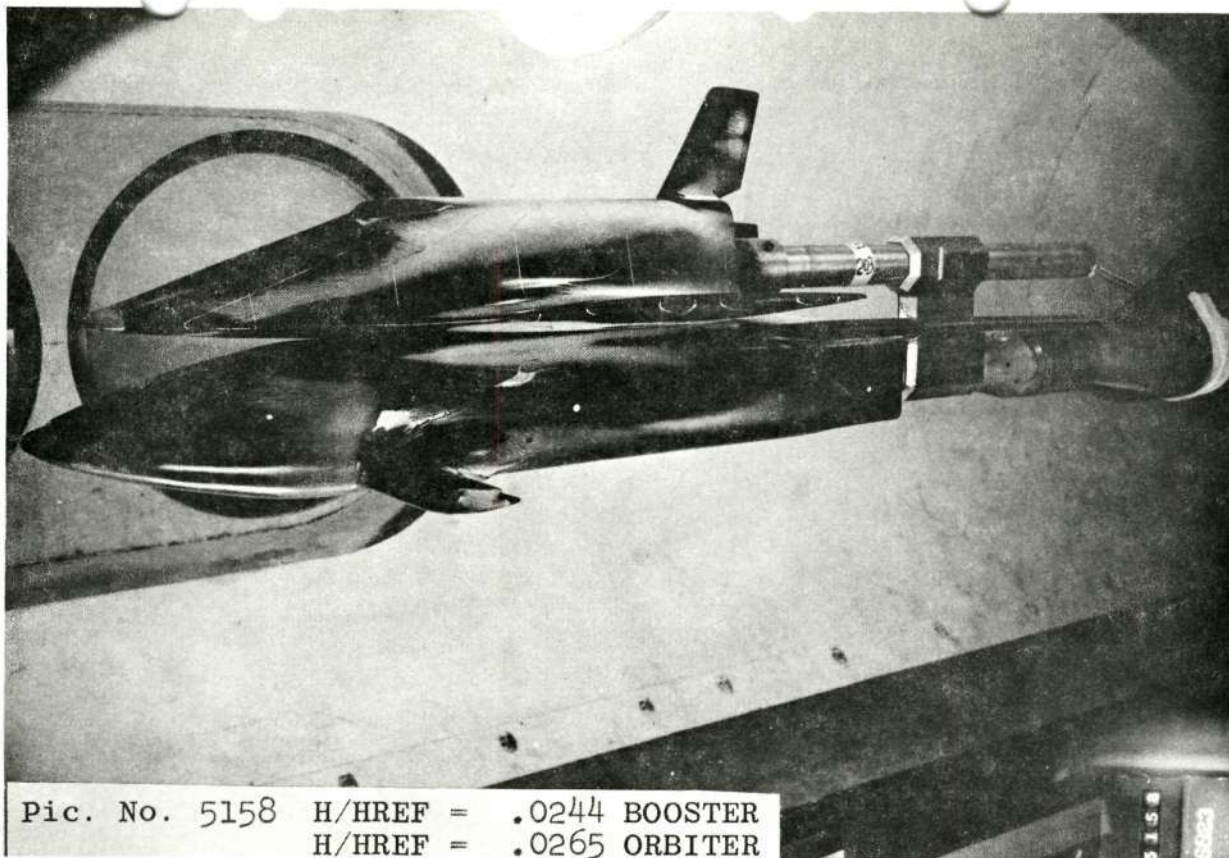
PIC MC	TIME DELTIME	M(TO)	M(TO)/MREF	M(-910)	M(-910)/MREF	M(-8510)	M(-8510)/MREF	ST(10)	MODEL TEMP F
US 5143 (1500)	4.20	3.16	0.466E-02	.9335	6.952E-02	1.3927	9.332E-02	1.8605	3.018E-02
US 5142 (1125)	4.20	3.16	8.262E-03	.0525	3.182E-03	.0638	3.565E-03	.0714	1.730E-02
US 5143 (1500)	4.20	3.16	R 4.63E-02	.9265	6.901E-02	1.3824	9.264E-02	1.8558	2.995E-02
US 5142 (1125)	4.20	3.16	0.2.04E-03	.0568	3.444E-03	.0690	3.861E-03	.0773	1.675E-02
US 5150 (1500)	7.90	6.06	0.2.04E-02	.5891	4.387E-02	.8768	5.889E-02	1.1797	1.904E-02
US 5150 (1125)	7.90	6.06	R 1.65E-03	.0371	2.009E-03	.0402	2.230E-03	.0451	1.092E-02
US 5150 (1500)	7.90	6.06	8.2.92E-02	.5847	4.355E-02	.8723	5.846E-02	1.1710	1.090E-02
US 5150 (1125)	7.90	6.06	0.2.17E-03	.0353	2.174E-03	.0435	2.436E-03	.0488	1.183E-02
US 5150 (1500)	12.10	11.04	0.2.17E-02	.4347	3.236E-02	.6406	4.344E-02	.8705	1.405E-02
US 5150 (1125)	12.10	11.04	R 1.22E-03	.0244	1.481E-03	.0297	1.659E-03	.0372	8.957E-04
US 5150 (1500)	12.10	11.04	8.2.15E-02	.4314	3.212E-02	.6437	4.312E-02	.8641	1.395E-02
US 5150 (1125)	12.10	11.04	0.1.32E-03	.0265	1.603E-03	.0321	1.791E-03	.0390	8.731E-04
US 5165 (1500)	16.00	14.94	0.1.37E-02	.3542	2.638E-02	.5264	3.541E-02	.7004	1.145E-02
US 5165 (1125)	16.00	14.94	R 9.03E-04	.0199	1.700E-03	.0242	1.353E-03	.0371	6.564E-04
US 5165 (1500)	16.00	14.94	8.1.75E-02	.3516	2.610E-02	.5245	3.515E-02	.7041	1.136E-02
US 5165 (1125)	16.00	14.94	0.1.06E-03	.0216	1.307E-03	.0262	1.465E-03	.0293	7.113E-04



Pic. No. 5143 H/HREF = .0525 BOOSTER
H/HREF = .0568 ORBITER

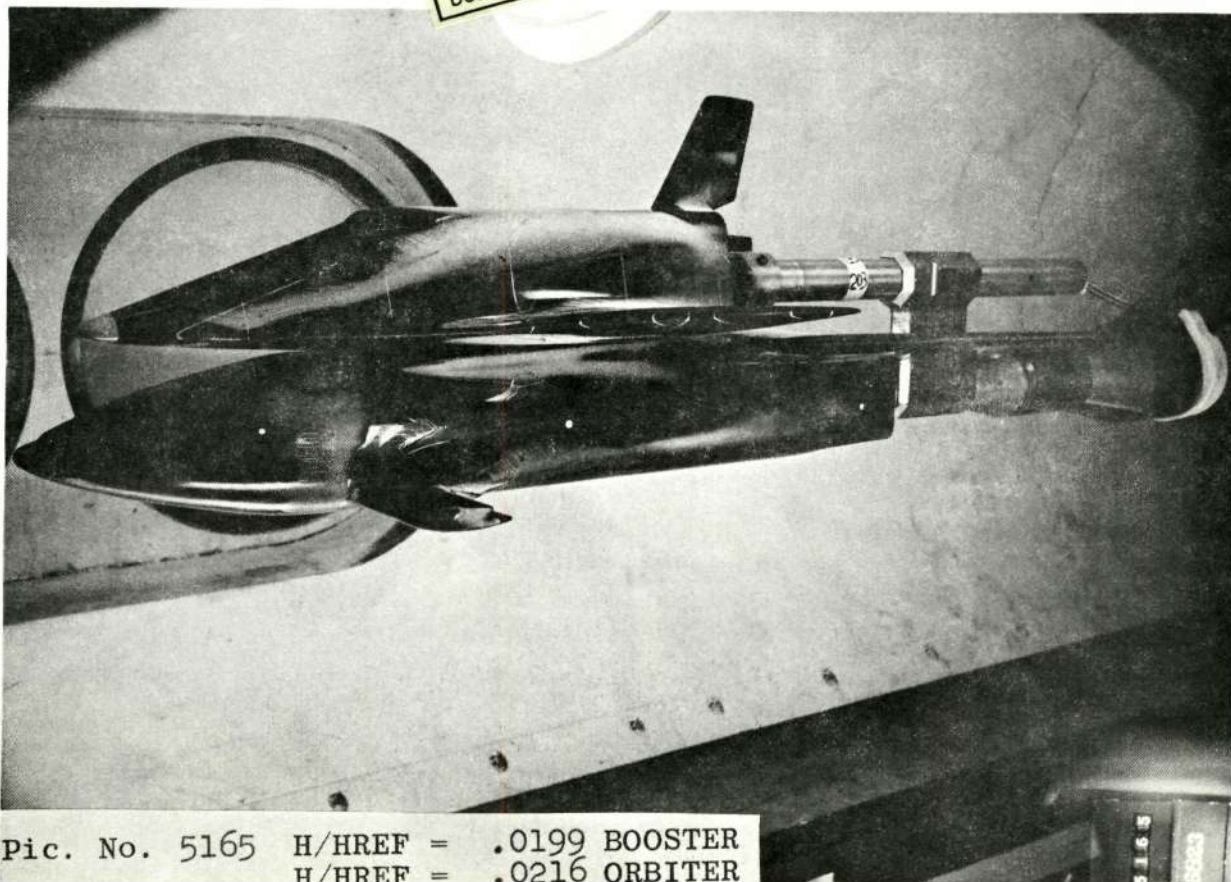


Pic. No. 5150 H/HREF = .0331 BOOSTER
H/HREF = .0359 ORBITER

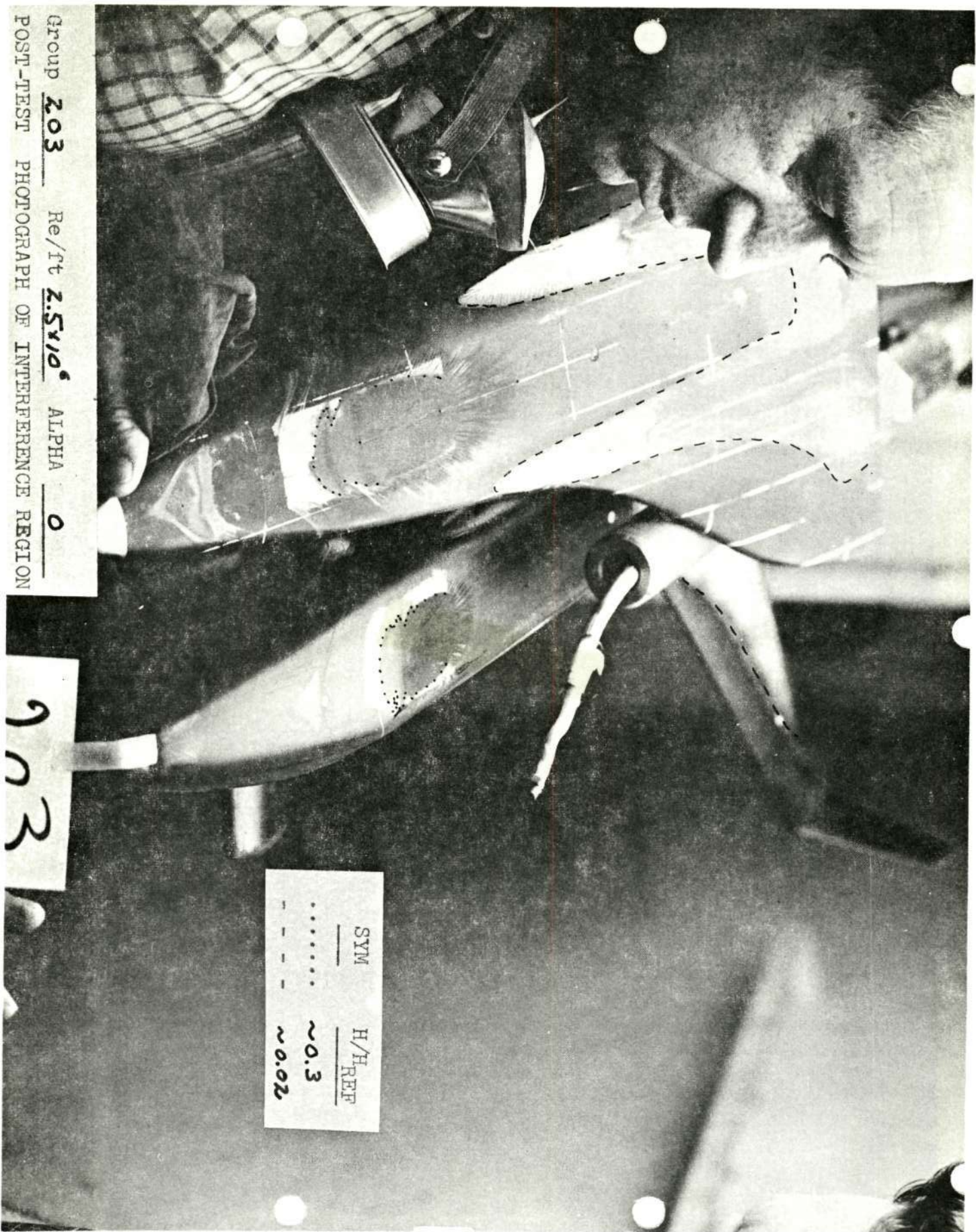


Pic. No. 5158 H/HREF = .0244 BOOSTER
H/HREF = .0265 ORBITER

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Pic. No. 5165 H/HREF = .0199 BOOSTER
H/HREF = .0216 ORBITER



Group 203 Re/ft 2.5x10⁶ ALPHA 0
POST-TEST PHOTOGRAPH OF INTERFERENCE REGION

203

SYM	H/H _{REF}
.....	~0.3
---	~0.02

50 INCH HIPERSUMIC JOURNAL 8
V11162

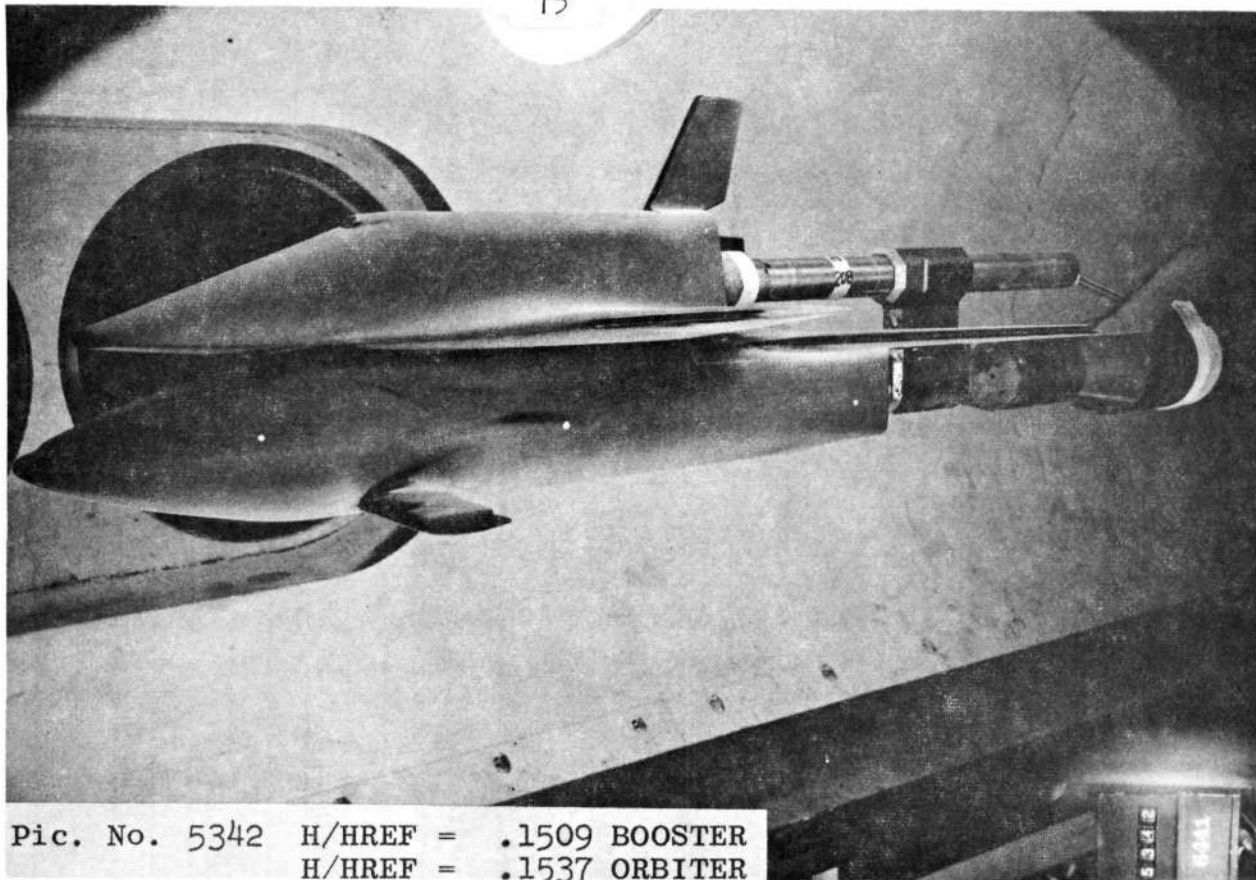
GROUP	CONFIG	MODEL	MACH NO	PO PSIA	TO DEG F	ALPHA-VELOC	ALPHA-SECTOR	ALPHA-PREBEND	ROLL-MODEL	YAW-MODEL
209	3221	PDAC-B-DUC	8.00	555.0	1327	0	0	0	0	0

[illegible]

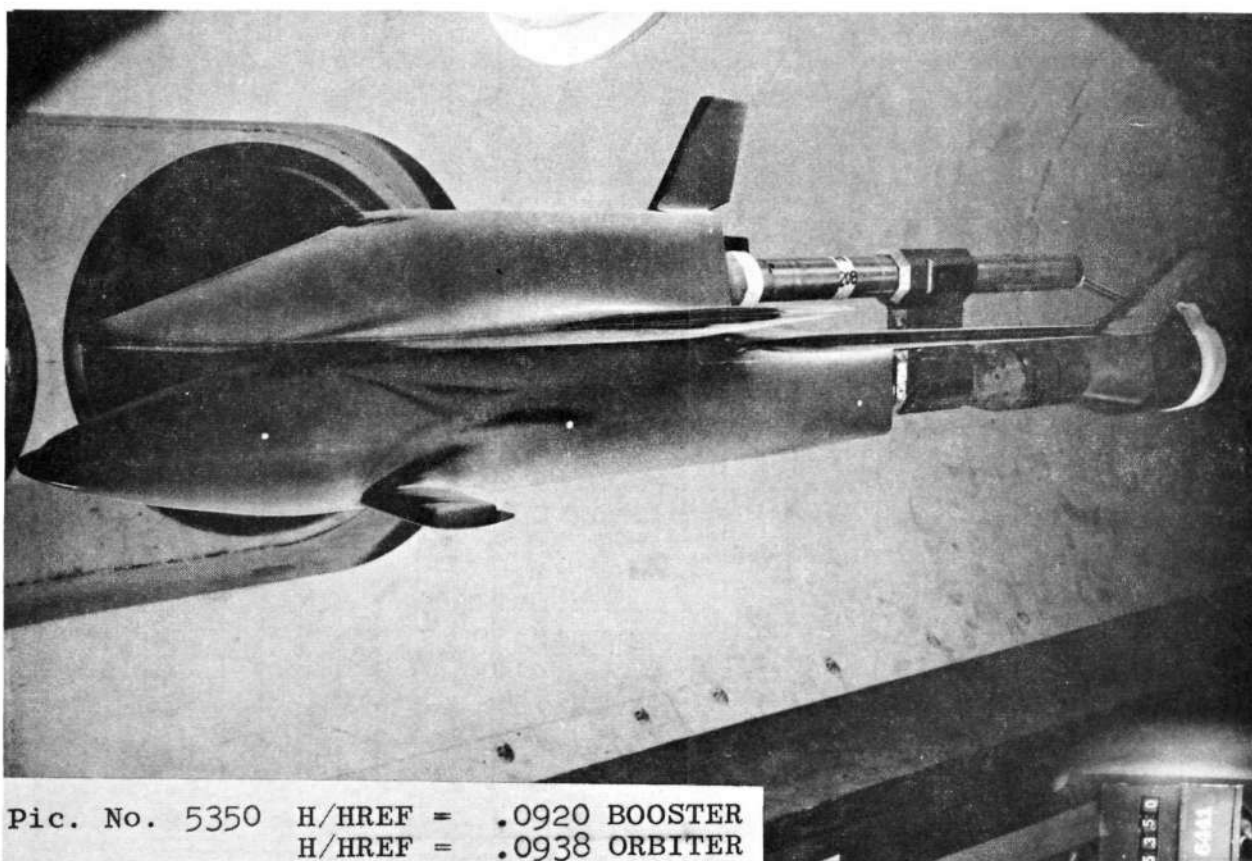
SICE(US)	200	AVERAGE IN = 89 (2)
SICE(ILS)	200	AVERAGE IN = 87 (0)

-008(SQUARE ROUT DEL TIME) • 0.11

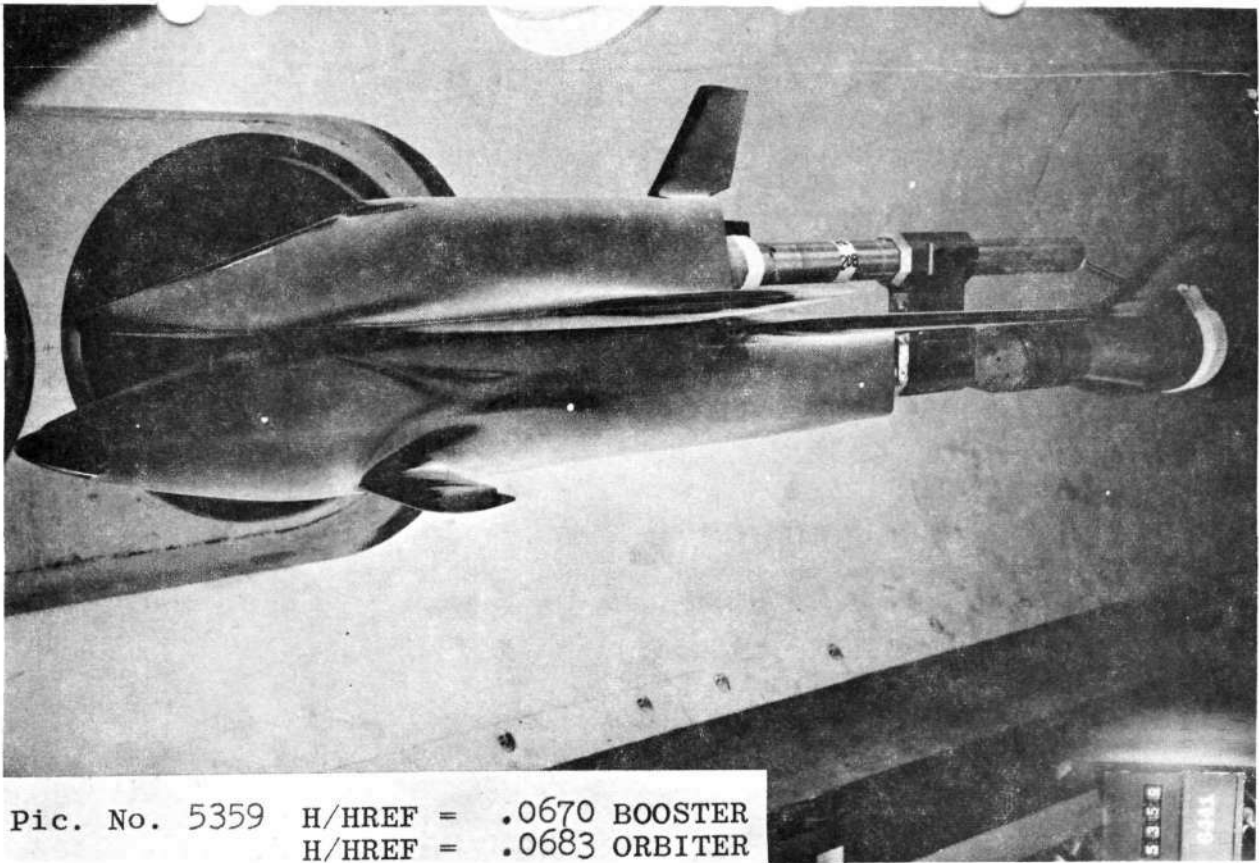
[illegible]



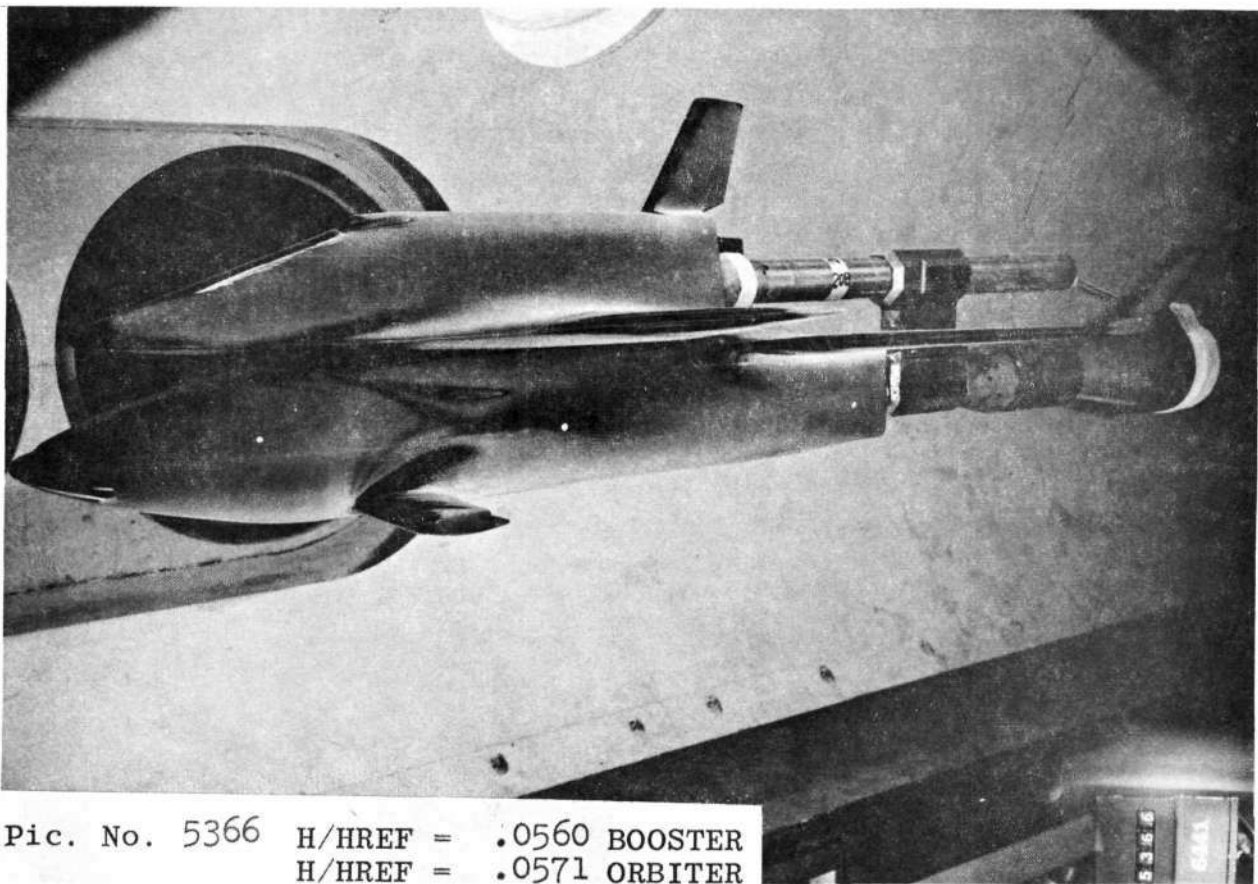
Pic. No. 5342 H/HREF = .1509 BOOSTER
H/HREF = .1537 ORBITER



Pic. No. 5350 H/HREF = .0920 BOOSTER
H/HREF = .0938 ORBITER



Pic. No. 5359 H/HREF = .0670 BOOSTER
H/HREF = .0683 ORBITER



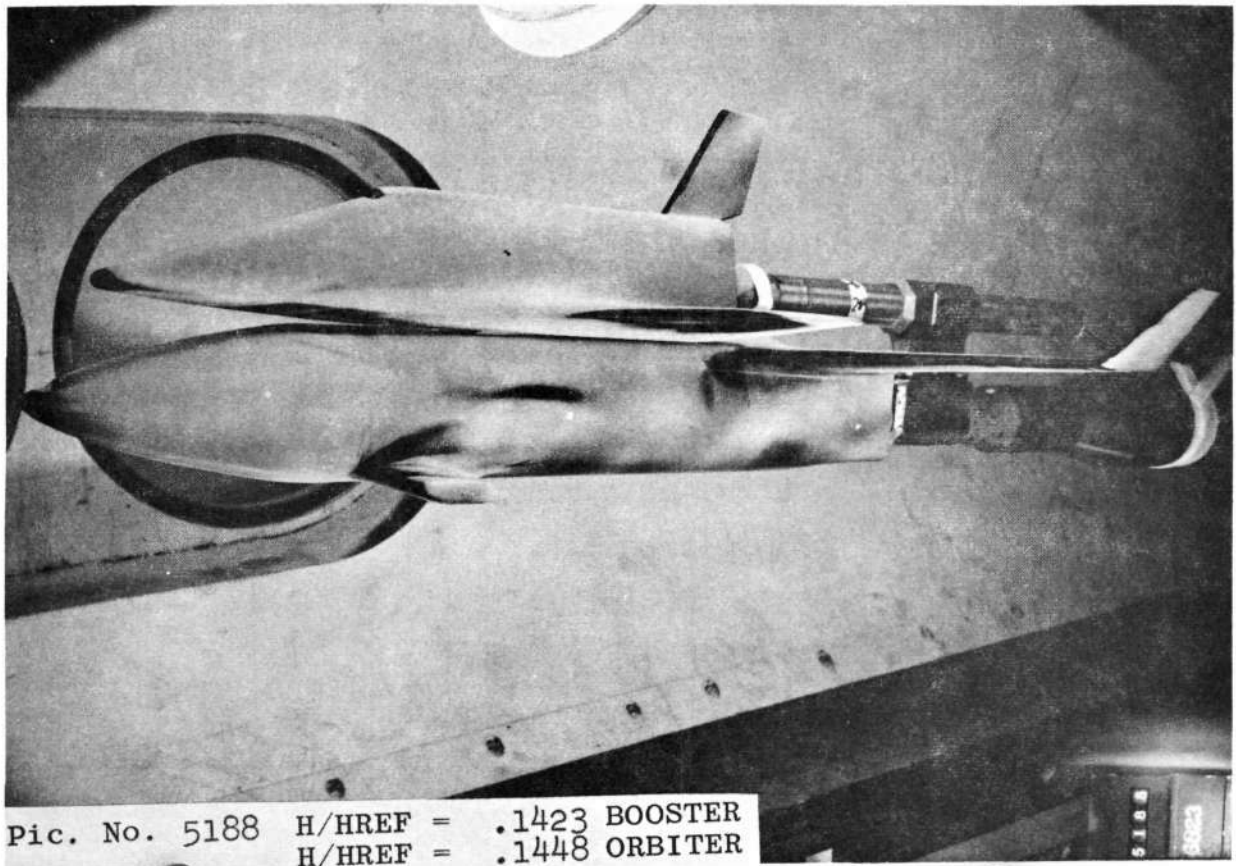
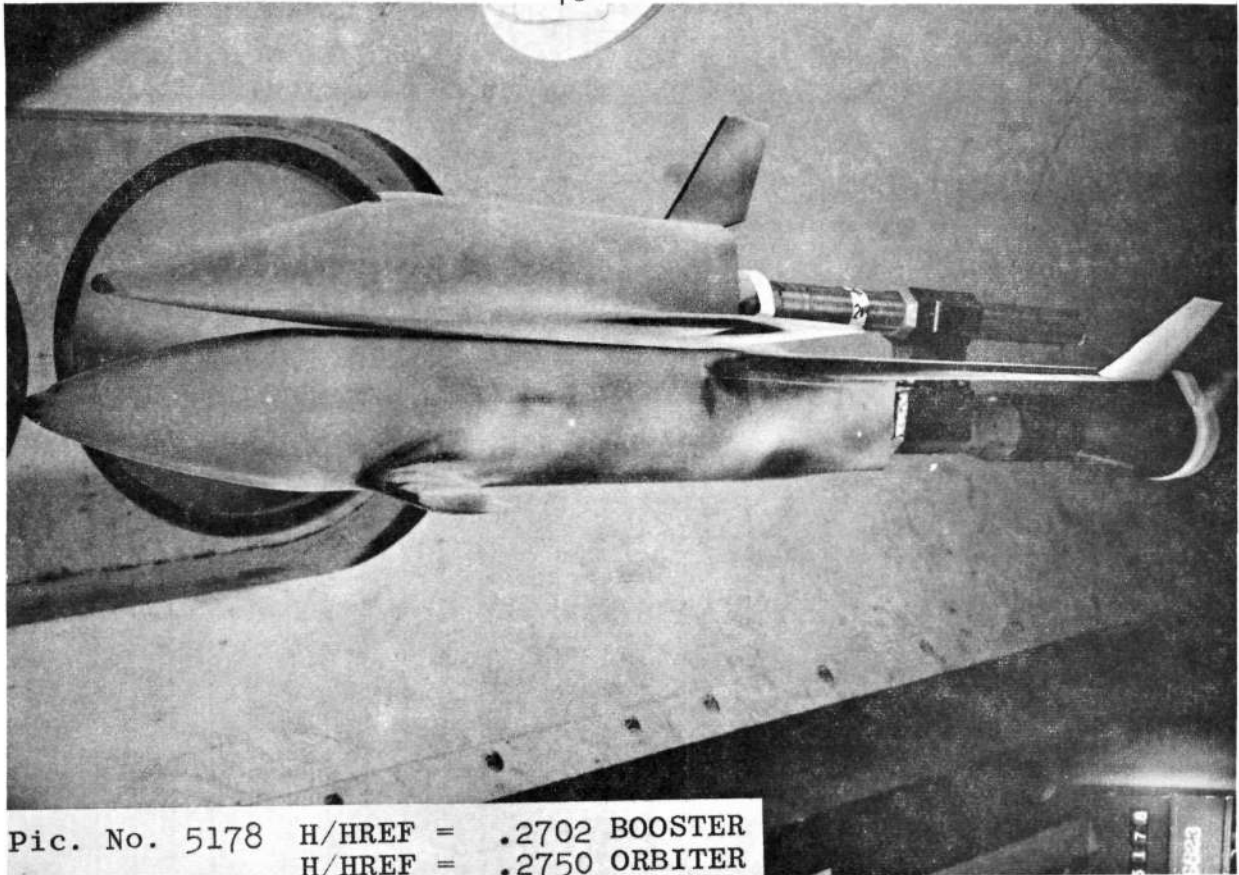
Pic. No. 5366 H/HREF = .0560 BOOSTER
H/HREF = .0571 ORBITER

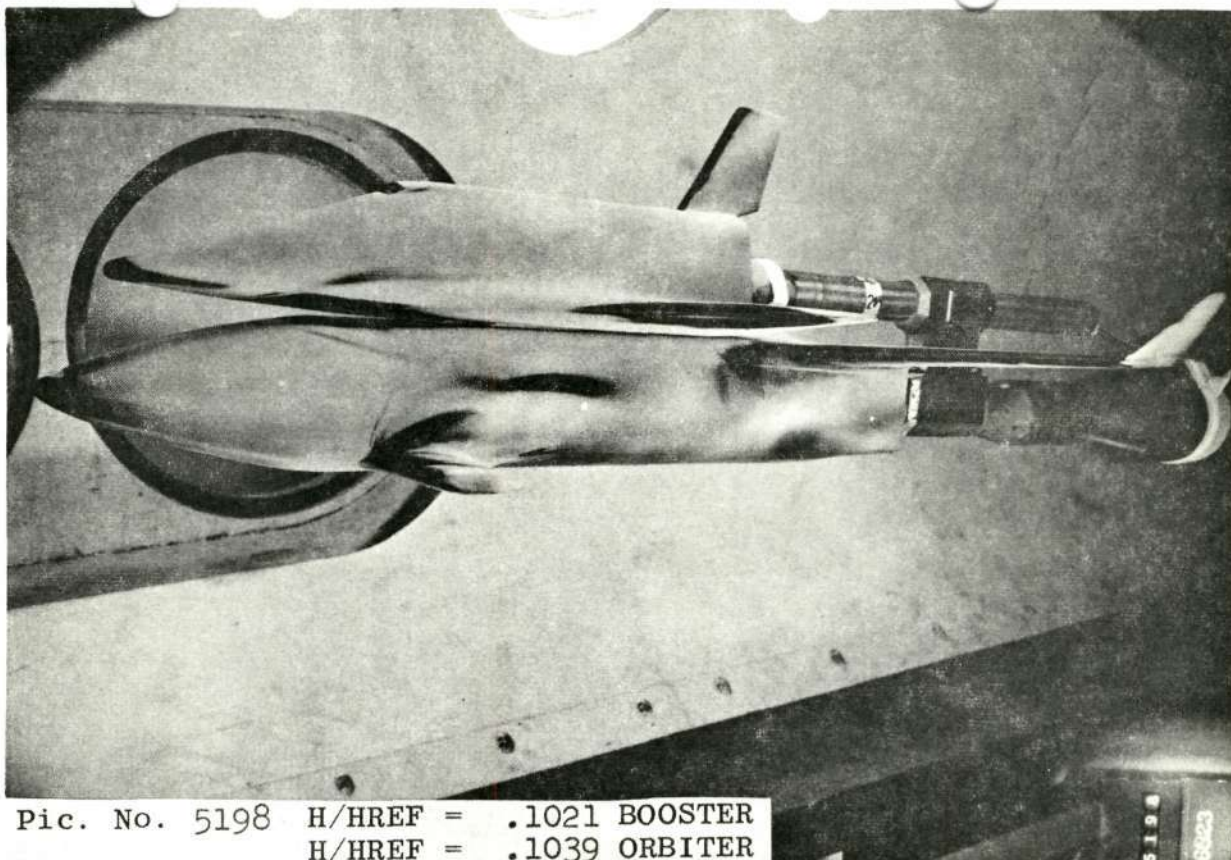
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AFDCIARO-INC.) ARNOLD AFS, TENNESSEE
VON KARMAN GAS DYNAMICS FACILITY
50 INCH HYPERSONIC TUNNEL B
VT1162

GROUP	CONFID	MODEL	MACH NO	PO PSIA	TO DEG R	ALPHA-RODEL	ALPHA-SECTOR	ALPHA-PREBEND	ROLL-MODEL	VAN
204	1221	W0AC-8.0VC	8.00	549.4	1326	5.02	5.02			
1-1NF P-1NF Q-1NF V-1NF RHO-1NF MU-1NF REFT WREF STRIF										
(DEG R) (PSIA) (PSIA) (FT/SEC) (SLUGS/FT) (LB-SEC/FT) (FT-1) (IN-0.01FT) (IN-0.01FT)										
90.1	.056	2.521	3443	4.912E-05	7.138E-08	2.44E-06	4.989E-02	3.287E-42		
CAVEA PAINT TEMP (DEG F) INITIAL TEMP (DEG F) SQUARE ROOT (RHOXCR)										
TEMP (T) 250										
STRE (US) 500										
SIC (LS) 500										
AVERAGE T _W = 87 (R)										
AVERAGE T _W = 84 (O)										
--000(SQUARE ROOT DEL TIME) * 0.11										

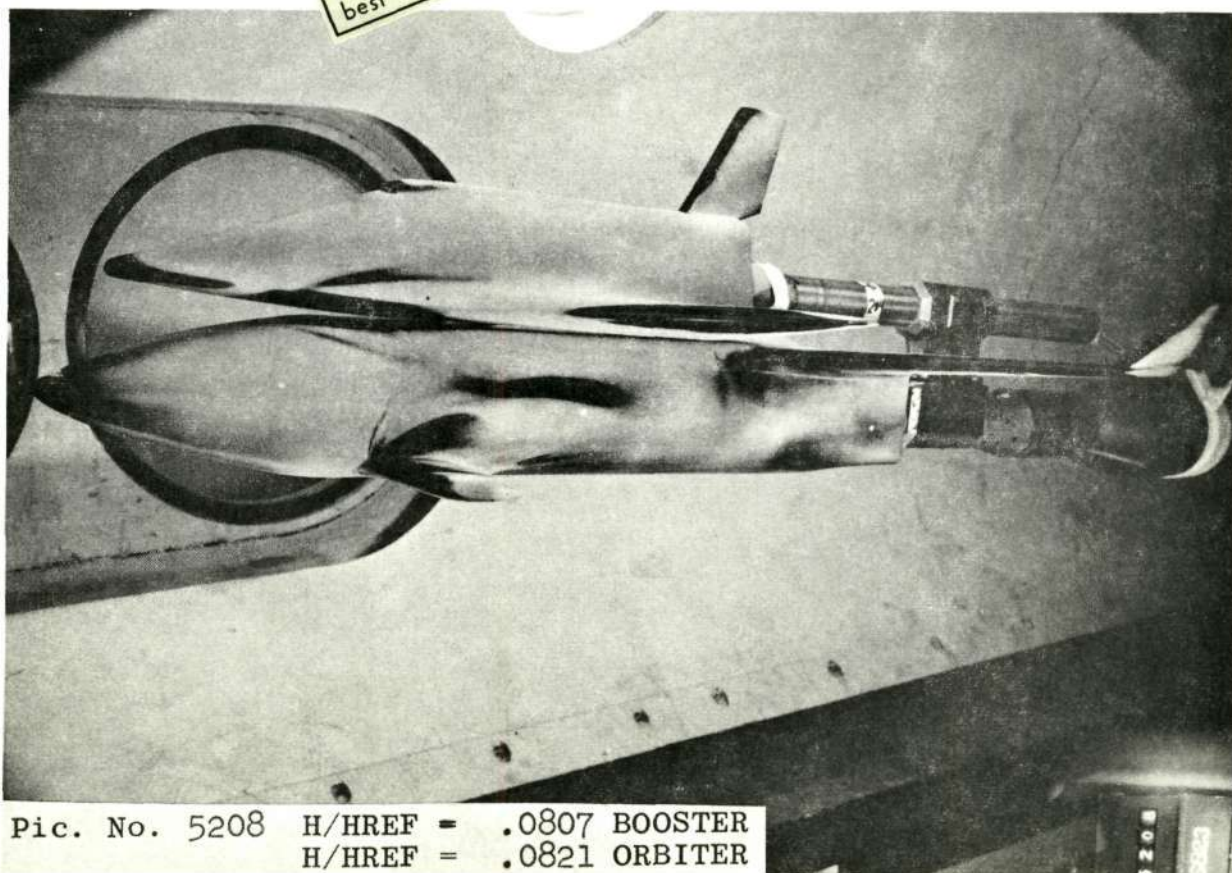
PIC NC	TIME DELTIME	M(TO)	M(TO)/MREF	M(.9TO)	M(.9TO)/MREF	M(.85TO)	M(.85TO)/MREF	SI(TO)	MODEL	TEMP F
US 517E (500)	3.65	2.50	0.571E-02	1.0651	7.795E-02	1.5635	1.049E-01	2.1023	3.375E-02	90 84 86 82
US 517E (250)	3.65	2.50	0.173E-02	.2702	1.698E-02	.3490	1.952E-02	.3913	0.644E-03	90 84 86 82
US 517E (500)	3.65	2.50	0.519E-02	1.0393	7.745E-02	1.5525	1.002E-01	2.0848	3.353E-02	90 84 86 82
US 517E (250)	3.65	2.50	0.137E-02	.2750	1.728E-02	.3463	1.964E-02	.3901	9.000E-03	90 84 86 82
US 518E (500)	8.70	7.63	0.274E-02	.5502	4.103E-02	.8226	5.531E-02	1.1048	1.777E-02	93 84 103 82
US 518E (250)	8.70	7.63	0.710E-03	.1473	0.939E-03	.1742	1.028E-02	.2040	4.657E-03	93 84 103 82
US 518E (500)	8.70	7.63	0.273E-02	.5466	4.071E-02	.8176	5.406E-02	1.0907	1.765E-02	93 84 103 82
US 518E (250)	8.70	7.63	0.722E-03	.1448	0.904E-03	.1823	1.065E-02	.2096	4.739E-03	93 84 103 82
US 519E (500)	13.80	12.73	0.197E-02	.3947	2.944E-02	.5962	3.961E-02	.7941	1.275E-02	102 85 125 82
US 519E (250)	13.80	12.73	0.54E-03	.1021	4.414E-03	.1266	7.372E-03	.1470	3.541E-03	102 85 125 82
US 519E (500)	13.80	12.73	0.196E-02	.3922	2.923E-02	.5864	3.936E-02	.7900	1.266E-02	102 85 125 82
US 519E (250)	13.80	12.73	0.519E-03	.1019	6.523E-03	.1368	7.530E-03	.1544	3.400E-03	102 85 125 82
US 520E (500)	18.90	17.83	0.146E-02	.3121	2.332E-02	.4667	3.132E-02	.6279	1.008E-02	110 86 145 83
US 520E (250)	18.90	17.83	0.463E-03	.0807	5.071E-03	.1017	5.829E-03	.1149	2.642E-03	110 86 145 83
US 520E (500)	18.90	17.83	0.145E-02	.3101	2.313E-02	.4637	3.122E-02	.6279	1.002E-02	110 86 145 83
US 520E (250)	18.90	17.83	0.410E-03	.0821	5.159E-03	.1034	5.930E-03	.1199	2.609E-03	110 86 145 83





Pic. No. 5198 H/HREF = .1021 BOOSTER
H/HREF = .1039 ORBITER

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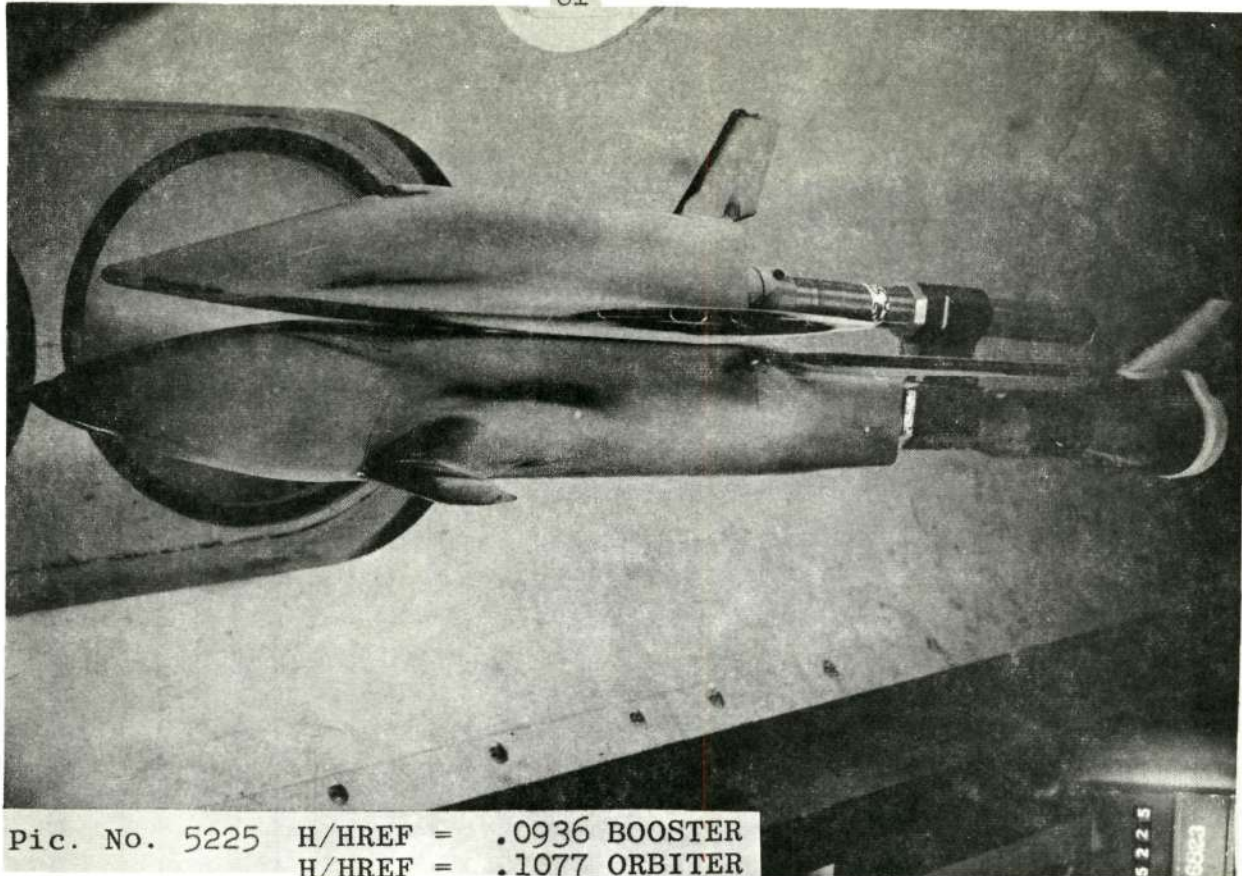
Pic. No. 5208 H/HREF = .0807 BOOSTER
H/HREF = .0821 ORBITER

6/ 3/71

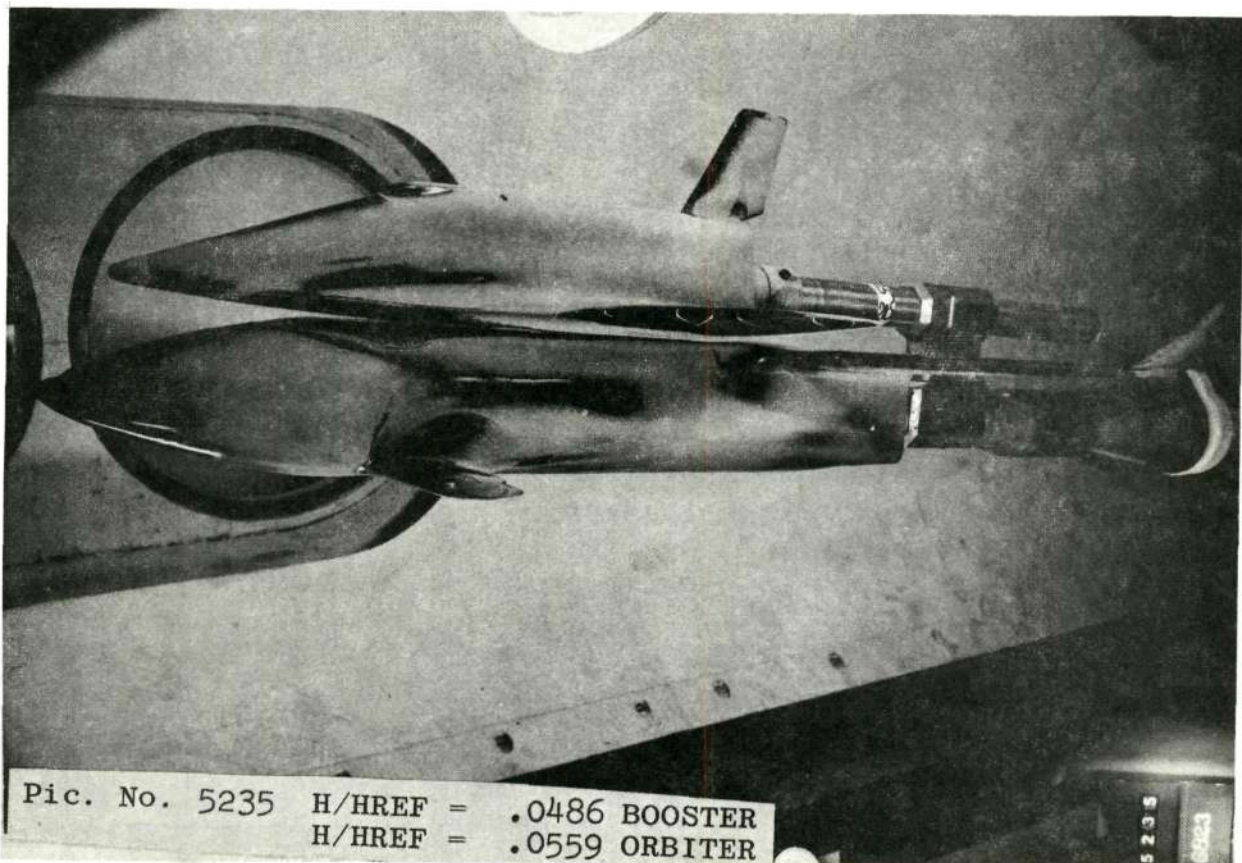
AFDC(ARO-INC.) ARMOLO AFS, TENNESSEE
VON KARMAN GAS DYNAMICS FACILITY
50 INCH HYPERSONIC TUNNEL B
V71162

GROUP CONFIG MODEL MACH NO PO PSIA TO DEG R ALPHA-MODEL ALPHA-SECTOR ALPHA-REFBEND ROLL-MODEL YAW
205 1222 PDAC-8-0-MO 8.00 553.2 1320 5.06 5.06 0 0
T-1AF P-1AF 0-1AF V-1AF RHO-1AF MU-1AF RE/FT HREF STREF
(DEG R) (PSIA) (FT/SEC) (SLUGS/FT³) (LB-SEC/FT²) (FT-1) (LB-OIL/FT) (LB-OIL/FT)
95.7 .057 2.538 3974 4.968E-05 7.703E-08 2.47E 06 5.002E-02 3.267E-02
CAMERA PAINT TEMP (DEG F) INITIAL TEMP (DEG F) SQUARE ROOT (INCH/CT) STREF
TEMP (F) 15.0
SLOC(US) 156
SLOC(LS) 156
AVERAGE TW = 98 (F)
AVERAGE TW = 78 (C)
-0.008(SQUARE ROOT DEL TIME) * 0.11

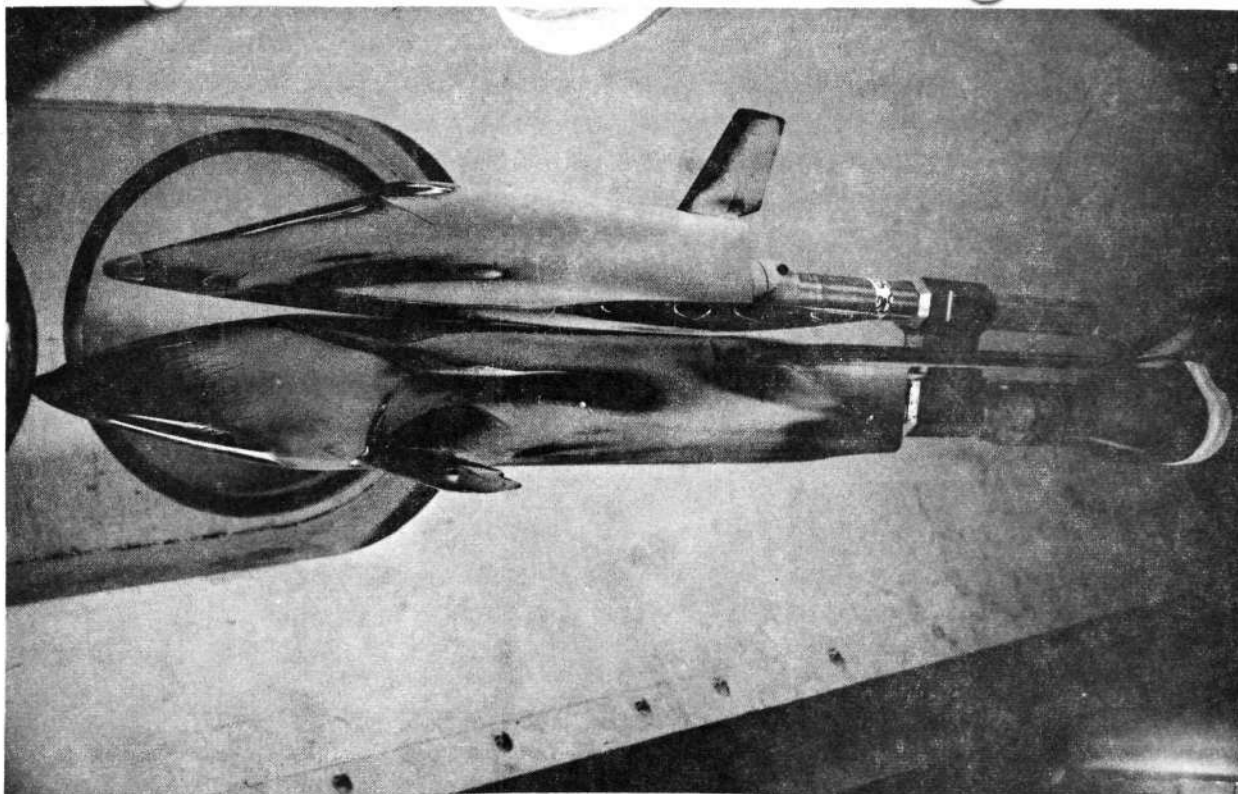
PIC NC	TIME	DELTIME	M(TO)	M(TO)/REF	M(.910)	M(.910)/REF	M(.8510)	M(.8510)/REF	ST(10)	MODEL	TEMP	F
US 5225 (150)	3.55	2.51	0	5.30E-03	.1077	6.587E-03	.1137	7.413E-03	.1482	3.521E-03	91	84
US 5225 (150)	3.55	2.51	0	4.49E-03	.0936	5.726E-03	.1145	6.450E-03	.1290	3.062E-03	91	84
US 5225 (150)	3.55	2.51	0	4.49E-03	.0936	5.726E-03	.1145	6.450E-03	.1290	3.062E-03	91	84
US 5225 (150)	3.55	2.51	0	5.30E-03	.1077	6.587E-03	.1137	7.413E-03	.1482	3.521E-03	91	84
US 5225 (150)	8.65	7.61	0	2.79E-03	.0559	3.419E-03	.0683	3.847E-03	.0749	1.628E-03	95	85
US 5225 (150)	8.65	7.61	0	2.43E-03	.0486	2.972E-03	.0594	3.347E-03	.0649	1.589E-03	95	85
US 5225 (150)	8.65	7.61	0	2.43E-03	.0486	2.972E-03	.0594	3.347E-03	.0649	1.589E-03	95	85
US 5225 (150)	8.65	7.61	0	2.79E-03	.0559	3.419E-03	.0683	3.847E-03	.0749	1.628E-03	95	85
US 5225 (150)	13.75	12.71	0	2.60E-03	.0401	2.451E-03	.0490	2.750E-03	.0551	1.310E-03	101	86
US 5225 (150)	13.75	12.71	0	1.74E-03	.0348	2.131E-03	.0426	2.400E-03	.0440	1.139E-03	101	86
US 5225 (150)	13.75	12.71	0	2.00E-03	.0401	2.451E-03	.0490	2.750E-03	.0551	1.310E-03	101	86
US 5225 (150)	13.75	12.71	0	1.74E-03	.0348	2.131E-03	.0426	2.400E-03	.0440	1.139E-03	101	86
US 5225 (150)	18.85	17.81	0	1.58E-03	.0317	1.938E-03	.0387	2.180E-03	.0436	1.036E-03	110	87
US 5225 (150)	18.85	17.81	0	1.38E-03	.0275	1.684E-03	.0337	1.977E-03	.0379	9.004E-04	110	87
US 5225 (150)	18.85	17.81	0	1.38E-03	.0275	1.684E-03	.0337	1.977E-03	.0379	9.004E-04	110	87
US 5225 (150)	18.85	17.81	0	1.58E-03	.0317	1.938E-03	.0387	2.180E-03	.0436	1.036E-03	110	87



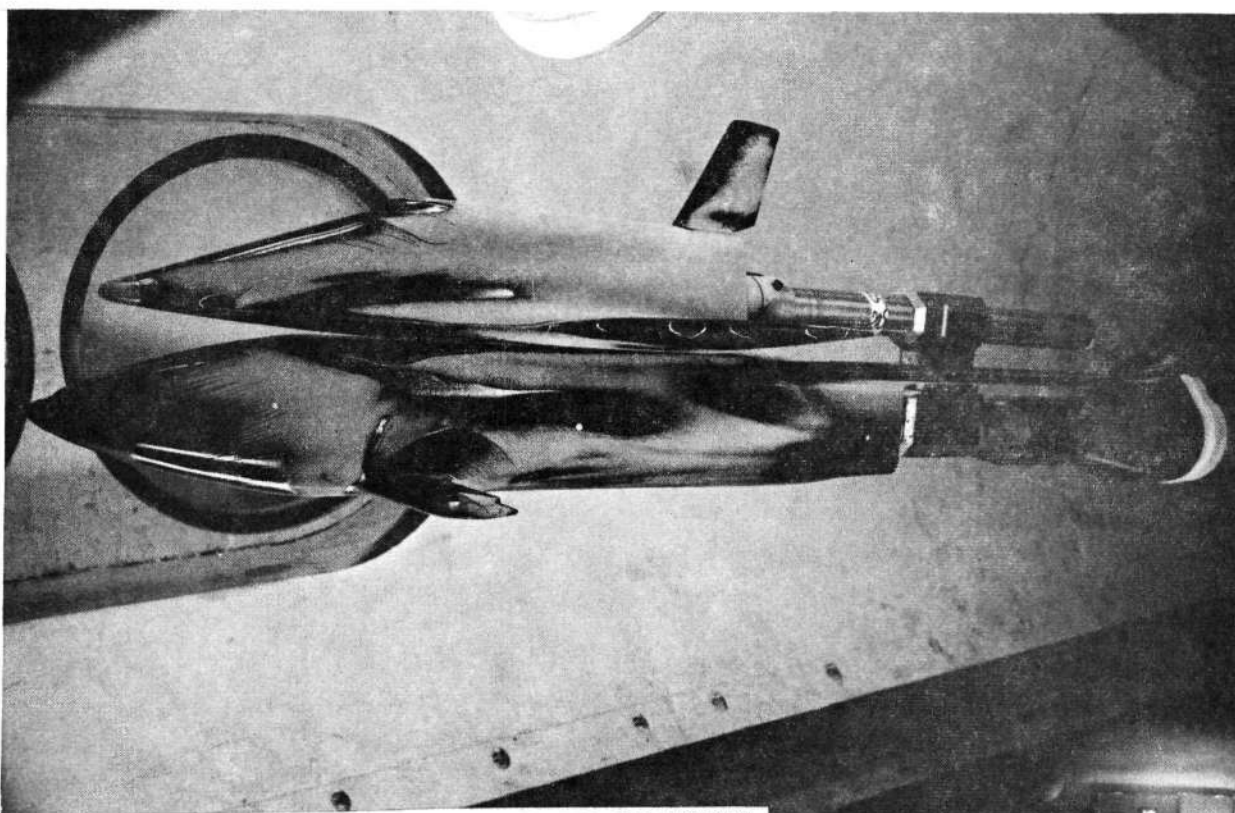
Pic. No. 5225 H/HREF = .0936 BOOSTER
H/HREF = .1077 ORBITER



Pic. No. 5235 H/HREF = .0486 BOOSTER
H/HREF = .0559 ORBITER



Pic. No. 5245 H/HREF = .0348 BOOSTER
H/HREF = .0401 ORBITER



Pic. No. 5255 H/HREF = .0275 BOOSTER
H/HREF = .0317 ORBITER

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AFDC/ARNO, INC.) ARNOLD AFS, TENNESSEE
 VON KARMAN GAS DYNAMICS FACILITY
 50 INCH HYPERSONIC TUNNEL B
 V11162

GROUP	CONFID	MODEL	MACH NO	PO PSIA	TO DEG R	ALPHA-MODEL	ALPHA-SECTION	ALPHA-PREBEND	ROLL-MODEL	YAW
206	3221	MOAC-B-DWQ	8.00	548.9	1326	-4.08	-4.98			

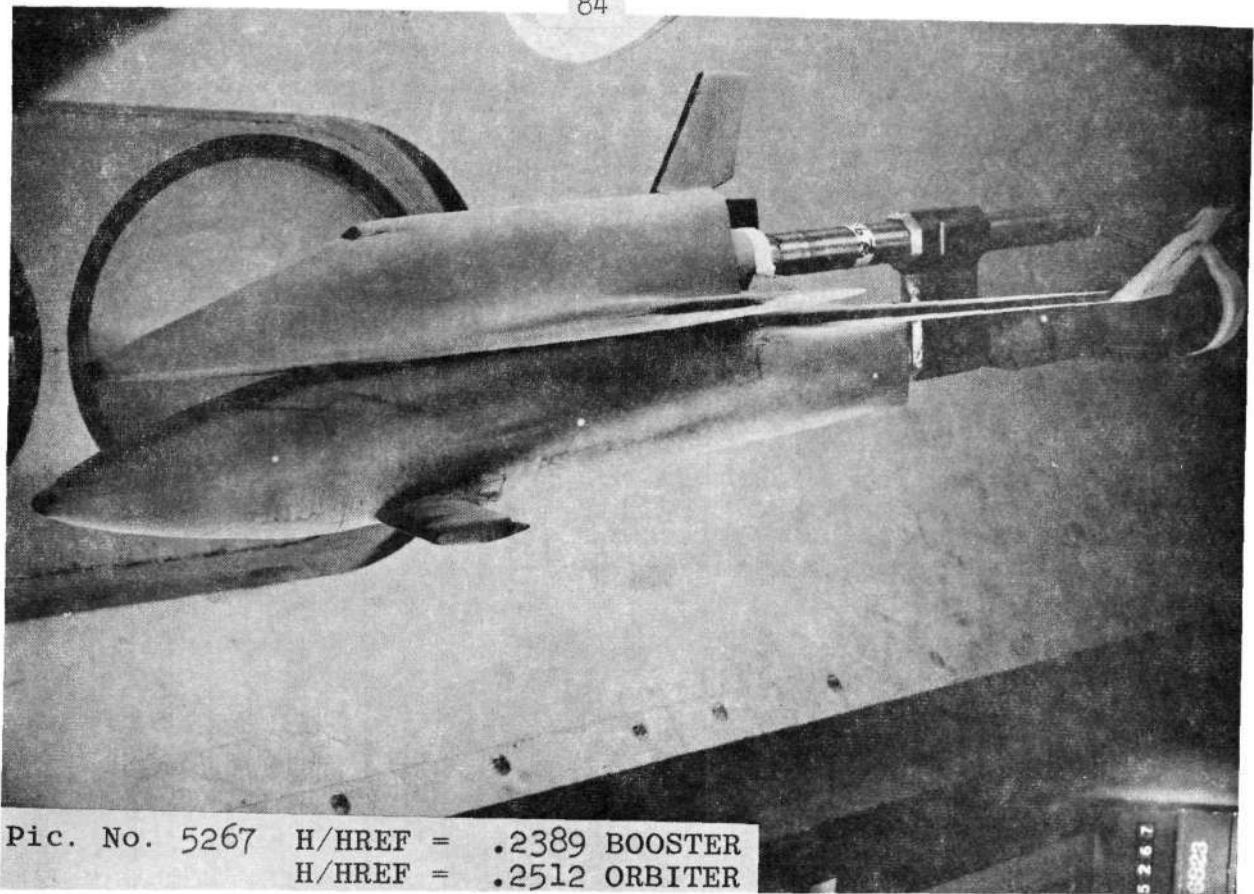
T-1NF	P-1NF	Q-1NF	V-1NF	RHO-1NF	MU-1NF	RE/FT	WREF	STREF
(OEG R) (PSIA)	(PSIA)	(FT/SEC)	(SLUGS/FT ³)	(LB-SEC/FT ²)	(FT-1)	(R-0.01FT)	(R-0.01FT)	(R-0.01FT)
96.1	.056	2.519	3042	4.911E-05	7.734E-08	2.44E 06	4.987E-02	3.207E-02

CAMERA	PAINT TEMP (OEG F)	INITIAL TEMP (OEG F)	SQUARE ROOT (RMDACX)
TOP(T1)	250		
SICE(U5)	500		
SIDE(L5)	500		

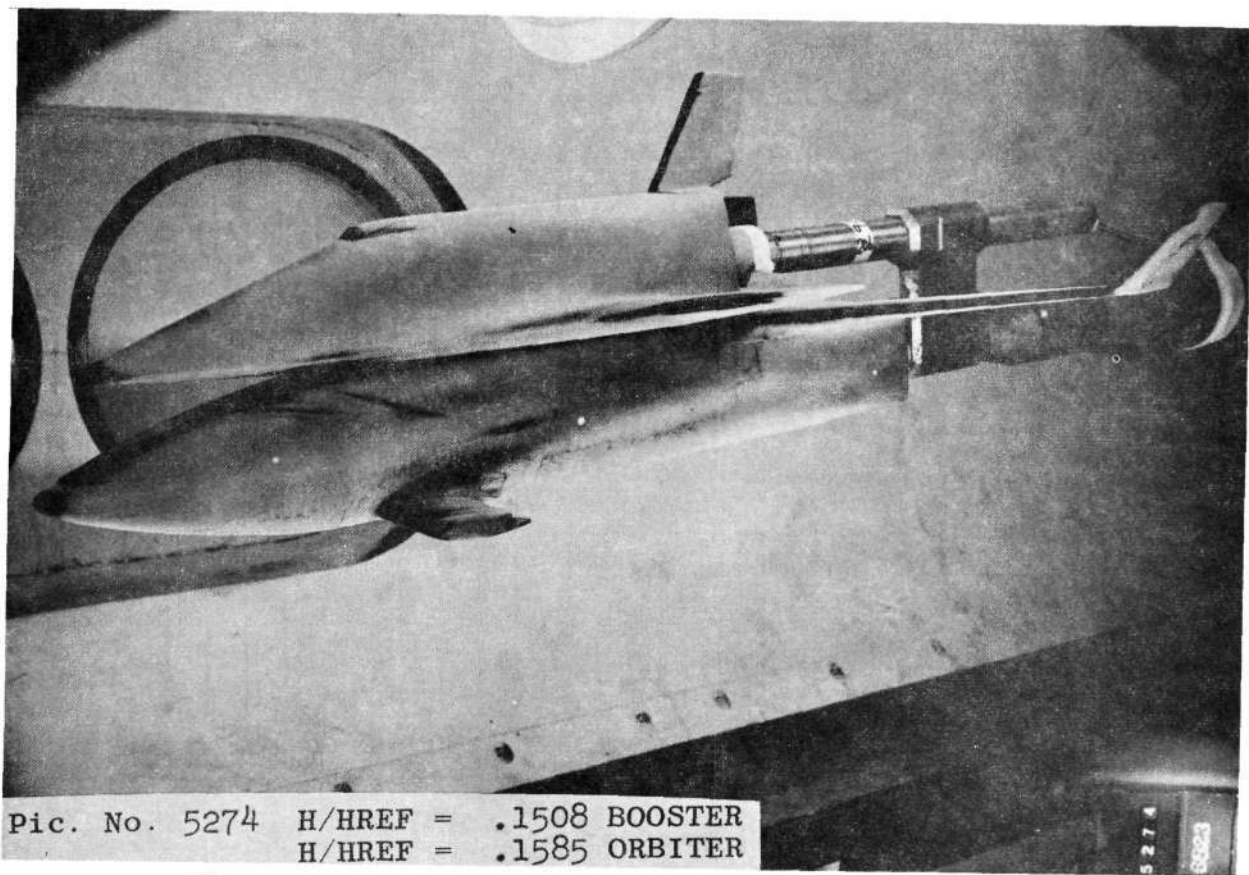
AVERAGE TM = 89 (8)
 AVERAGE TW = 88 (0)

-.008(SQUARE ROOT DEL TIME) * 0.11

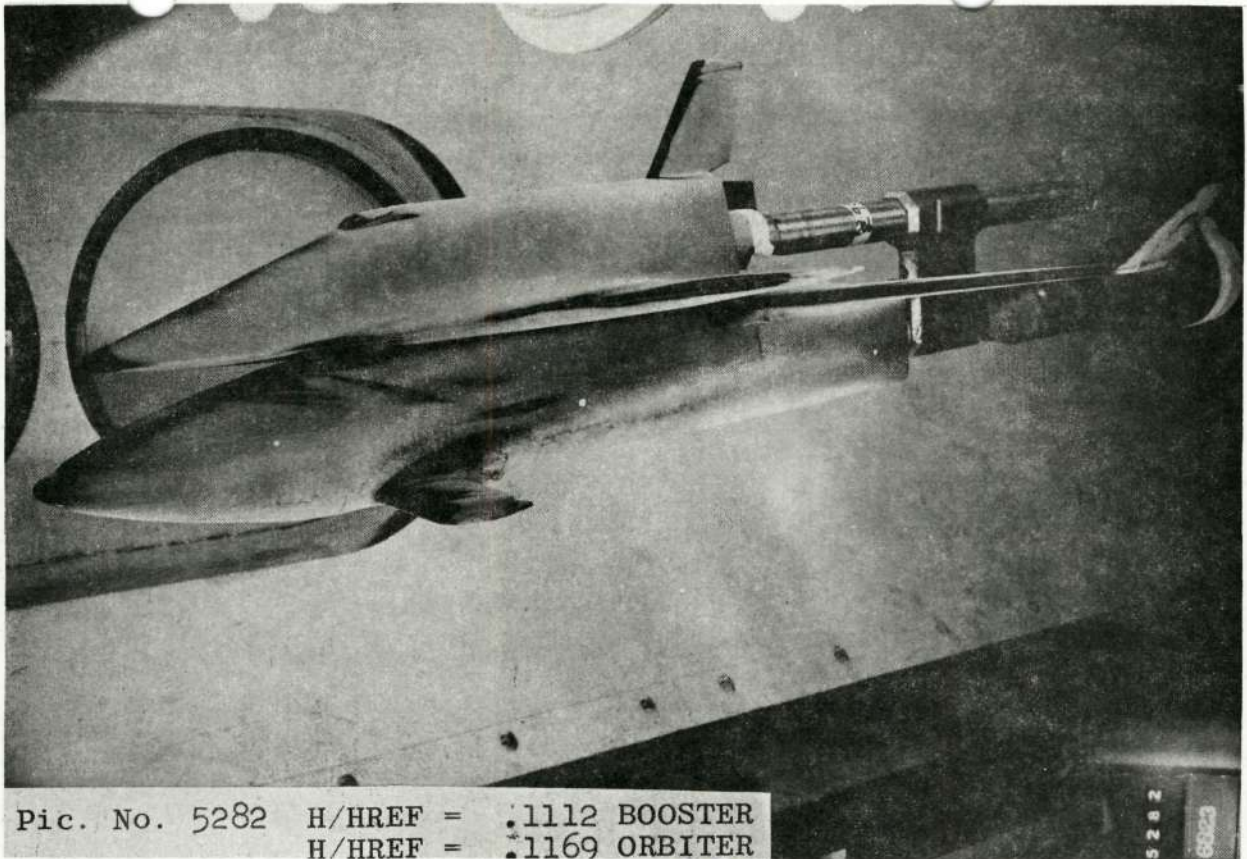
PIC NO	TIME DELTIVE	M(TO)	M(TO)/MREF	M(-9TO)	M(-9TO)/MREF	M(.85TO)	M(.85TO)/MREF	ST(10)	MODEL TEMP F
US 5267 (500)	4.20	3.14	0.470E-02	.9618	7.020E-02	1.4089	9.462E-02	1.8972	3.041E-02
US 5267 (250)	4.20	3.14	0.119E-02	.2309	1.501E-02	.3009	1.726E-02	1.8972	7.010E-02
US 5267 (500)	4.20	3.16	8.441E-02	.9241	6.800E-02	1.3628	9.207E-02	1.8621	2.984E-02
US 5267 (250)	4.20	3.16	0.175E-02	.2512	1.578E-02	.3163	1.813E-02	1.8621	8.220E-02
US 5274 (500)	7.90	6.86	0.206E-02	.5944	4.434E-02	.8892	5.971E-02	1.1974	1.920E-02
US 5274 (250)	7.90	6.86	0.742E-03	.1508	9.412E-03	.1899	1.089E-02	.2194	4.910E-02
US 5274 (500)	7.90	6.86	8.291E-02	.5833	4.352E-02	.8728	5.061E-02	1.1743	1.084E-02
US 5274 (250)	7.90	6.86	0.791E-03	.1508	9.412E-03	.1899	1.089E-02	.2194	4.910E-02
US 5282 (500)	12.10	11.04	0.219E-02	.4384	3.271E-02	.6558	4.404E-02	.8031	3.640E-02
US 5282 (250)	12.10	11.04	8.535E-03	.1112	6.987E-03	.1401	8.322E-03	.1611	3.640E-03
US 5292 (500)	12.10	11.04	0.215E-02	.4302	3.210E-02	.6437	4.323E-02	.8446	1.389E-02
US 5292 (250)	12.10	11.04	0.549E-03	.1169	7.394E-03	.1473	8.441E-03	.1693	3.028E-02
US 5292 (500)	16.30	15.24	0.174E-02	.3525	2.629E-02	.5273	3.541E-02	.7161	1.139E-02
US 5292 (250)	16.30	15.24	8.446E-03	.0894	5.617E-03	.1126	6.457E-03	.1295	2.920E-02
US 5290 (500)	16.30	15.24	8.172E-02	.3459	2.501E-02	.5176	3.475E-02	.6949	1.110E-02
US 5290 (250)	16.30	15.24	0.446E-03	.0940	5.904E-03	.1164	6.786E-03	.1361	3.079E-03



Pic. No. 5267 H/HREF = .2389 BOOSTER
H/HREF = .2512 ORBITER

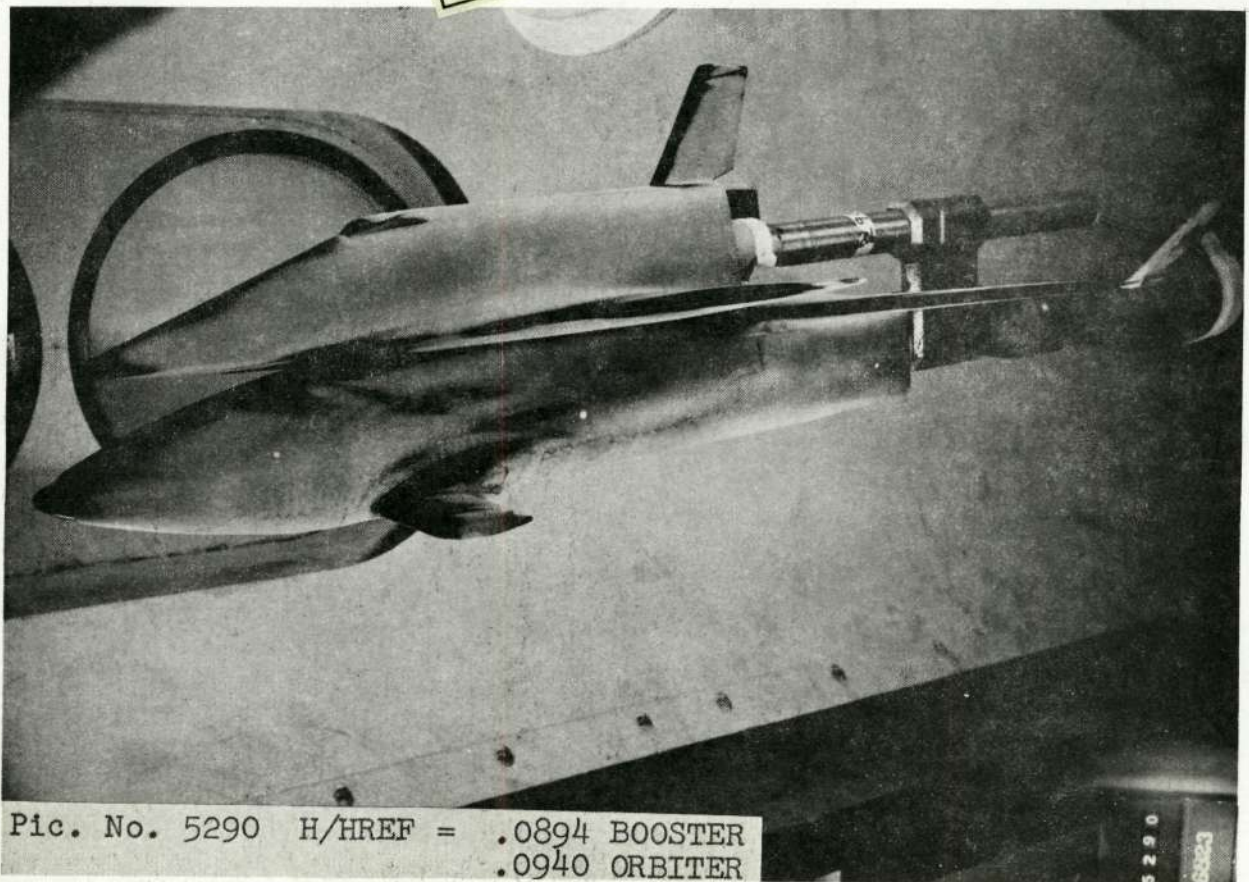


Pic. No. 5274 H/HREF = .1508 BOOSTER
H/HREF = .1585 ORBITER

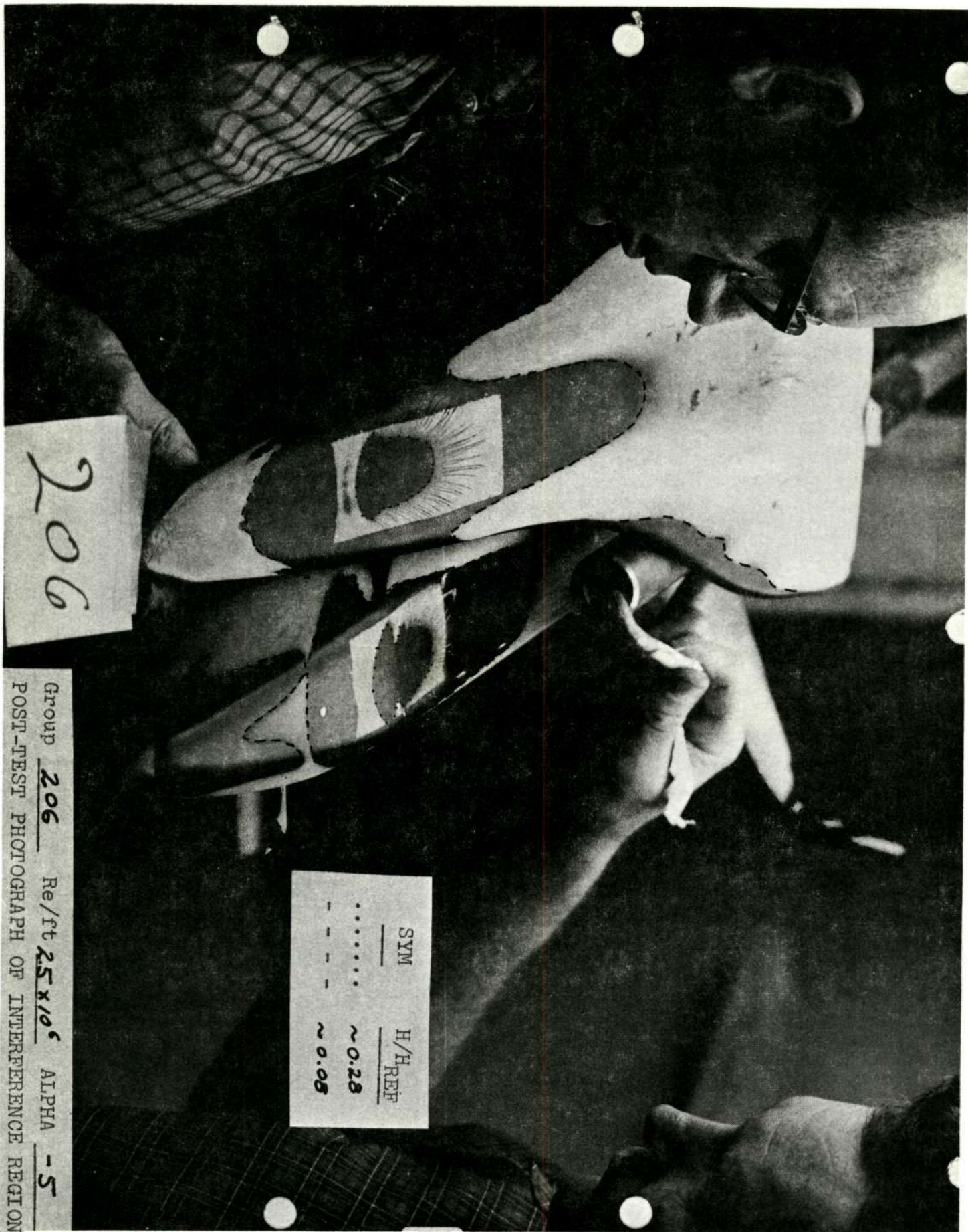


Pic. No. 5282 H/HREF = .1112 BOOSTER
H/HREF = .1169 ORBITER

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Pic. No. 5290 H/HREF = .0894 BOOSTER
.0940 ORBITER



SYM	H/H _{REF}
.....	~0.28
- - - -	~0.08

Group 206 Re/ft 2.5 x 10⁶ ALPHA -5
 POST-TEST PHOTOGRAPH OF INTERFERENCE REGION

AEDC (ARO, INC.) ARNOLD AFS, TENNESSEE
VON KARMAN AIR ACQUISITION OFFICE

50 INCH HYPERSONIC TUNNEL 8
W11162

2911A

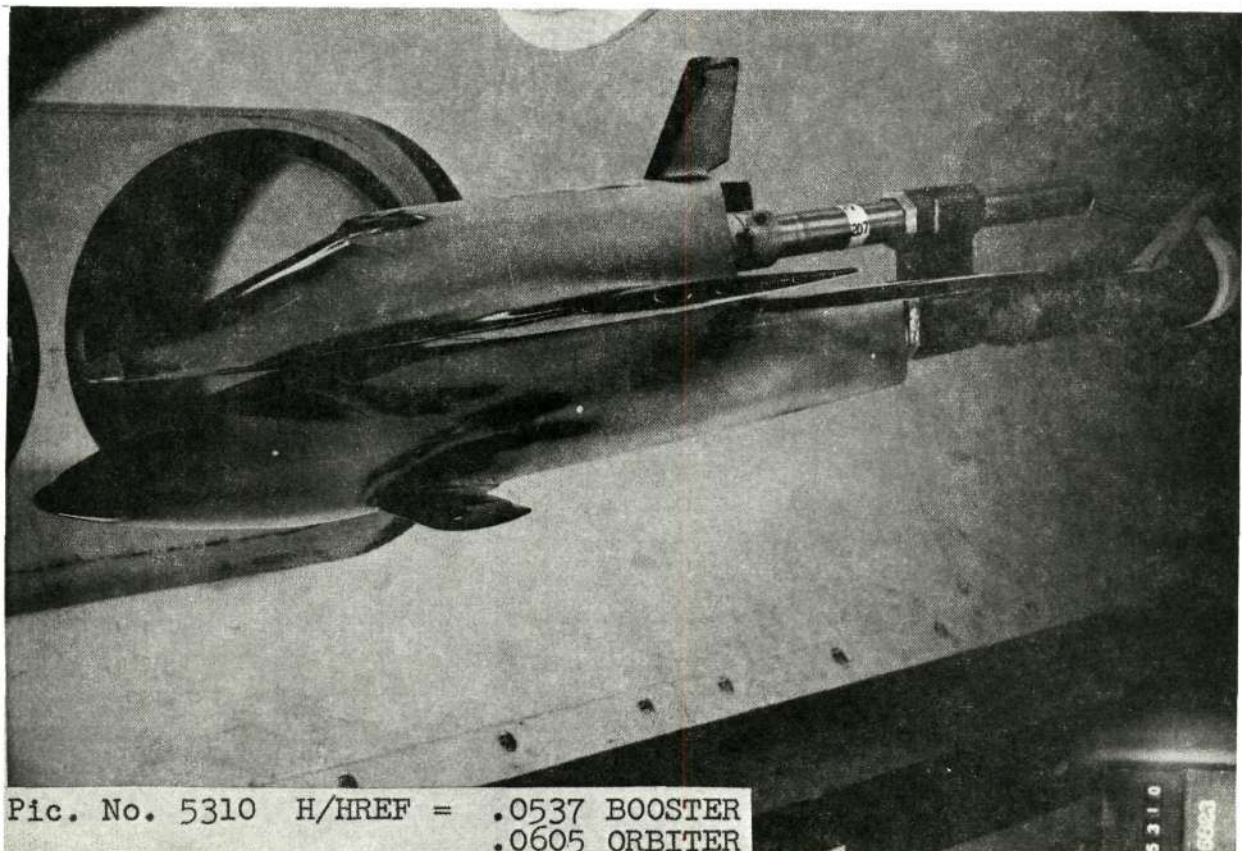
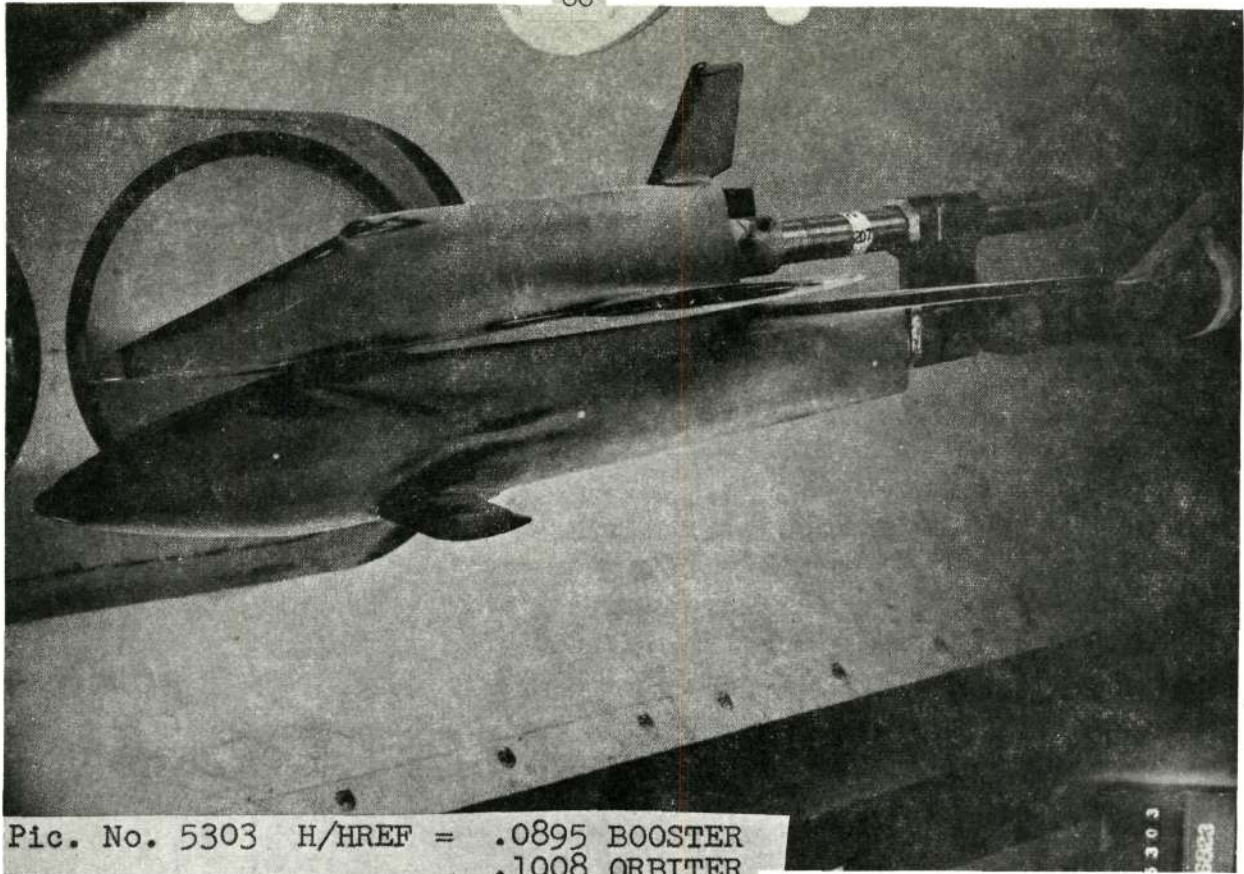
GROUP	MODEL	MACM NO	PO PSIA	TO DEG R	ALPHA-PROEL	ALPHA-SECTION	ALPHA-PREEND	ROLL-MODEL	YAW
207	1222	PDAC-8-DWC	8.00	551.1	1328	-4.99	-4.99	0	0

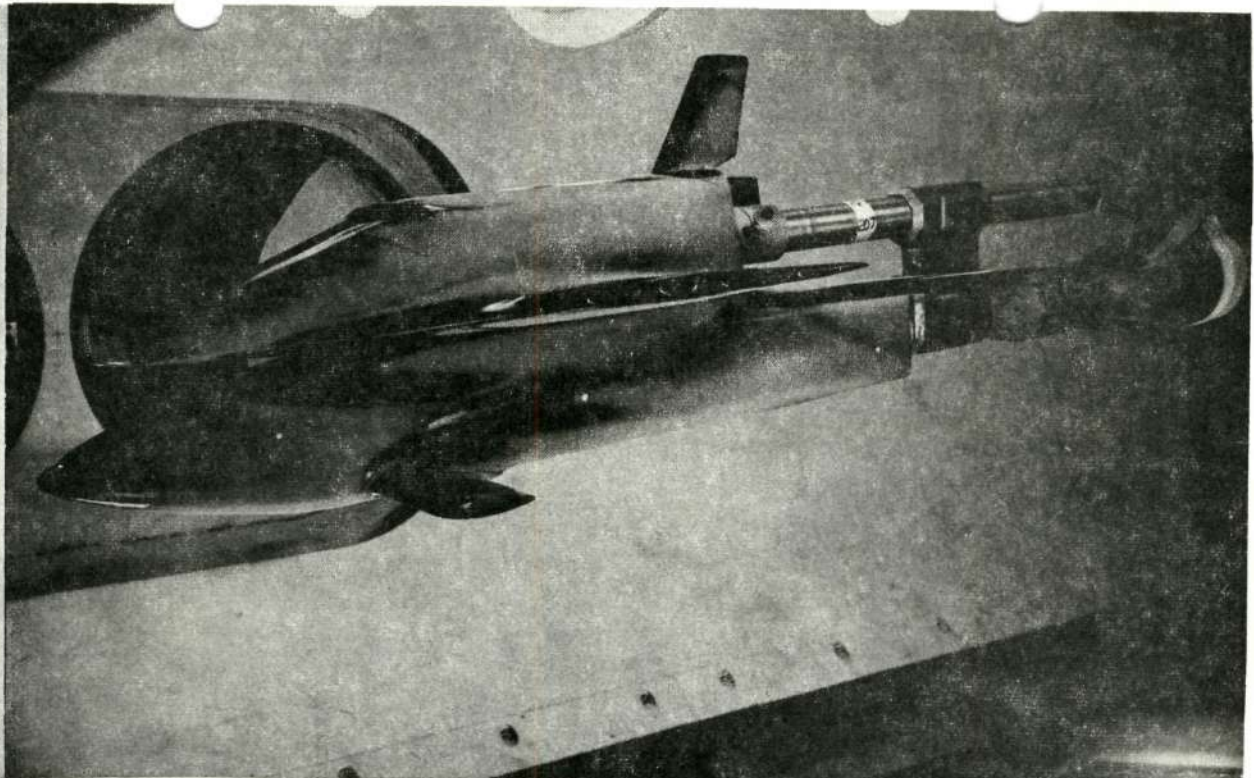
Year	1981	1982	1983	1984	1985	1986	1987	1988	1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014	2015	2016	2017	2018	2019	2020	2021	2022	2023	2024	2025	2026	2027	2028	2029	2030	2031	2032	2033	2034	2035	2036	2037	2038	2039	2040	2041	2042	2043	2044	2045	2046	2047	2048	2049	2050	2051	2052	2053	2054	2055	2056	2057	2058	2059	2060	2061	2062	2063	2064	2065	2066	2067	2068	2069	2070	2071	2072	2073	2074	2075	2076	2077	2078	2079	2080	2081	2082	2083	2084	2085	2086	2087	2088	2089	2090	2091	2092	2093	2094	2095	2096	2097	2098	2099	2100
1981	1982	1983	1984	1985	1986	1987	1988	1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014	2015	2016	2017	2018	2019	2020	2021	2022	2023	2024	2025	2026	2027	2028	2029	2030	2031	2032	2033	2034	2035	2036	2037	2038	2039	2040	2041	2042	2043	2044	2045	2046	2047	2048	2049	2050	2051	2052	2053	2054	2055	2056	2057	2058	2059	2060	2061	2062	2063	2064	2065	2066	2067	2068	2069	2070	2071	2072	2073	2074	2075	2076	2077	2078	2079	2080	2081	2082	2083	2084	2085	2086	2087	2088	2089	2090	2091	2092	2093	2094	2095	2096	2097	2098	2099	2100	

CAVEIRA	PAINT TEMP (DEG F)	INITIAL TEMP (DEG F)	SQUARE ROOT (PHOXCKXK)
70871	11		

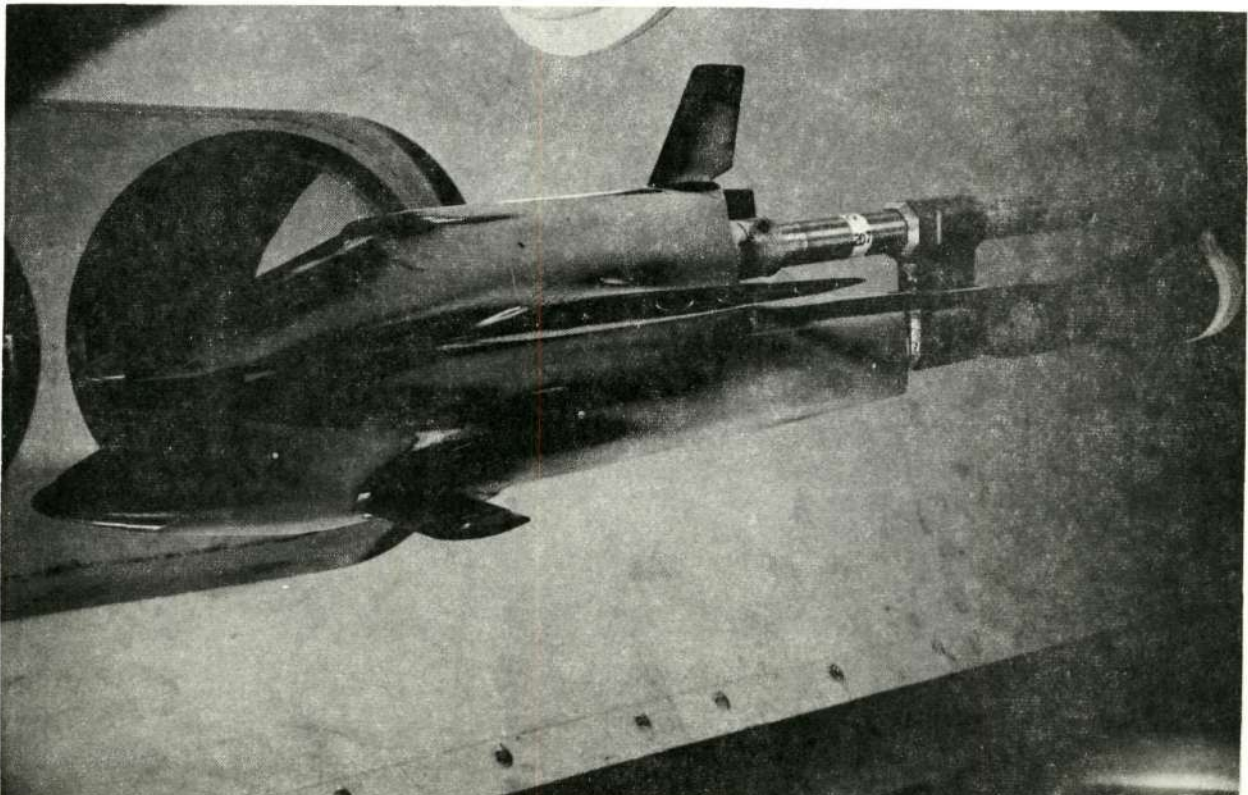
SIZE (US)	15A	AVERAGE TW =	66 (2)	-0.06(SQUARE ROOT OFL TIME) + 0.11
SIZE (LS)	15A	AVERAGE TW =	66 (2)	

PC MC	TIME	ELAPSE	MITO	MITO/REF	M1.(T0)	M1.(T1)/REF	M1.(S0)	M1.(S1)/REF	MITO	MODEL	TEMP	F
US 5303	(150)	3.70	2.63	0	5.06E-03	.1008	6.153E-03	.1232	6.922E-03	5.310E-03	91	86
US 5302	(150)	3.70	2.63	0	4.47E-03	.0895	5.465E-03	.1094	6.149E-03	2.943E-03	91	86
US 5301	(150)	3.70	2.63	0	4.47E-03	.0895	5.465E-03	.1094	6.149E-03	2.943E-03	91	86
US 5300	(150)	3.70	2.63	0	5.06E-03	.1008	6.153E-03	.1232	6.922E-03	5.310E-03	91	86
US 5299	(150)	3.70	2.63	0	5.06E-03	.1008	6.153E-03	.1232	6.922E-03	5.310E-03	91	86
US 5298	(150)	3.70	2.63	0	5.06E-03	.1008	6.153E-03	.1232	6.922E-03	5.310E-03	91	86
US 5297	(150)	3.70	2.63	0	5.06E-03	.1008	6.153E-03	.1232	6.922E-03	5.310E-03	91	86
US 5296	(150)	3.70	2.63	0	5.06E-03	.1008	6.153E-03	.1232	6.922E-03	5.310E-03	91	86
US 5295	(150)	3.70	2.63	0	5.06E-03	.1008	6.153E-03	.1232	6.922E-03	5.310E-03	91	86
US 5294	(150)	3.70	2.63	0	5.06E-03	.1008	6.153E-03	.1232	6.922E-03	5.310E-03	91	86
US 5293	(150)	3.70	2.63	0	5.06E-03	.1008	6.153E-03	.1232	6.922E-03	5.310E-03	91	86
US 5292	(150)	3.70	2.63	0	5.06E-03	.1008	6.153E-03	.1232	6.922E-03	5.310E-03	91	86
US 5291	(150)	3.70	2.63	0	5.06E-03	.1008	6.153E-03	.1232	6.922E-03	5.310E-03	91	86
US 5290	(150)	3.70	2.63	0	5.06E-03	.1008	6.153E-03	.1232	6.922E-03	5.310E-03	91	86
US 5289	(150)	3.70	2.63	0	5.06E-03	.1008	6.153E-03	.1232	6.922E-03	5.310E-03	91	86
US 5288	(150)	3.70	2.63	0	5.06E-03	.1008	6.153E-03	.1232	6.922E-03	5.310E-03	91	86
US 5287	(150)	3.70	2.63	0	5.06E-03	.1008	6.153E-03	.1232	6.922E-03	5.310E-03	91	86
US 5286	(150)	3.70	2.63	0	5.06E-03	.1008	6.153E-03	.1232	6.922E-03	5.310E-03	91	86
US 5285	(150)	3.70	2.63	0	5.06E-03	.1008	6.153E-03	.1232	6.922E-03	5.310E-03	91	86
US 5284	(150)	3.70	2.63	0	5.06E-03	.1008	6.153E-03	.1232	6.922E-03	5.310E-03	91	86
US 5283	(150)	3.70	2.63	0	5.06E-03	.1008	6.153E-03	.1232	6.922E-03	5.310E-03	91	86
US 5282	(150)	3.70	2.63	0	5.06E-03	.1008	6.153E-03	.1232	6.922E-03	5.310E-03	91	86
US 5281	(150)	3.70	2.63	0	5.06E-03	.1008	6.153E-03	.1232	6.922E-03	5.310E-03	91	86
US 5280	(150)	3.70	2.63	0	5.06E-03	.1008	6.153E-03	.1232	6.922E-03	5.310E-03	91	86
US 5279	(150)	3.70	2.63	0	5.06E-03	.1008	6.153E-03	.1232	6.922E-03	5.310E-03	91	86
US 5278	(150)	3.70	2.63	0	5.06E-03	.1008	6.153E-03	.1232	6.922E-03	5.310E-03	91	86
US 5277	(150)	3.70	2.63	0	5.06E-03	.1008	6.153E-03	.1232	6.922E-03	5.310E-03	91	86
US 5276	(150)	3.70	2.63	0	5.06E-03	.1008	6.153E-03	.1232	6.922E-03	5.310E-03	91	86
US 5275	(150)	3.70	2.63	0	5.06E-03	.1008	6.153E-03	.1232	6.922E-03	5.310E-03	91	86
US 5274	(150)	3.70	2.63	0	5.06E-03							





Pic. No. 5319 H/HREF = .0376 BOOSTER
.0423 ORBITER



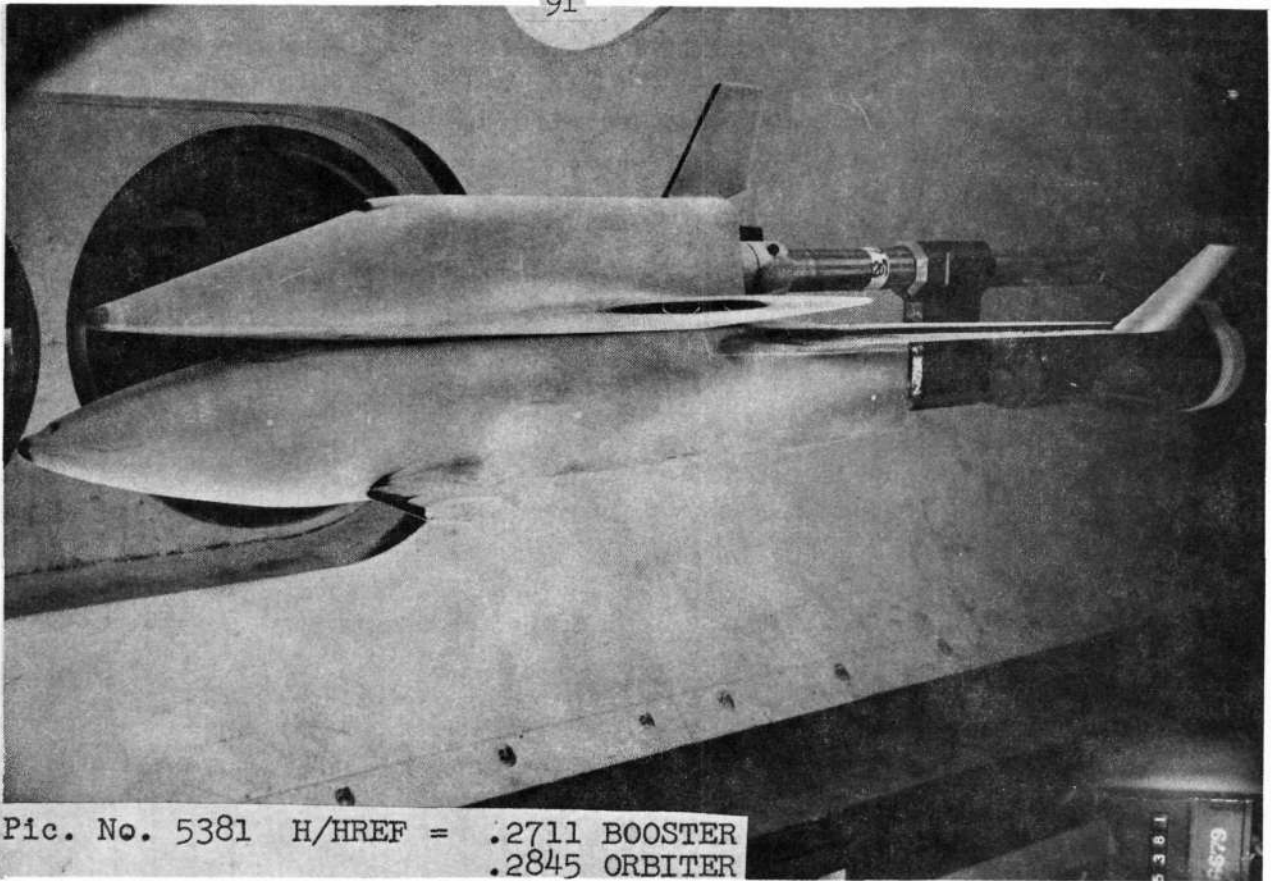
Pic. No. 5329 H/HREF = .0288 BOOSTER
.0325 ORBITER

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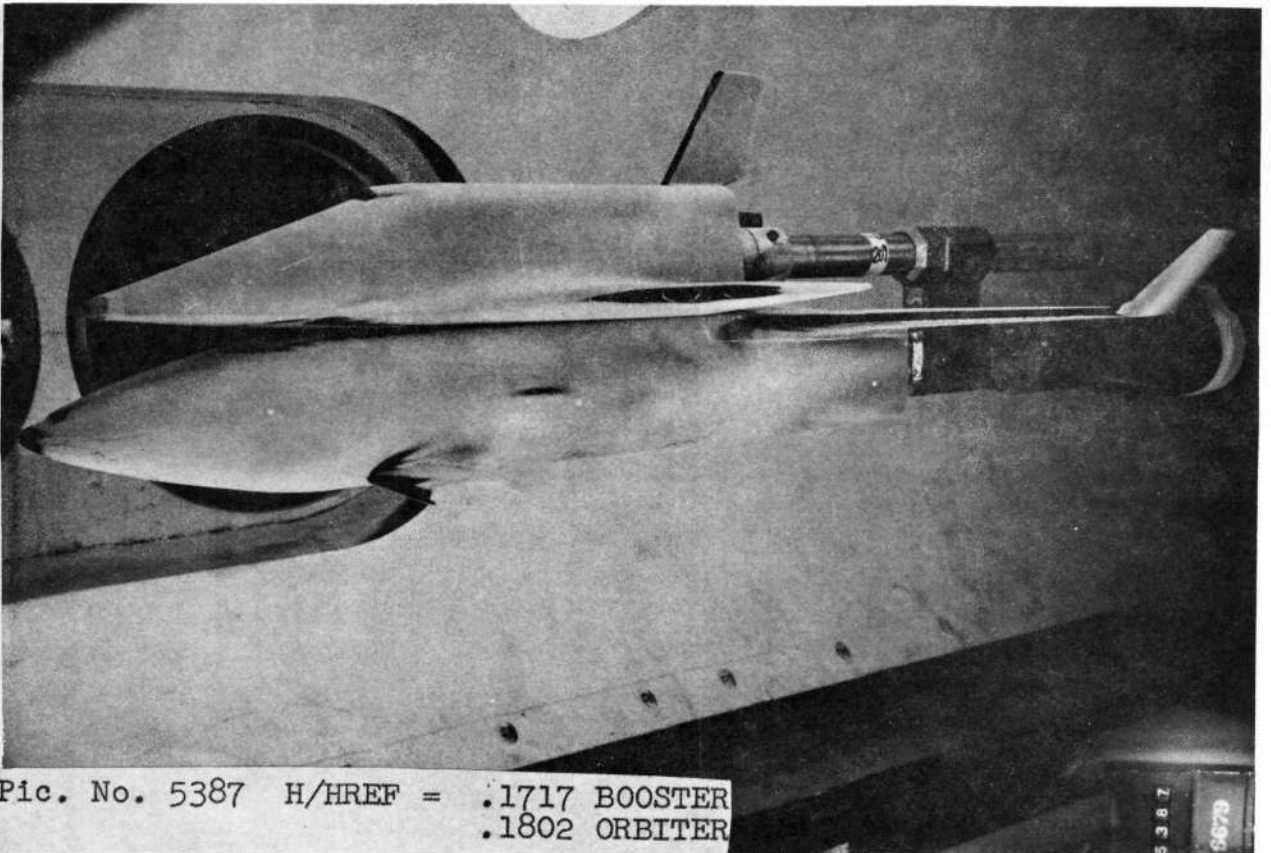
AEOLIO, INC. 1 ARNOLD AFB, TENNESSEE
VON KARMAN GAS DYNAMICS FACILITY
50 INCH HYPERSONIC TUNNEL B
VILLAGE

GROUP 3222 CONFIG MODEL MACH NO 0.00 PO PSIA 854.2 TD DEG R 1369 ALPHA=MODEL ALPHA-SECTOR ALPHA-PREBEND ROLL-MODEL YAW
209 3222 PDAC-B-DWC 0.00 854.2 1369
1-1NF 0-1NF V-1NF RHO-1NF MU-1NF ECFT MREF SINEF
(UEG R) (PSIA) (F1/SEC) (SLUGS/F13) (LB-SEC/F12) (F1-1) (G -0.11FT) (A -0.11FT)
99.2 087 3.920 3.905 7.399E-05 7.987E-08 3.62E 06 6.256E-02 2.087E-02
CAMERA PAINT TEMP (DEG F) INITIAL TEMP (DEG F) SQUARE ROOT (MMOLCKN)
TOP(T) 300
SIDE(US) 550 AVERAGE T_u = 91.181
SIDE(LS) 550 AVERAGE T_u = 80.101
-0.000(SQUARE ROOT DEL TIME) * 0.11

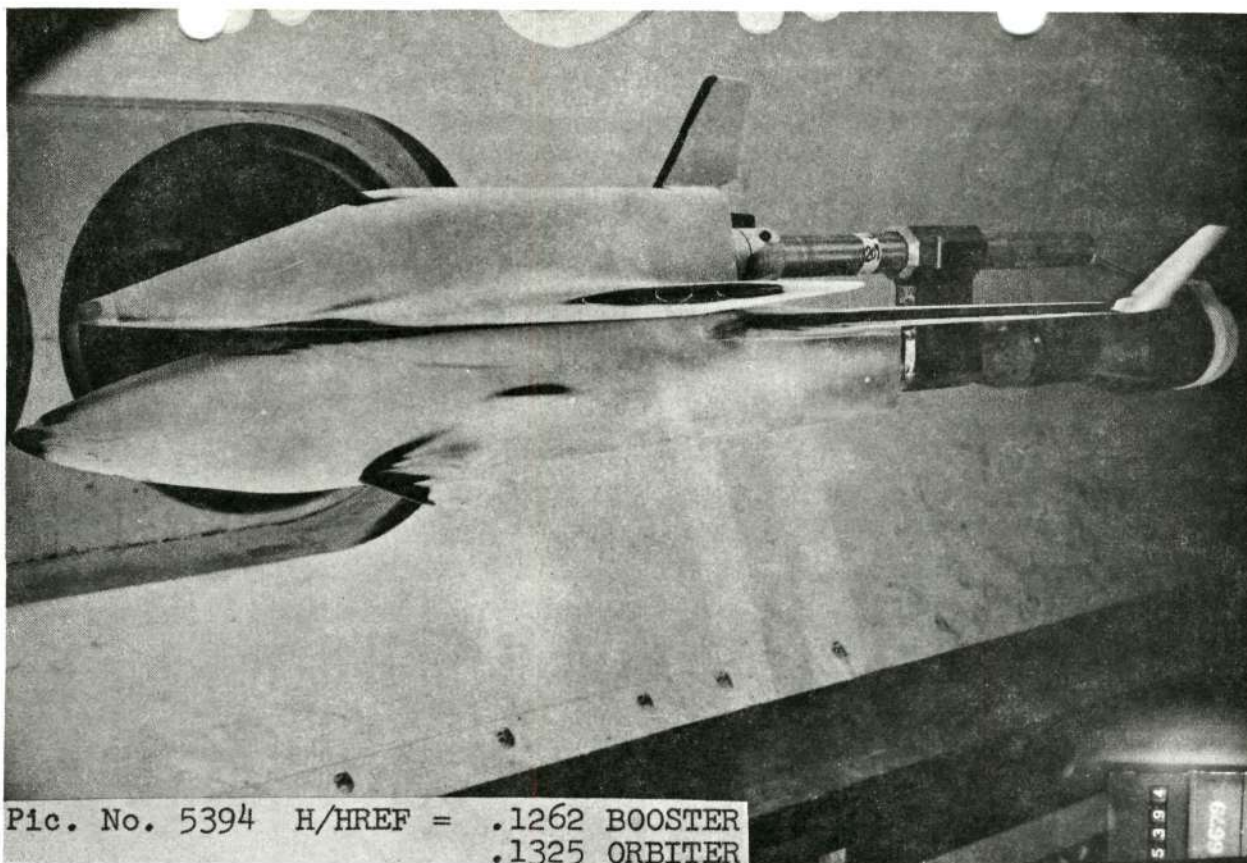
PIC MC	TIME DELTME	M(TO)	M(TO)/MREF	M(.910)	M(.8510)/MREF	M(.8510)	M(.8510)/MREF	ST(10)	MODEL TEMP F				
US 5381 (1550)	3.70	2.66	0 3.82E-02	.9301	8.923E-02	1.4268	1.238E-01	1.9194	2.449E-02	94	88	0	00
US 5381 (1300)	3.70	2.66	0 1.70E-02	.2711	2.153E-02	.3466	2.449E-02	.3909	7.234E-03	94	88	0	00
US 5381 (1550)	3.70	2.66	0 3.70E-02	.9106	8.743E-02	1.3972	1.212E-01	1.9392	2.398E-02	94	88	0	00
US 5381 (1300)	3.70	2.66	0 1.70E-02	.2845	2.261E-02	.3015	2.616E-02	.4193	7.593E-03	94	88	0	00
US 5387 (1550)	6.85	5.01	0 3.68E-02	.5889	3.654E-02	.9035	7.801E-02	1.2534	1.551E-02	96	89	0	00
US 5387 (1300)	6.85	5.01	0 1.07E-02	.1717	1.365E-02	.2182	1.580E-02	.2526	4.581E-03	96	89	0	00
US 5387 (1550)	6.85	5.01	0 3.61E-02	.5766	5.533E-02	.8847	7.877E-02	1.2273	1.518E-02	96	89	0	00
US 5387 (1300)	6.85	5.01	0 1.13E-02	.1802	1.432E-02	.2289	1.637E-02	.2649	4.808E-03	96	89	0	00
US 5394 (1550)	10.55	9.51	0 2.71E-02	.4330	4.153E-02	.6643	5.705E-02	.9216	1.140E-02	102	89	0	01
US 5394 (1300)	10.55	9.51	0 1.90E-02	.1202	1.002E-02	.1604	1.162E-02	.1857	3.368E-03	102	89	0	01
US 5394 (1550)	10.55	9.51	0 2.65E-02	.4260	4.063E-02	.6505	5.645E-02	.9024	1.116E-02	102	89	0	01
US 5394 (1300)	10.55	9.51	0 8.29E-03	.1325	1.053E-02	.1683	1.210E-02	.1947	3.535E-03	102	89	0	01
US 5400 (1550)	13.75	12.71	0 2.24E-02	.3573	3.433E-02	.5589	4.162E-02	.7615	9.422E-03	109	90	0	01
US 5400 (1300)	13.75	12.71	0 0.52E-03	.1043	0.289E-03	.1325	4.162E-02	.1536	2.703E-03	109	90	0	01
US 5400 (1550)	13.75	12.71	0 2.19E-02	.3503	3.381E-02	.5375	4.663E-02	.7456	9.224E-03	109	90	0	01
US 5400 (1300)	13.75	12.71	0 0.60E-03	.1095	0.695E-03	.1391	1.006E-02	.1699	2.921E-03	109	90	0	01



Pic. No. 5381 H/HREF = .2711 BOOSTER
.2845 ORBITER

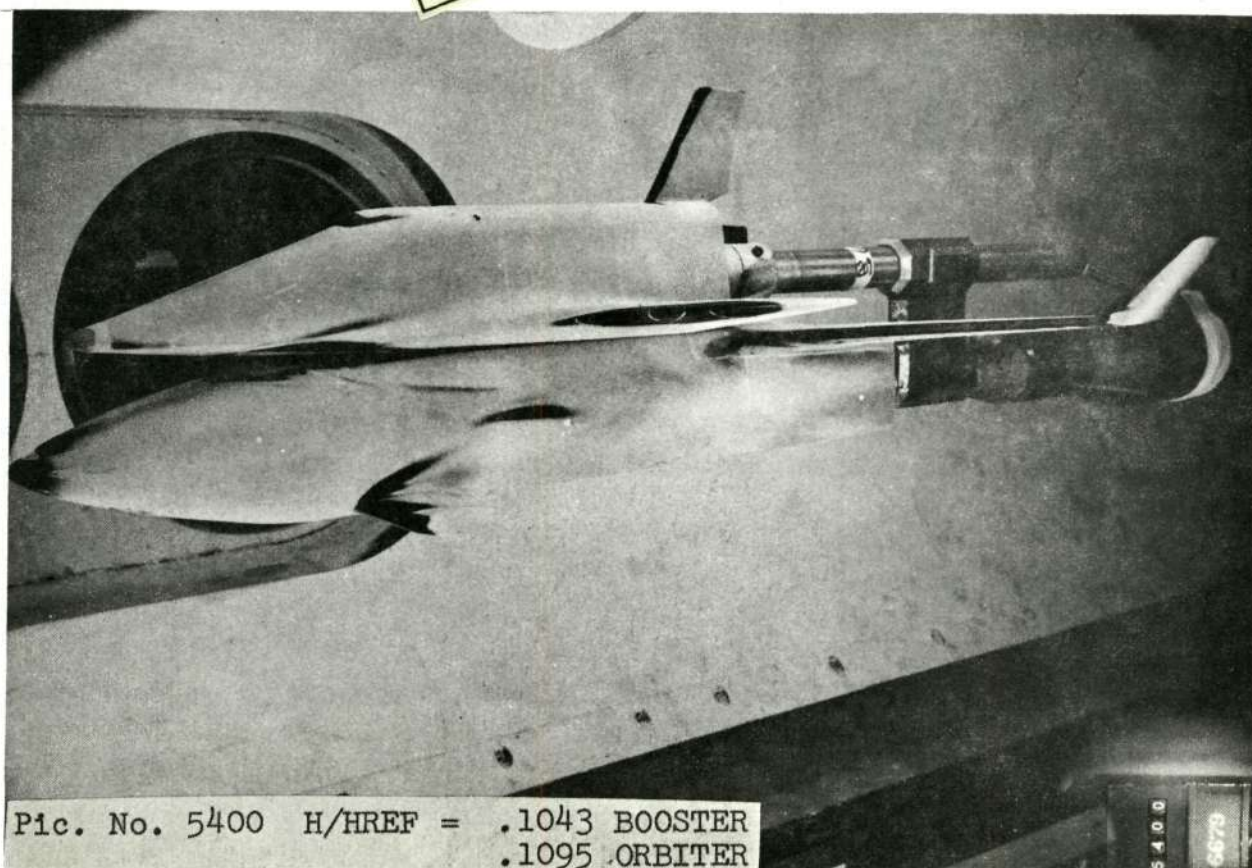


Pic. No. 5387 H/HREF = .1717 BOOSTER
.1802 ORBITER



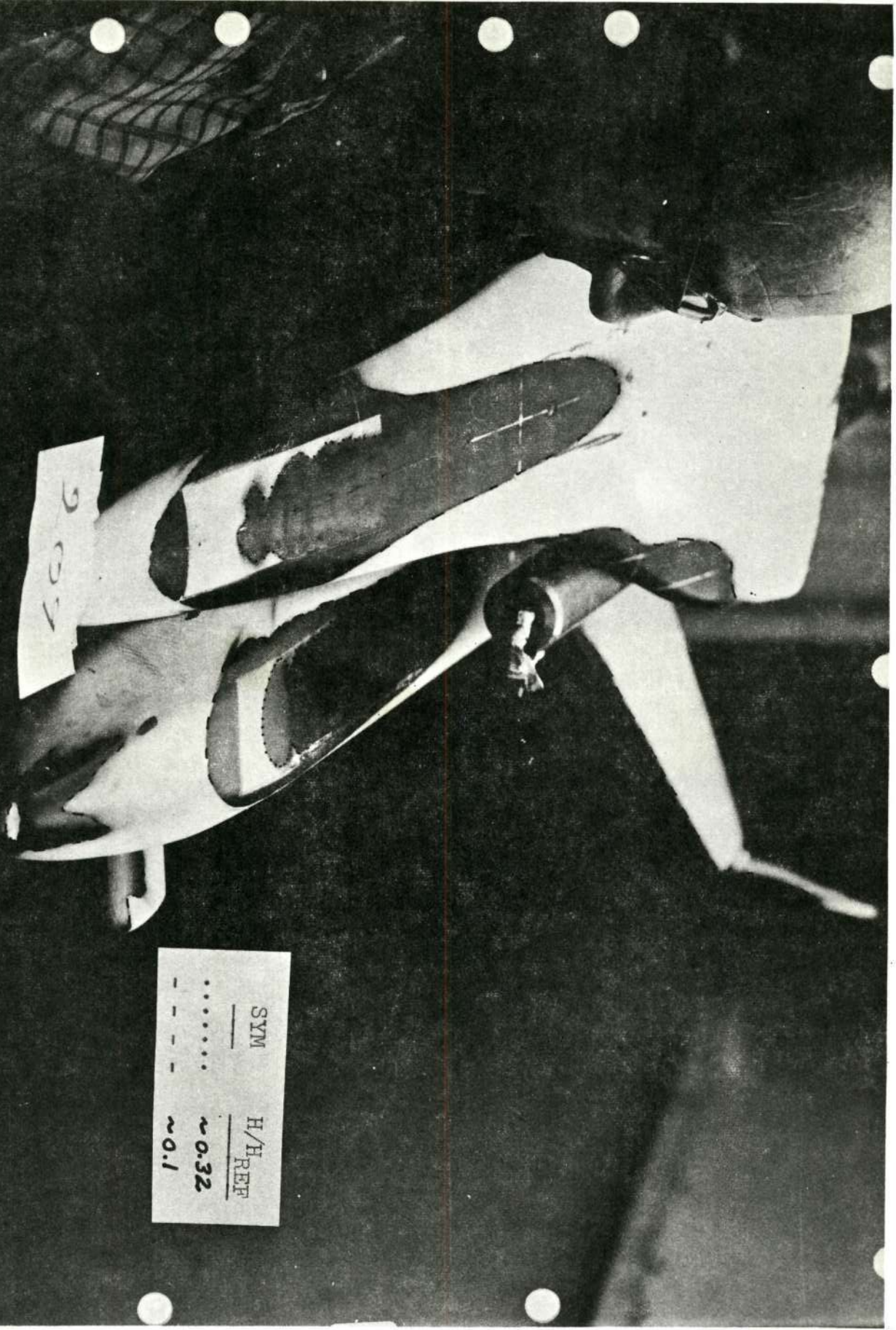
Pic. No. 5394 H/HREF = .1262 BOOSTER
.1325 ORBITER

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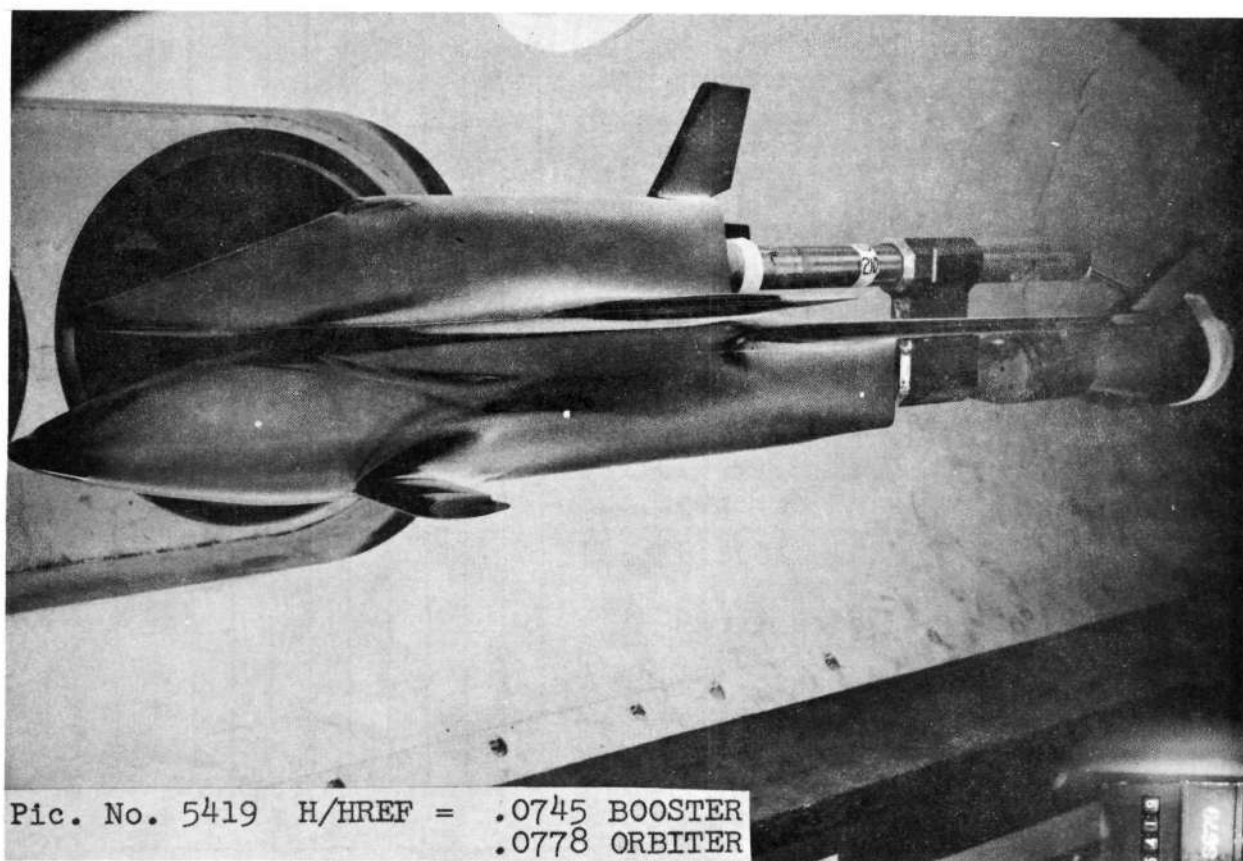
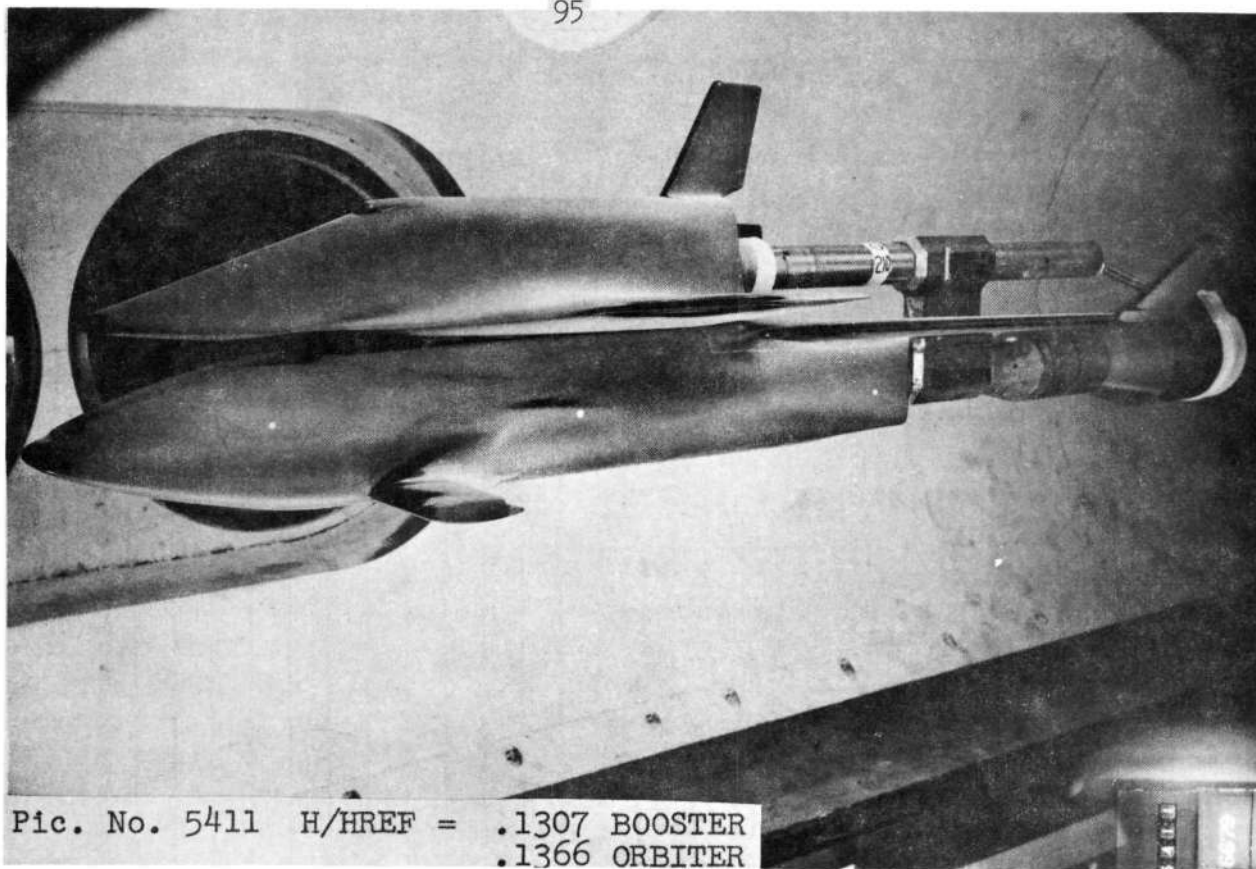


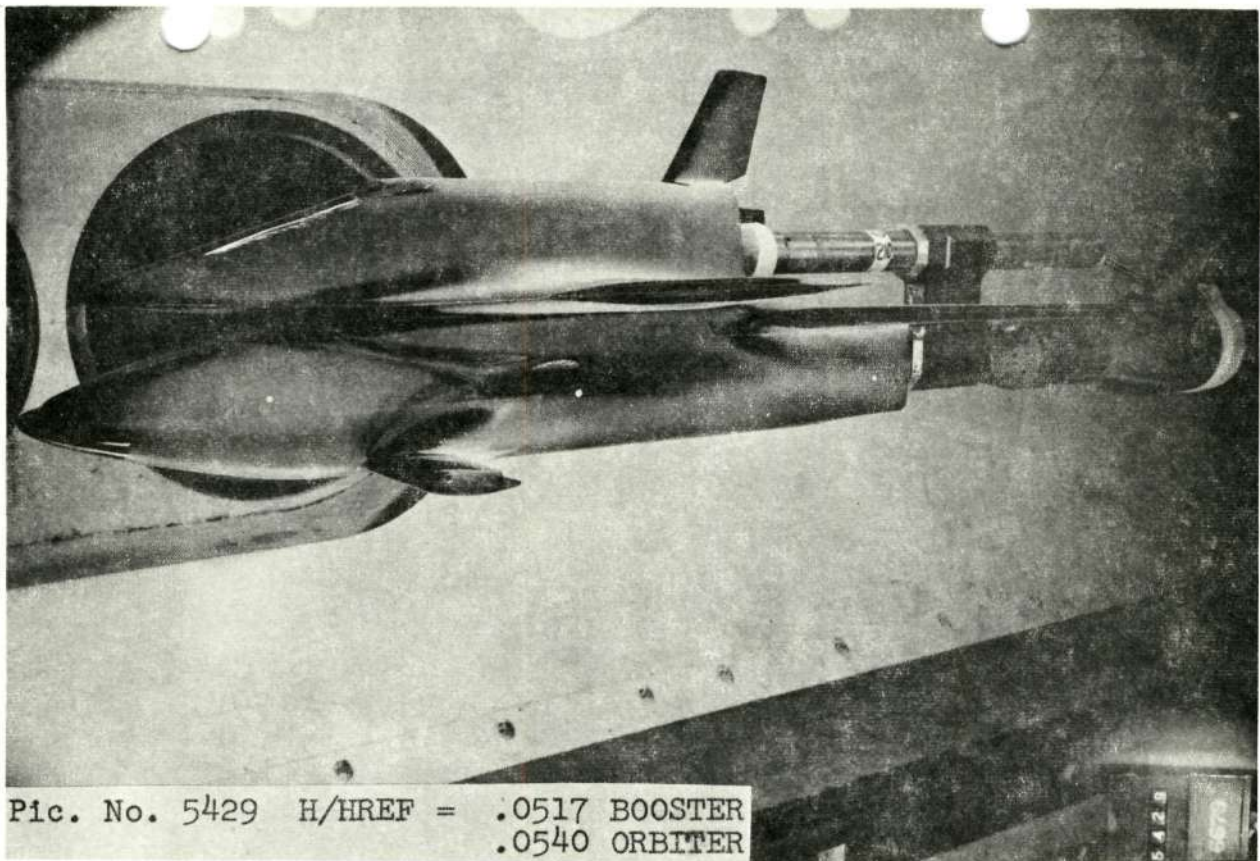
Pic. No. 5400 H/HREF = .1043 BOOSTER
.1095 ORBITER

Group 209 Re/ft 3.7x10⁶ ALPHA 0
 POST-TEST PHOTOGRAPH OF INTERFERENCE REGION



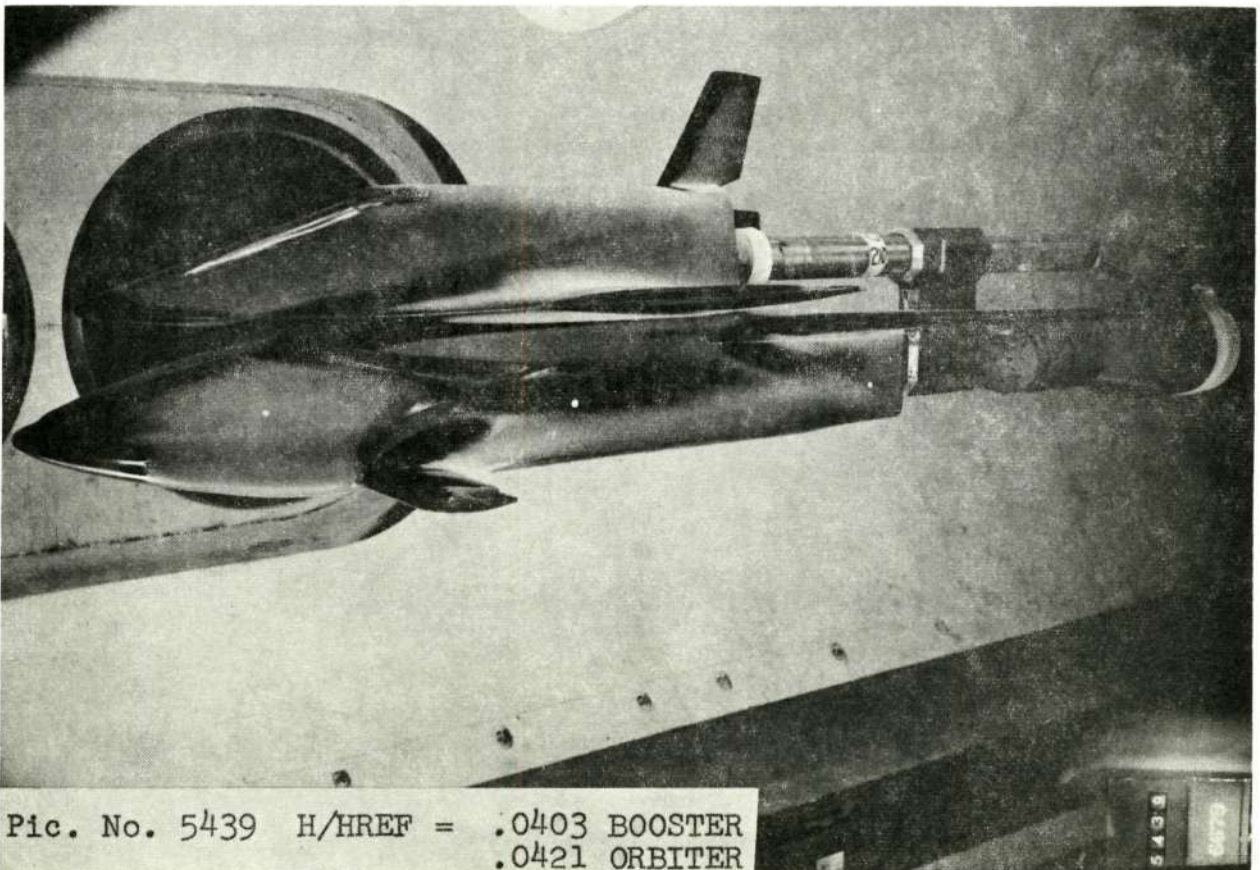
SYM	H/H _{REF}
.....	~0.32
- - - -	~0.1





Pic. No. 5429 H/HREF = .0517 BOOSTER
.0540 ORBITER

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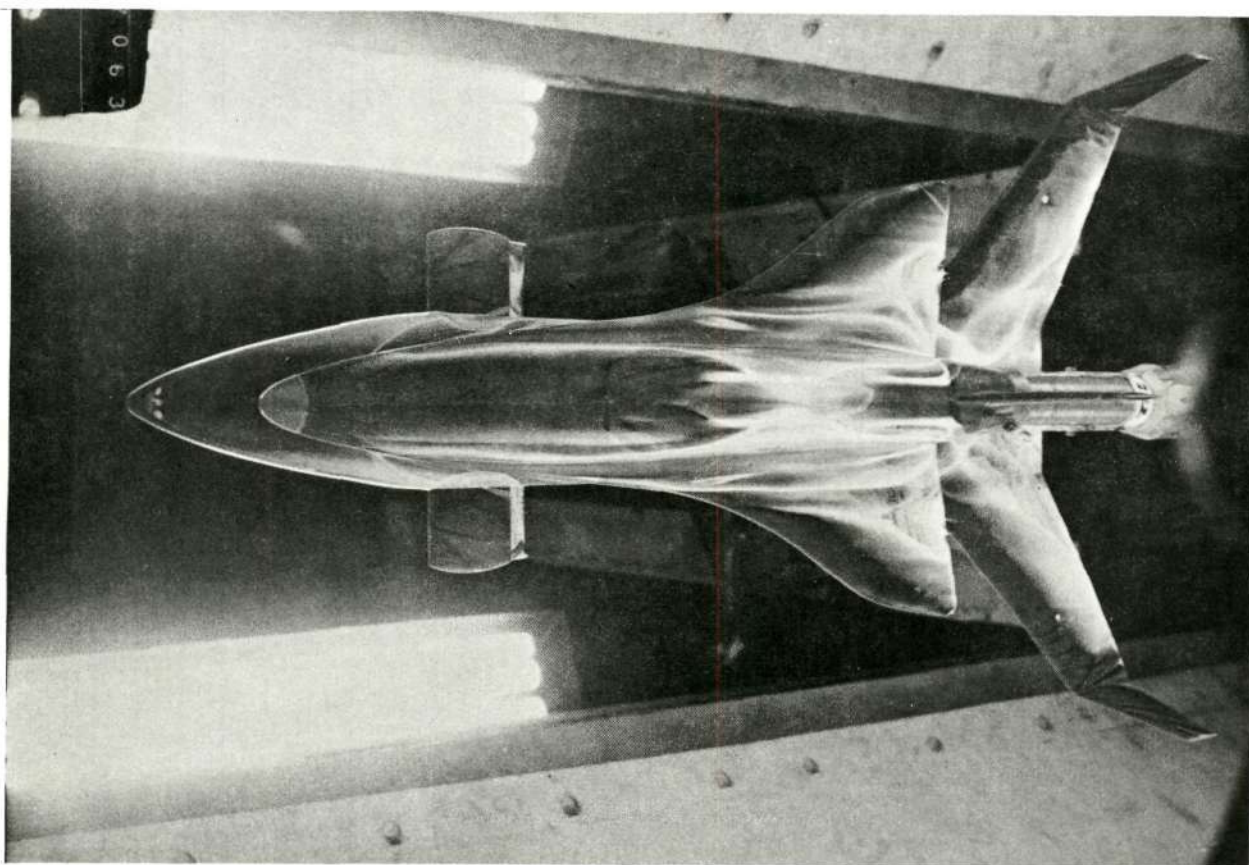
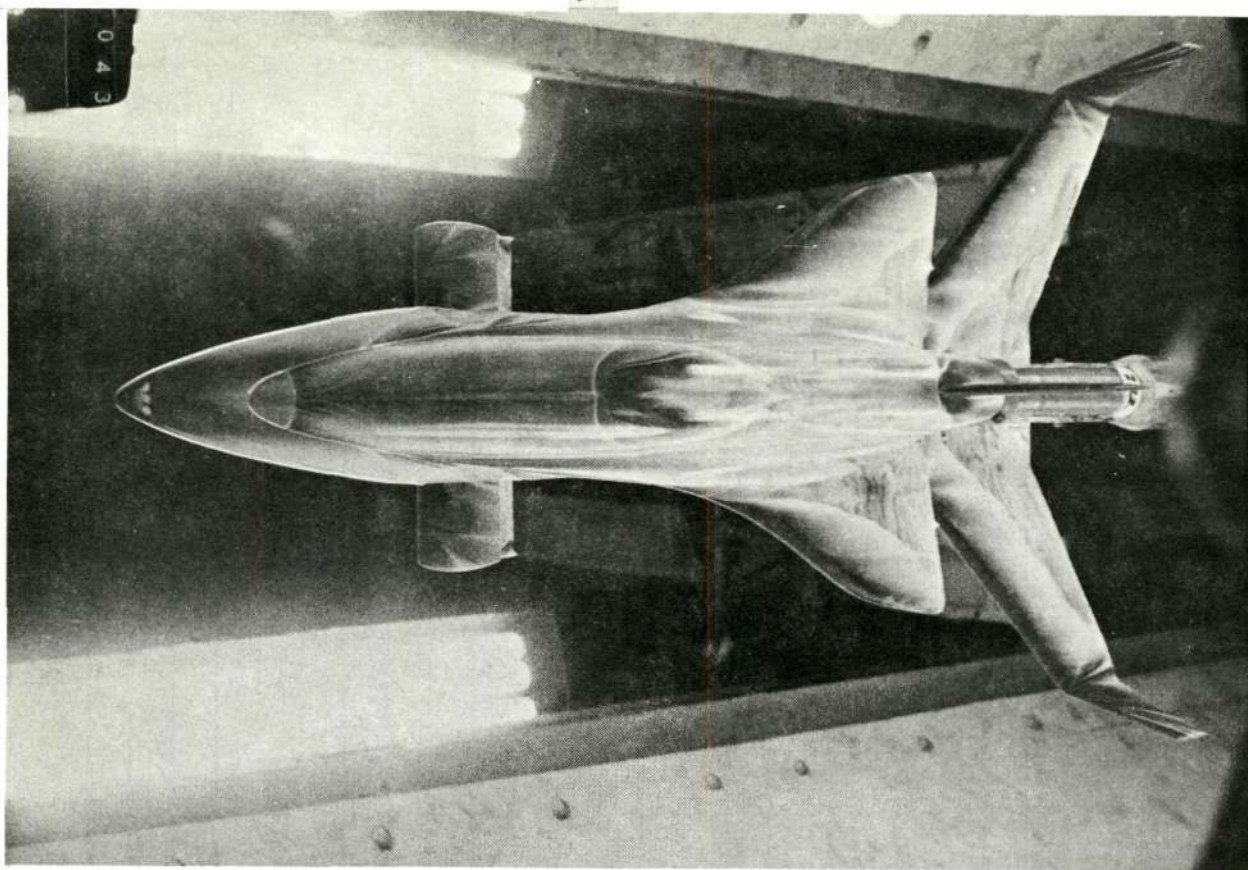


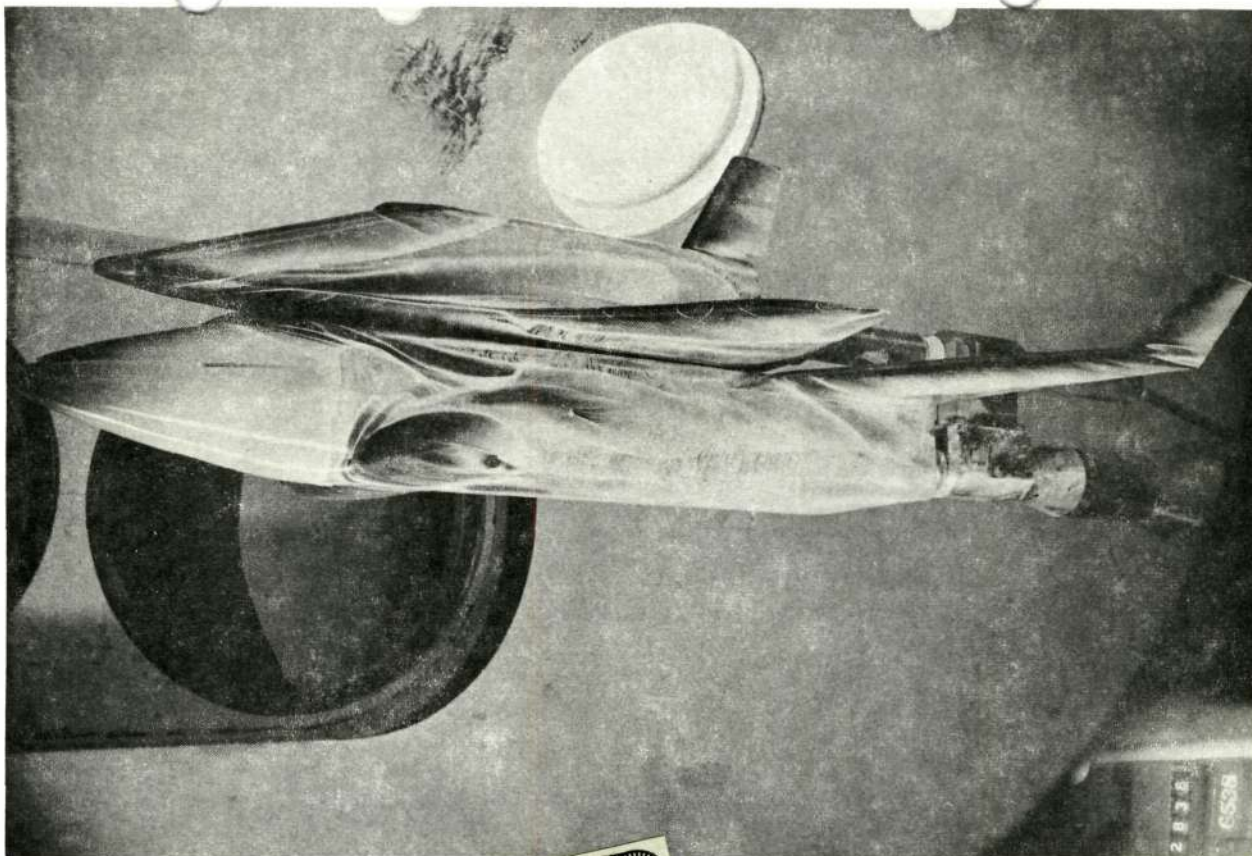
Pic. No. 5439 H/HREF = .0403 BOOSTER
.0421 ORBITER

AEDC(AMO, INC.) ARNOLD AFS, TENNESSEE
VUM KAMMAN GAS DYNAMICS FACILITY
50 INCH HYPERSONIC TUNNEL B
V11162

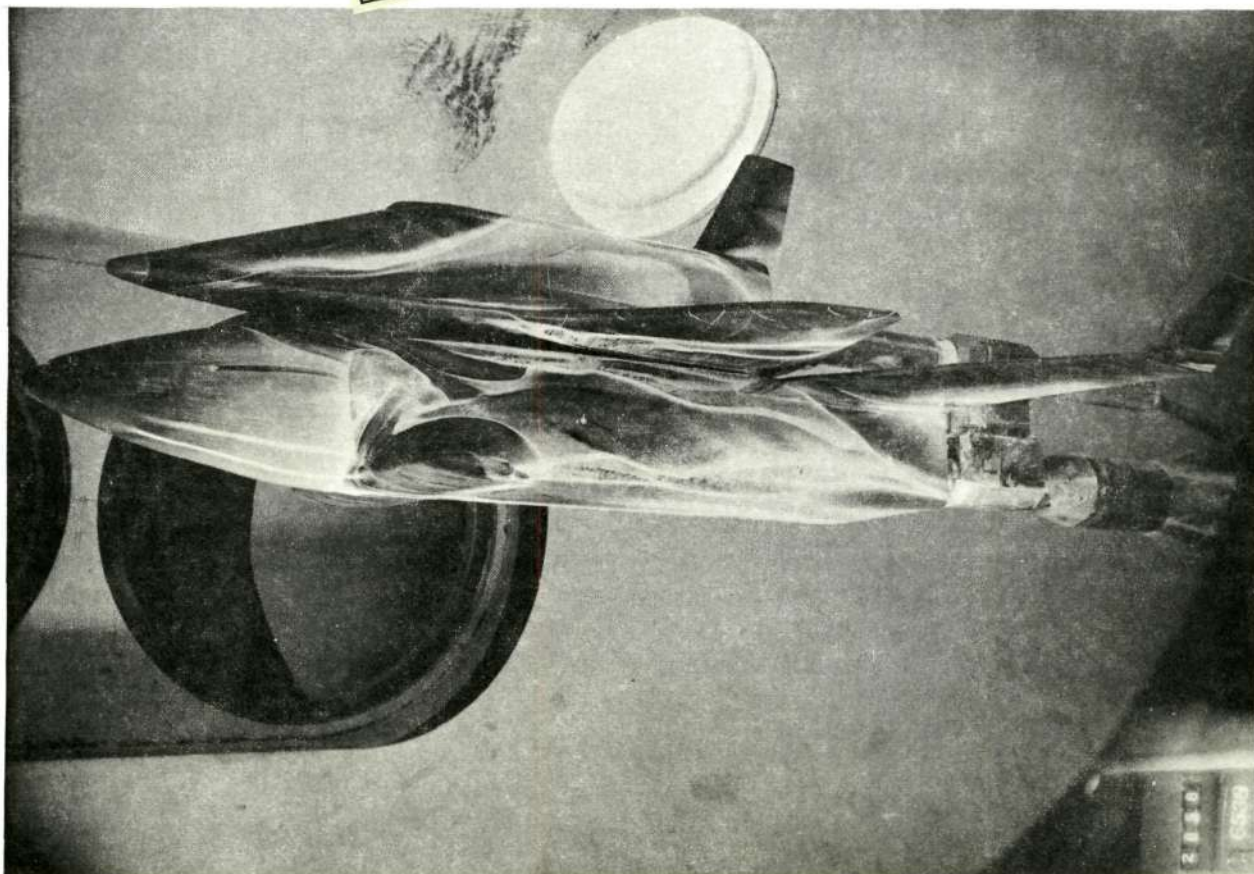
T-1NF	P-1NF	U-1NF	V-1NF	RNO-1NF	PU-1NF	HE/FT	HREF	SINF
(UE6 M)	(P5 IA)	(P5 IA)	(F17 SEC)	(STUGS/F13)	(L0-SLC/F12)	(F1*)	(R= .011F)	(R= .011F)
94.6	.056	2.527	3812	5.003E-05	7.015E-06	2.20E 06	4.981E-02	3.452E-02

97





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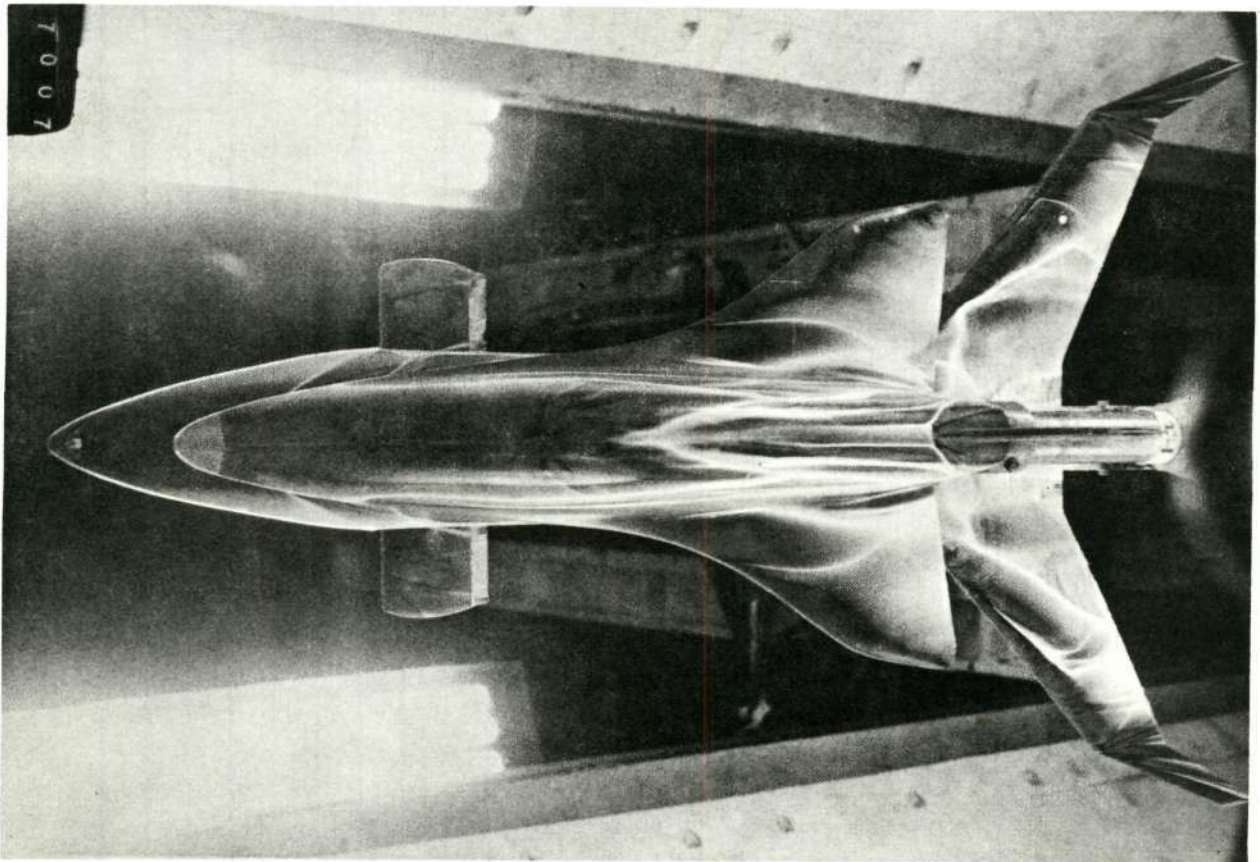
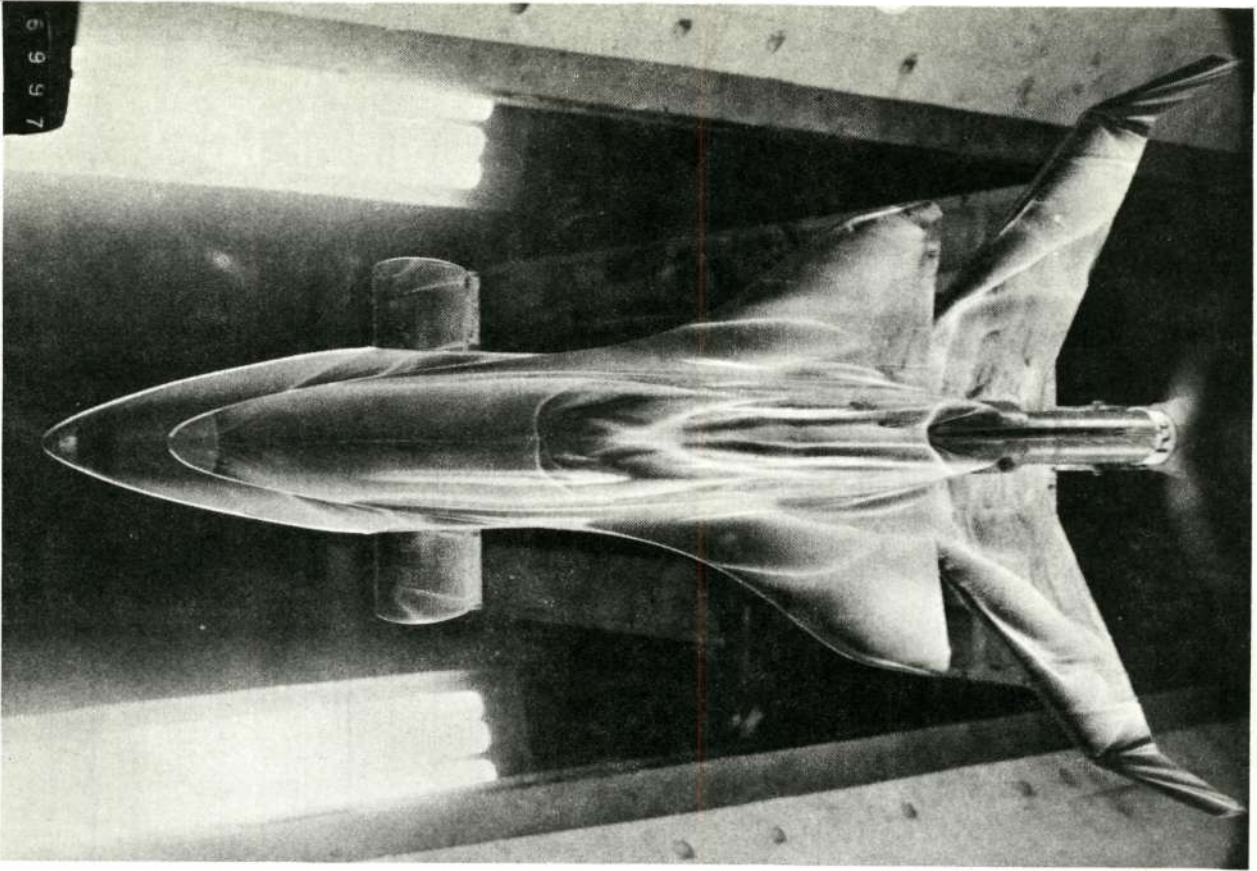


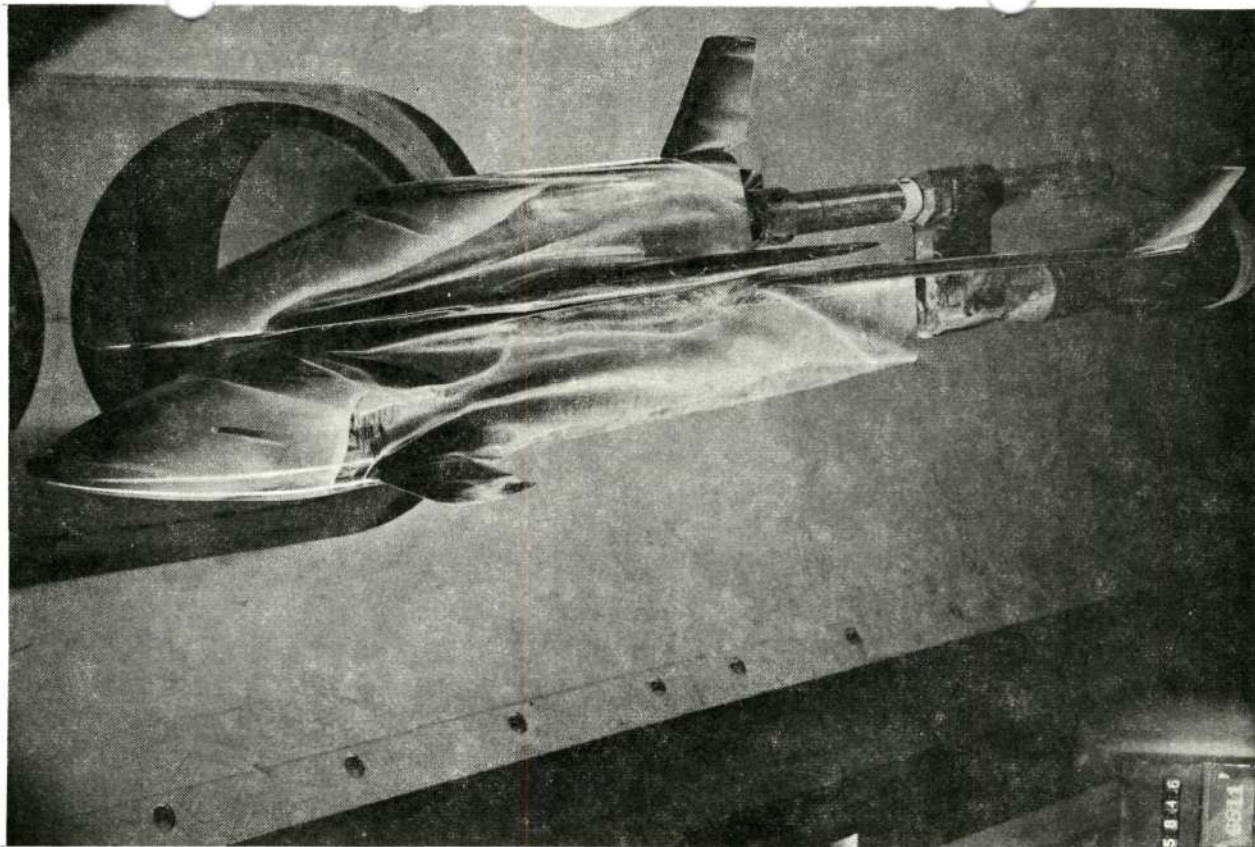
6/ 3/71

AEDC(ARO,INC.) ARNOLD AFS, TENNESSEE
VON KARMAN GAS DYNAMICS FACILITY
50 INCH HYPERSONIC TUNNEL B
VT1162

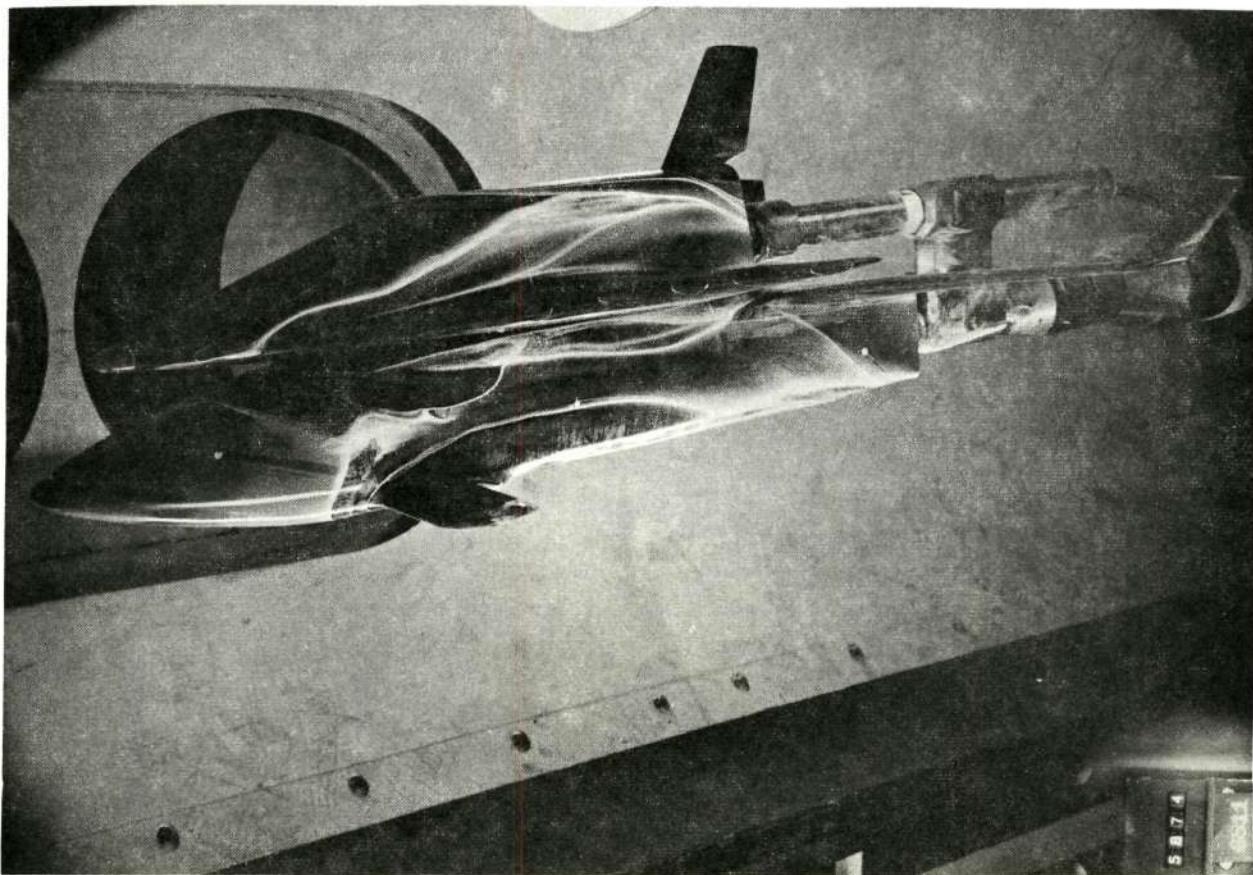
GROUP	CONF IG	MODEL	MACH NO	PO PSIA	TO DEG R	ALPHA-MODEL	ALPHA-SECTION	ALPHA-PREBEND	ROLL-MODEL	YAW
221	3222	WDAC-R+DWC	8.00	548.7	1310	-5.02	-5.02	0	0	0
T-1NF	P-1NF	Q-1NF	V-1NF	RHO-1NF	MU-1NF	REF/FT	HREF	SINEF		
(UEG R)	(PSIA)	(PSIA)	(FT/SEC)	(SLUGS/FT3)	(LB-SEC/FT2)	(FT-1)	(R= .011FT)	(N= .011FT)		
94.9	.056	2.51R	3819	4.969E-05	7.640E-08	2.48E 06	4.976E-02	3.264E-02		

OIL FLOW





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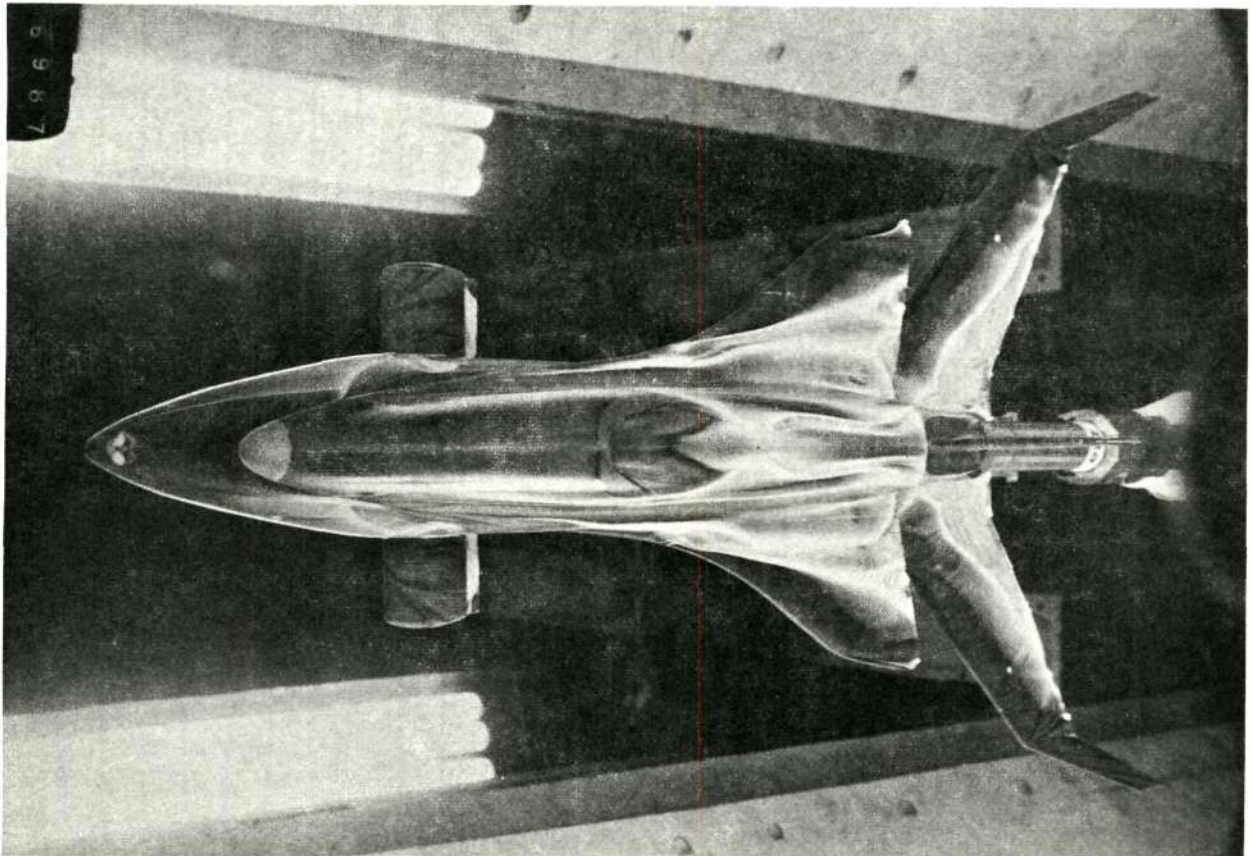
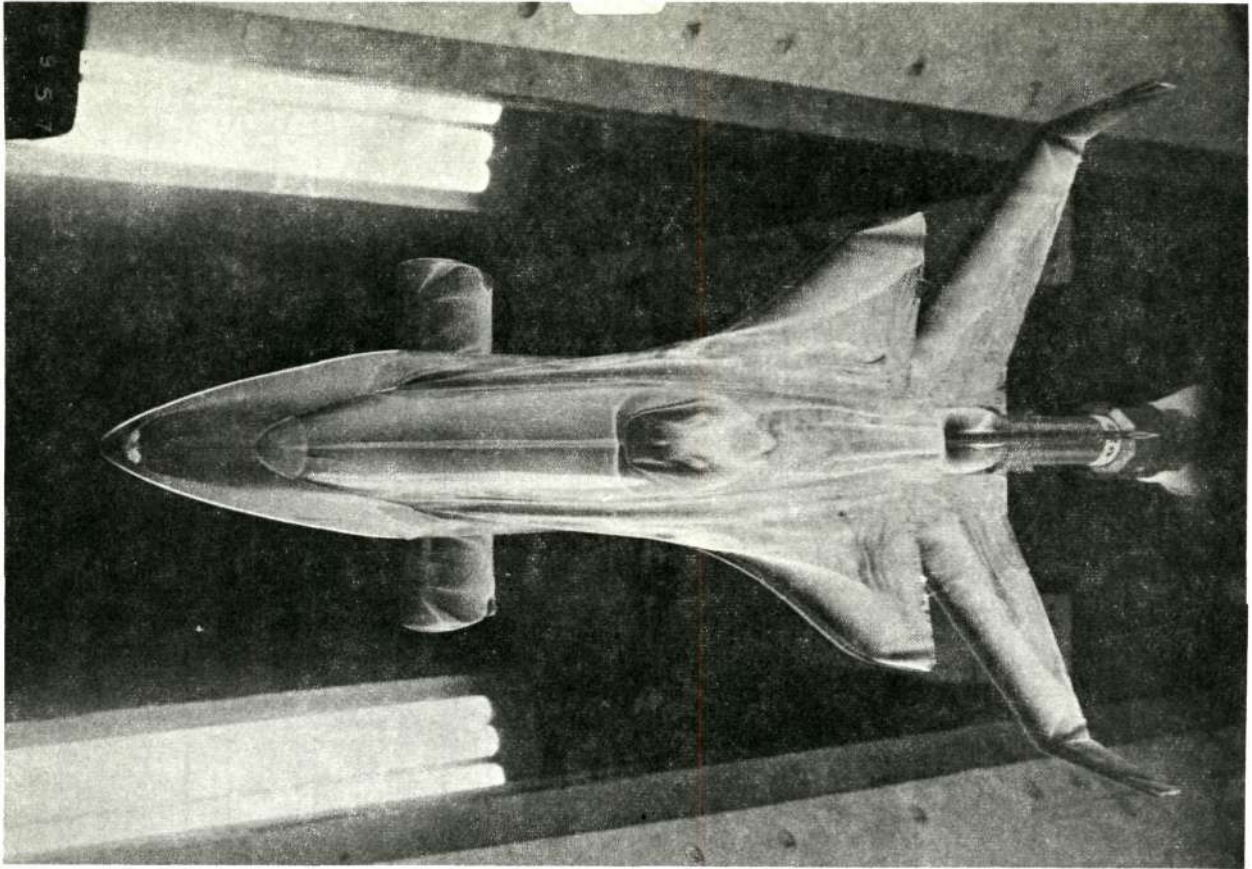
6/ 3/71

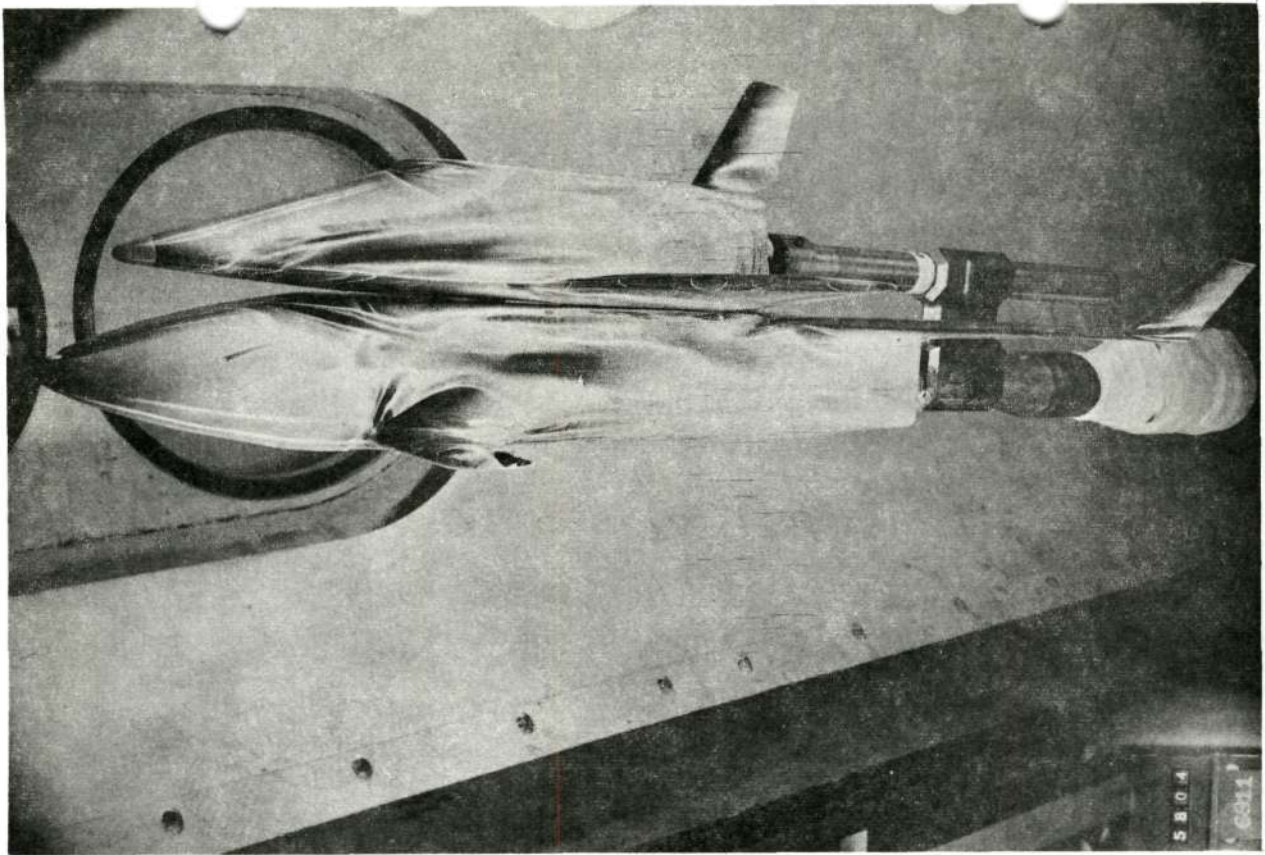
AEDC(ARO,INC.) ARNOLD AFS, TENNESSEE
VON KARMAN GAS DYNAMICS FACILITY
50 INCH HYPERSONIC TUNNEL B
V11162

GROUP	CONFID	MODEL	MACH NO	PO PSIA	TU DEG R	ALPHA-MODEL	ALPHA-SECTION	ALPHA-PREBEND	ROLL-MODEL	VAR
220	3222	WUAC-B-D-06	8.00	549.5	1308	5.01	5.01	0	0	0

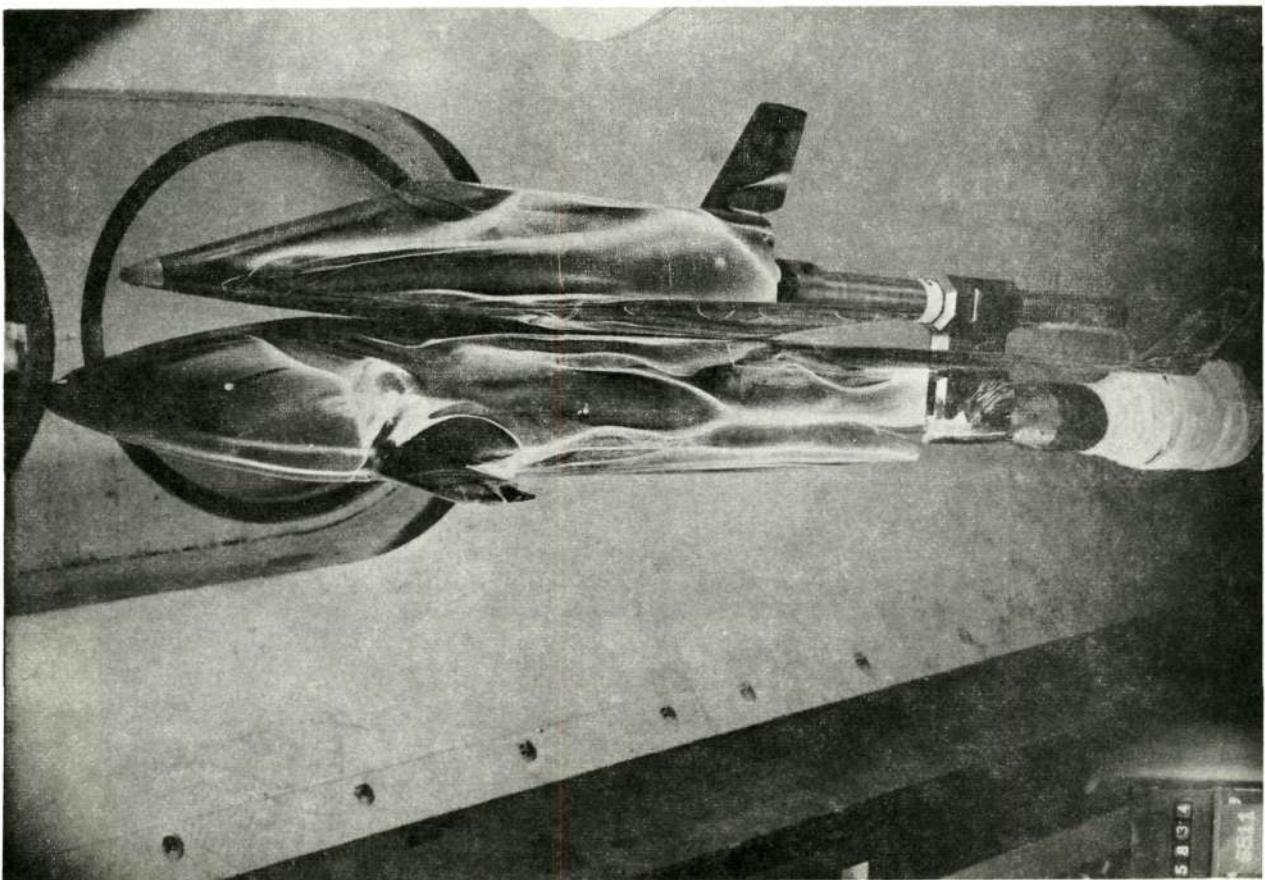
T-INF	P-INF	O-INF	V-INF	RHO-INF	MU-INF	RE/FT	hREF	S1REF
(DEG R)	(PSIA)	(PSIA)	(FT/SEC)	(SLUGS/FT ³)	(LB-SEC/FT ²)	(FT-1)	(R= .01/FT)	(R= .01/FT)
94.8	.056	2.522	3917	4.990E-05	7.634E-08	2.49E 06	4.978E-02	3.260E-02

OIL FLOW

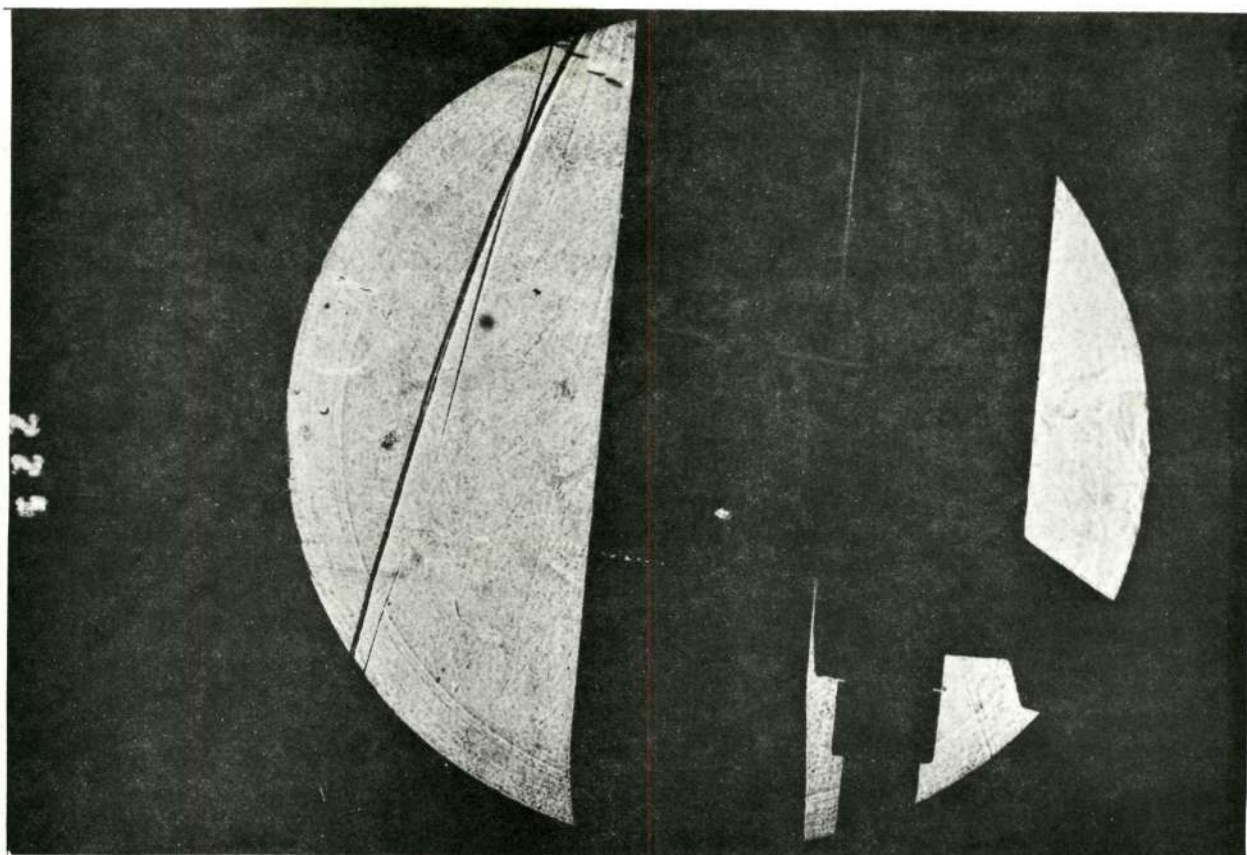
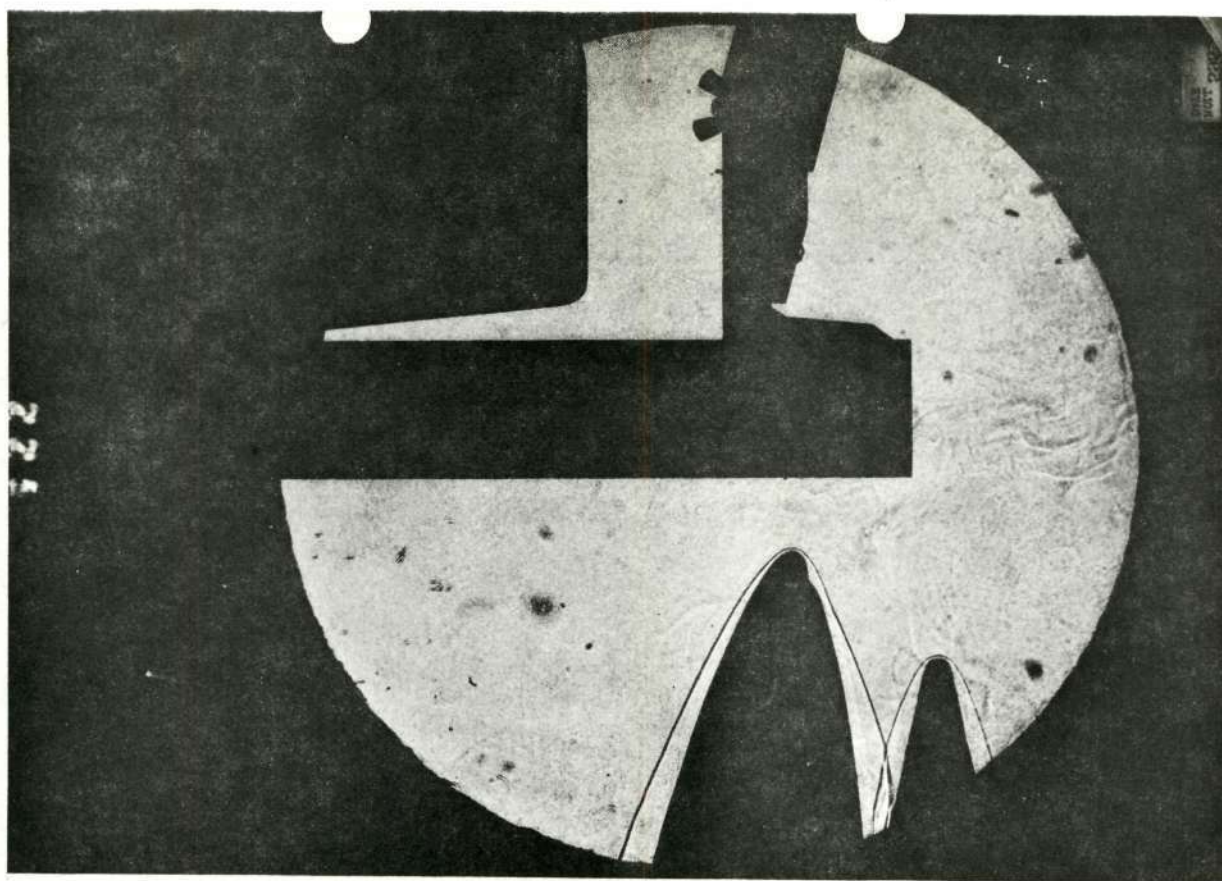




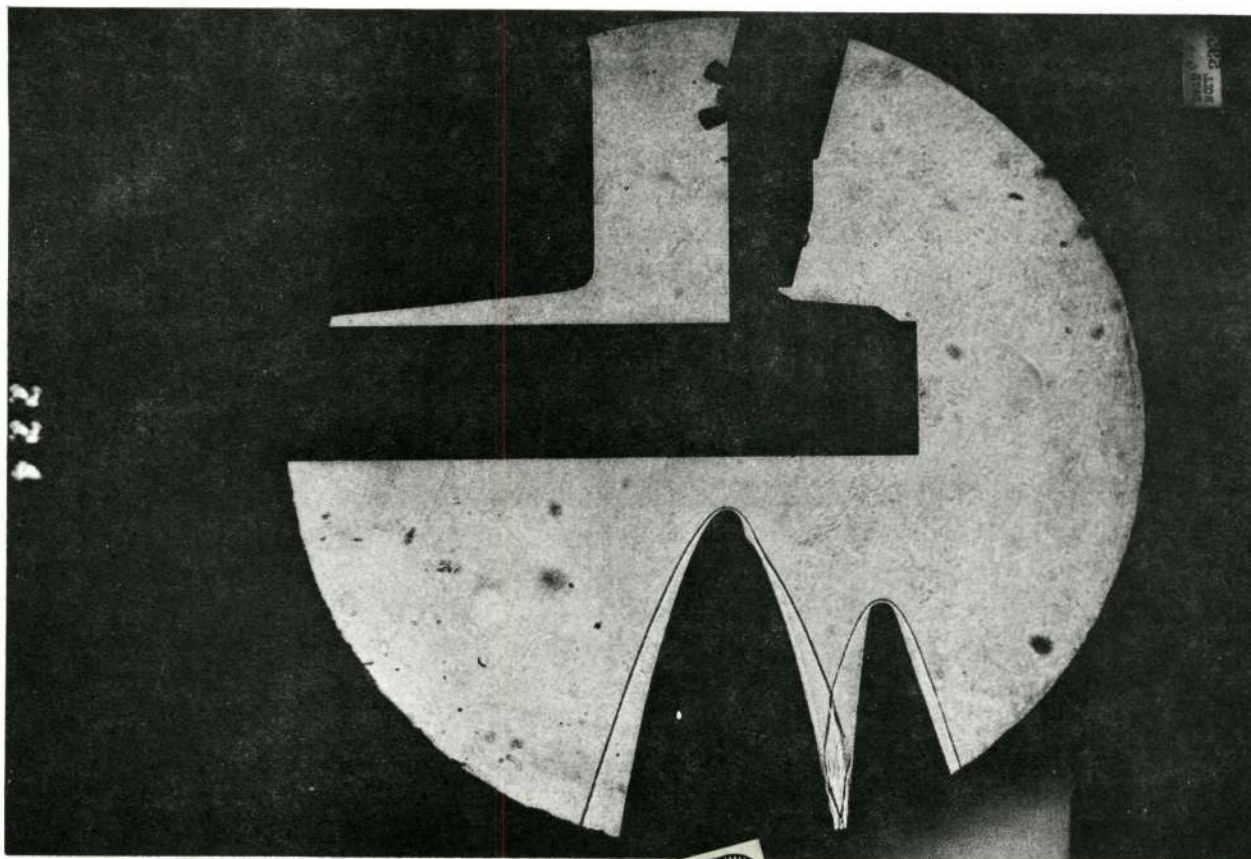
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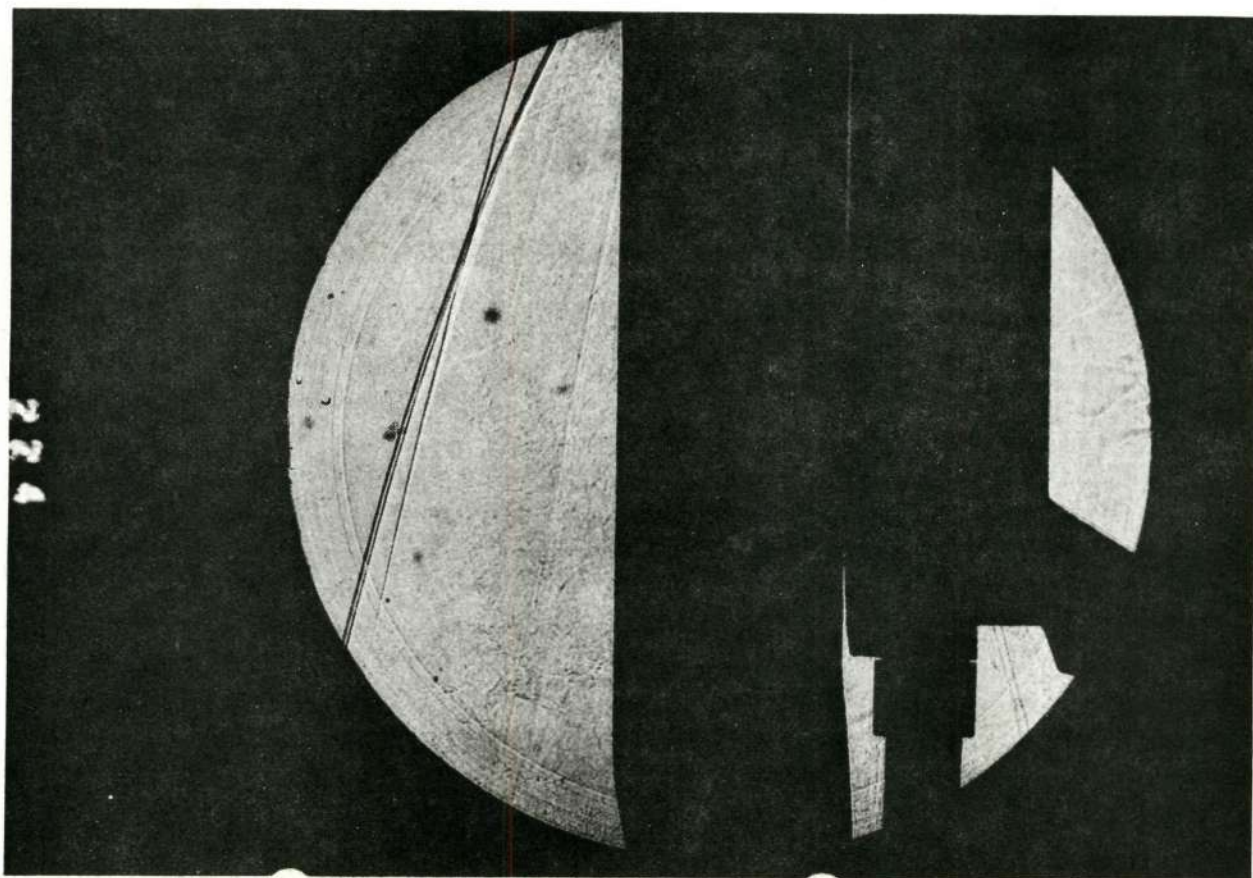
Shadowgraph Photograph at $\alpha = +5$, $\phi = 0$, $\text{Re}/\text{ft} = 2.5 \times 10^6$

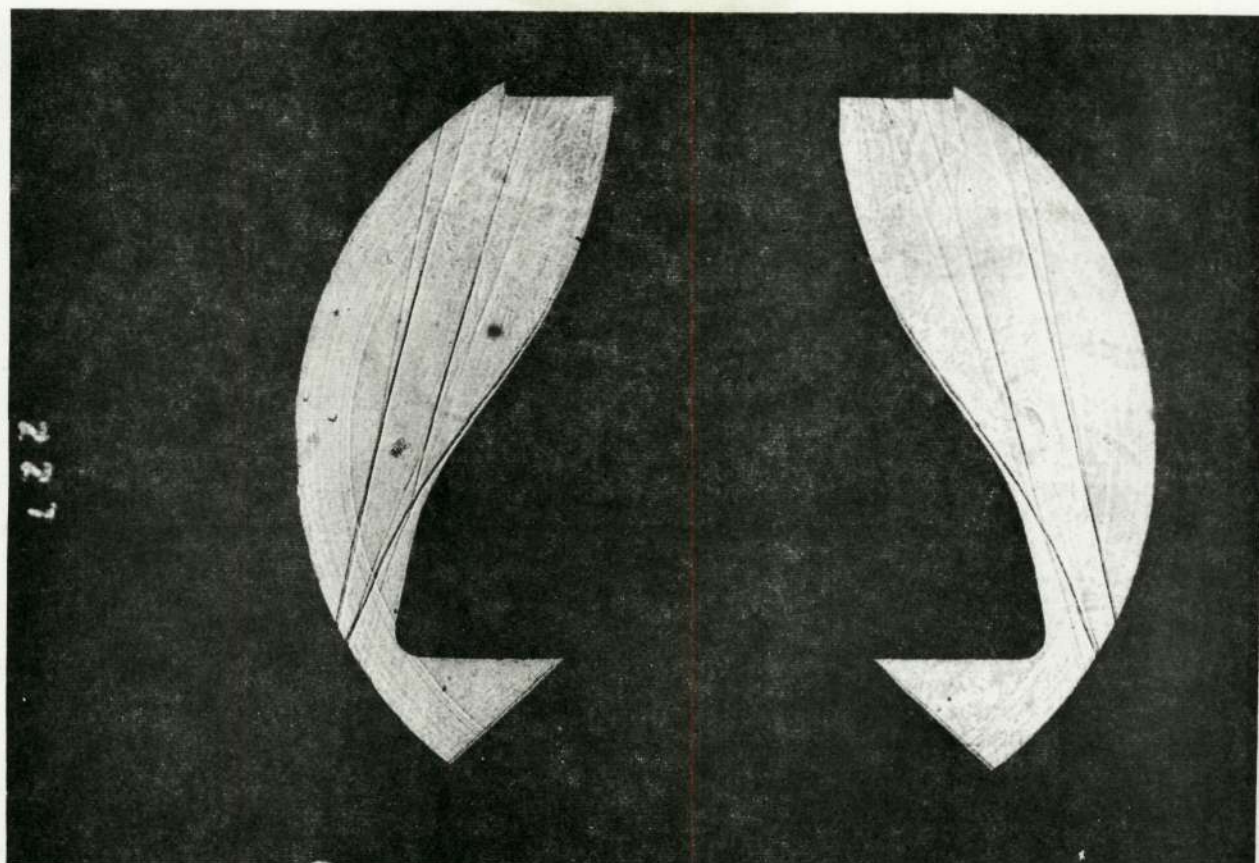
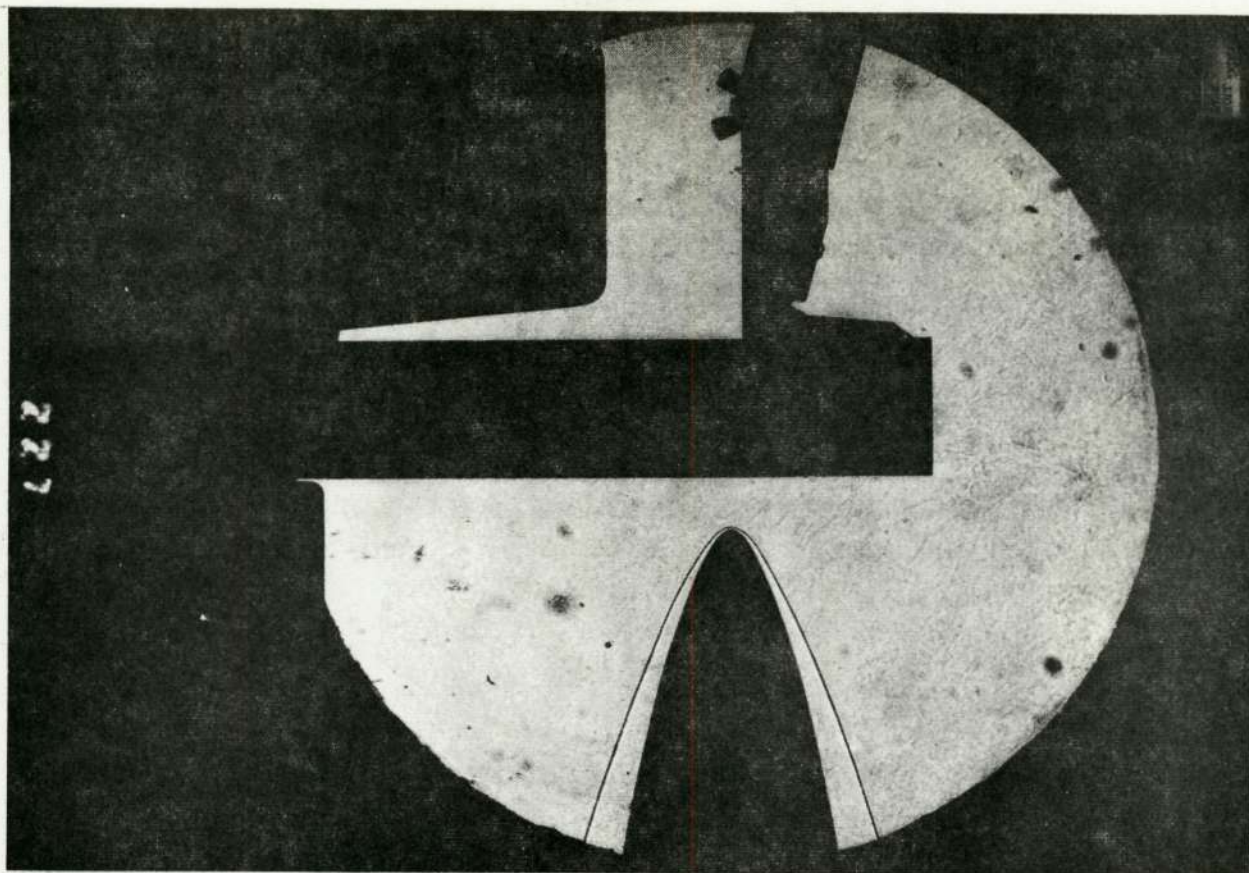


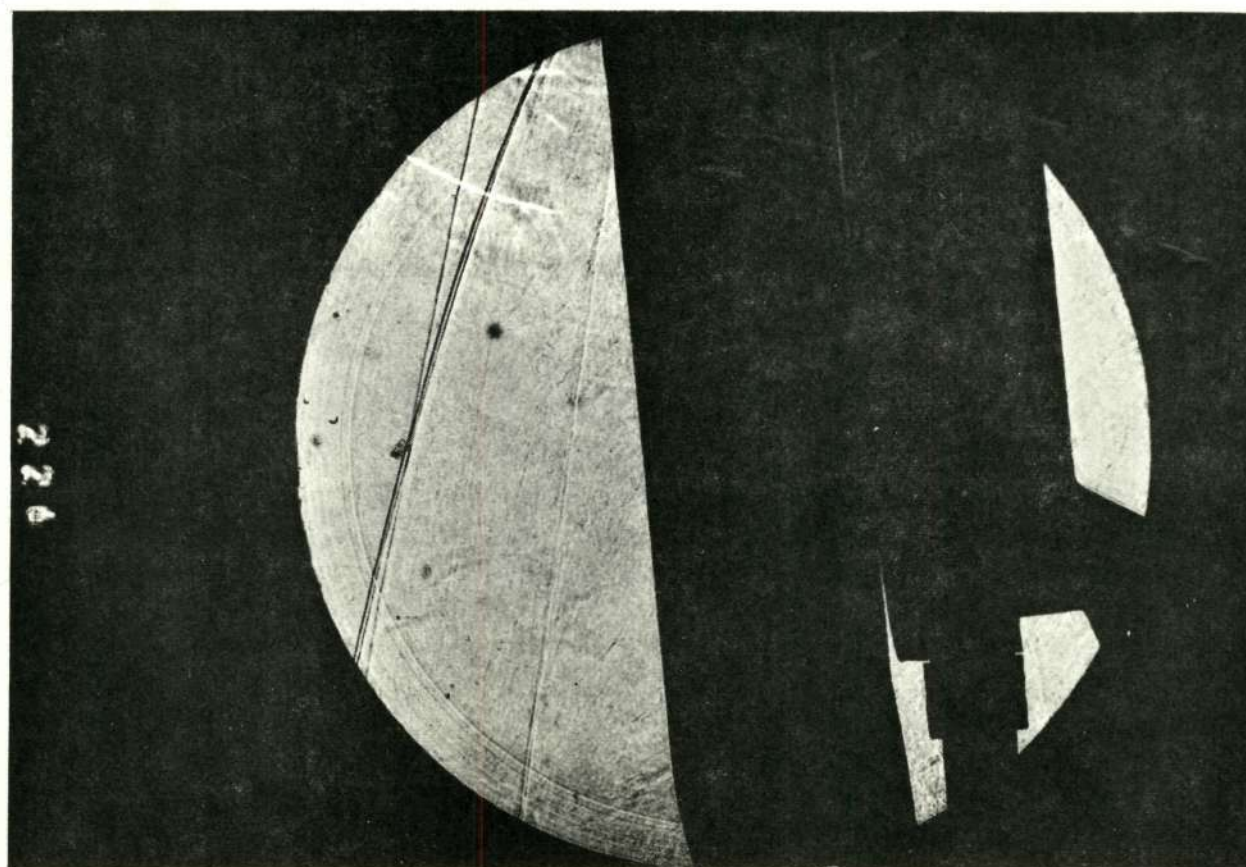
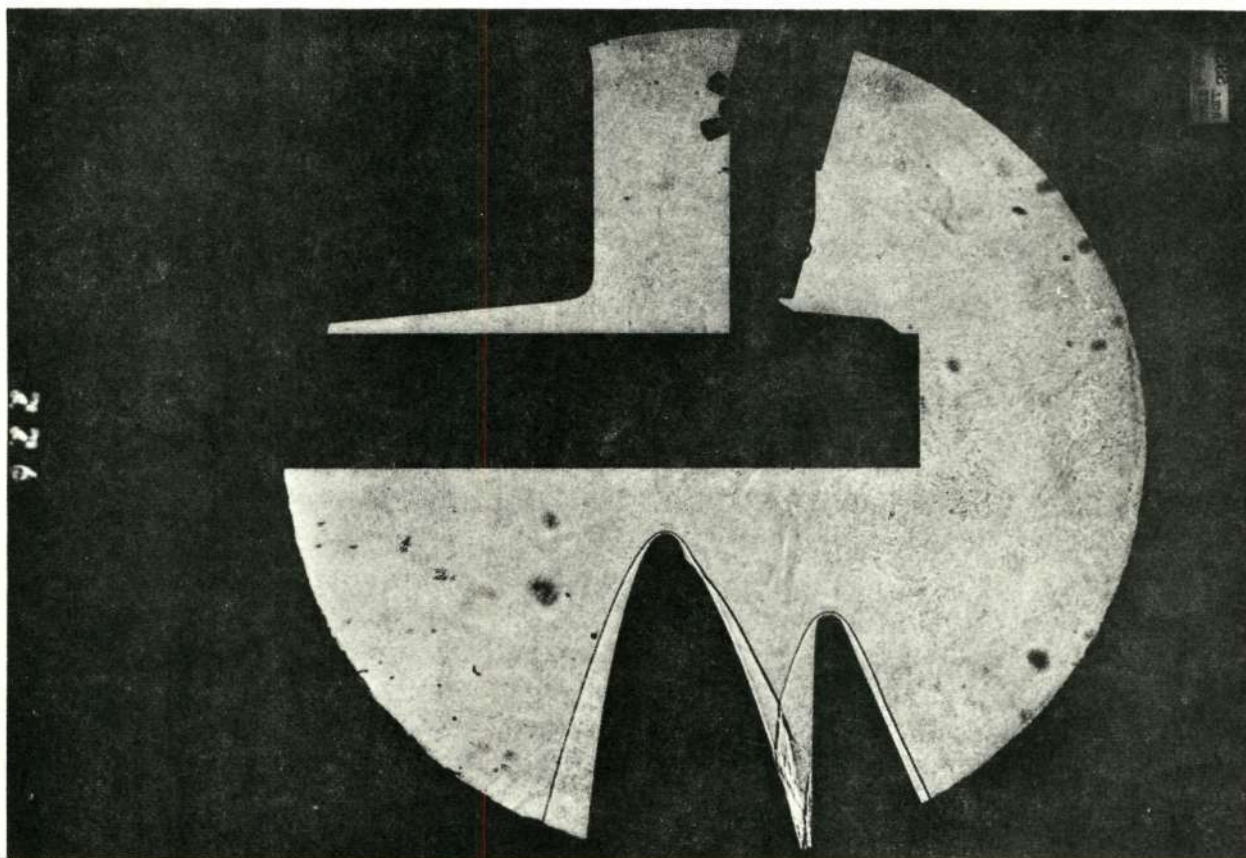
Shadowgraph Photograph at $\alpha = 0$, $\phi = 0$, $Re/ft = 2.5 \times 10^6$



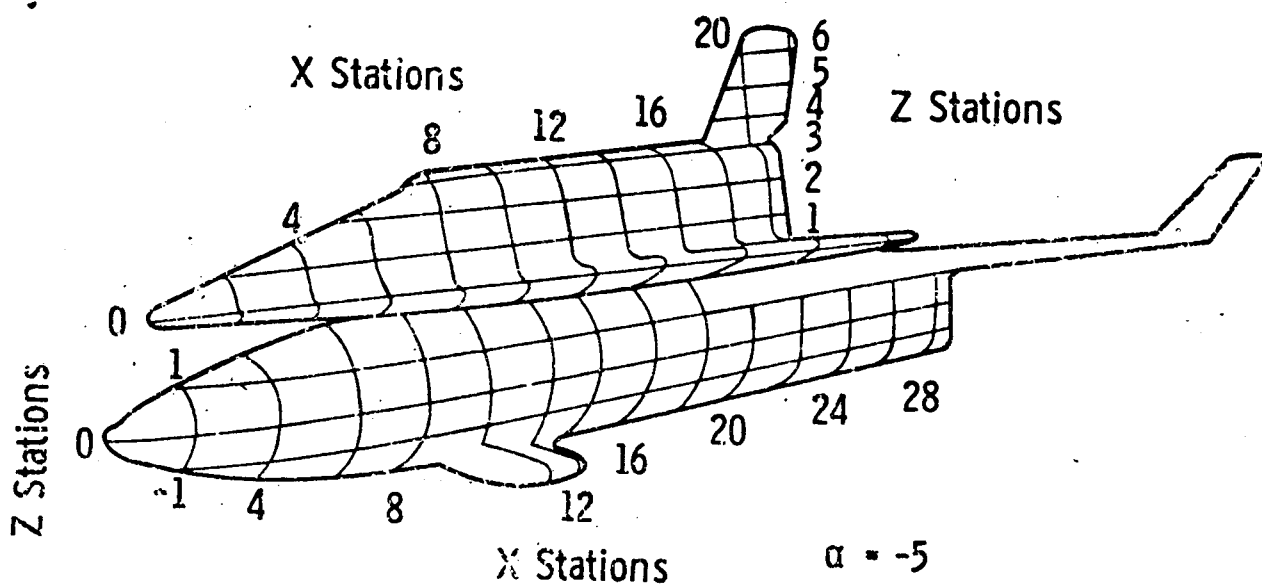
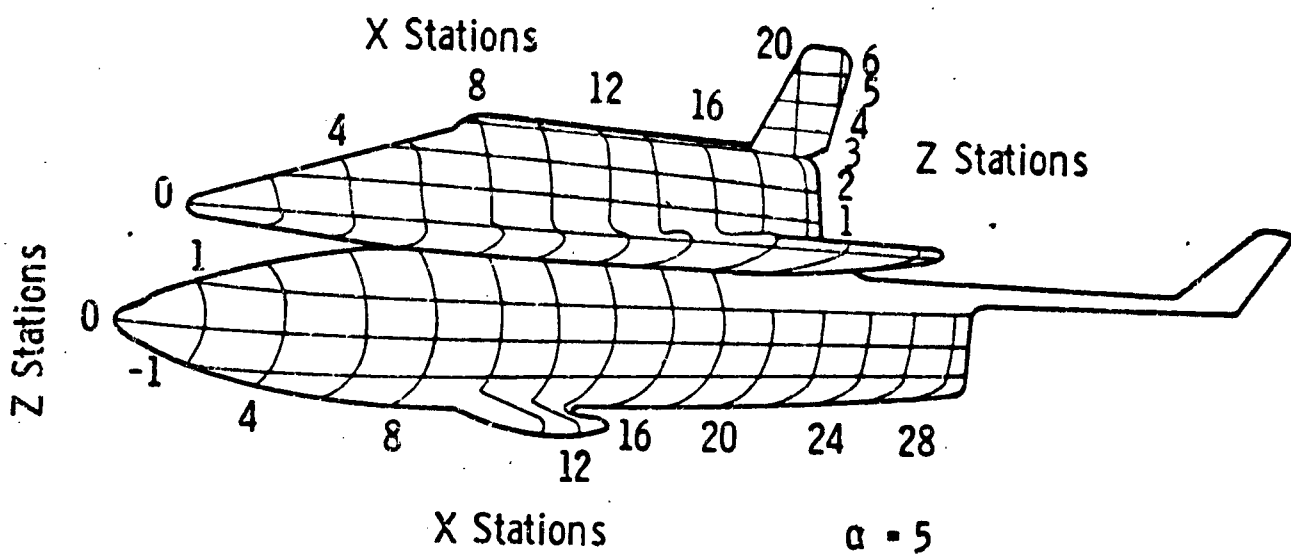
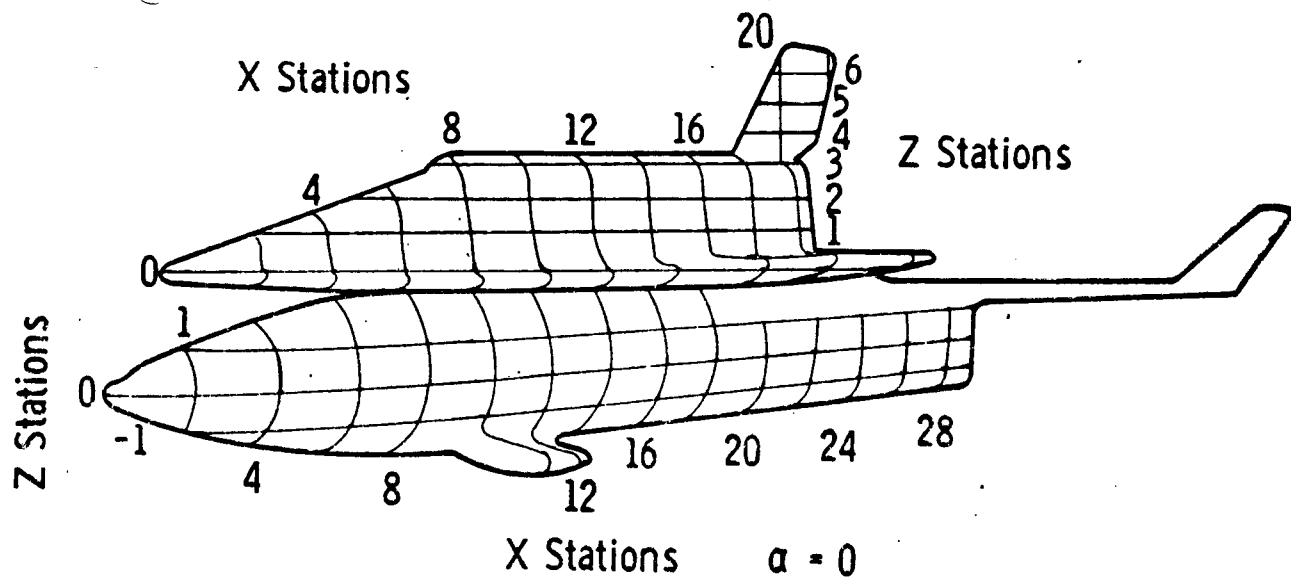
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Shadowgraph Photograph at $\alpha = -5$, $\phi = 0$, $\text{Re}/\text{ft} = 2.5 \times 10^6$



Grid Overlay for Mated Configurations